MUD COLUMN CHARACTERISTICS AND CONDITIONS IN THE CHENEY RANCH FIELD

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1.0 MUD COLUMN CHARACTERISTICS AND CONDITIONS IN THE CHENEY RANCH FIELD

1.1 SUMMARY

Responsive to EPA's December 3, 2019 letter Underground Injection Control (UIC) Permit Renewal Application Class 1 Non-Hazardous (NH) Permit No. R9 UIC-CA1-FY17-2R Technical Review Enclosure Item 1D, PEC has conducted further investigation of mud conditions in the nearby oil and gas wells. Well records on file at the California Geologic Energy Management Division's (CalGEM) online mapping application were obtained and reviewed for documentation of encountered mud conditions found during either well construction or plugging activities. Cheney Ranch Field is located north of PEC, near the periphery of the Area of Review. Records for every well that penetrated the Panoche Injection Interval were reviewed (23 wells). Details of well drilling and completion and plugging chronologies were generally included within the CalGEM public records. Some of the chronologies are very detailed while other records are "broad brush" summaries of general drilling activities.

Several of the detailed CalGEM chronologies present documentation of encountered mud conditions and properties in the local area. These details corroborate expectations from laboratory studies of mud properties and select well sampling of wells during reentry activities in other parts of the United States (see Appendix 4). In these cases, and as substantiated in the Cheney Ranch Field wells, the encountered static muds show the presence of stiff, thick muds in the wells. These mud have set up such that they are difficult to circulate and handle. As such, they will provide significant impairment to the emplacement of formation fluid or the advancing injectate into the wellbore and vertical displacement of the wellbore material. Therefore, these Cheney Ranch wells do not constitute a possible threat under the nonendangerment standard to human health or the environment as currently abandoned.

1

1.2 ENCOUNTERED MUD CONDITIONS

Well records on file at the California Geologic Energy Management Division's (CalGEM) online mapping application (https://maps.conservation.ca.gov/doggr/wellfinder/#openModal) were obtained for the Cheney Ranch Field. Well-specific chronologies were reviewed for documentation of encountered mud conditions either during well construction or plugging activities within the field. Information is included for three wells identified during records review. The location of the wells is presented in Figure 1 and the CalGEM records are contained in Appendices 1 through 3. The following information was found for three of the installed and abandoned wells:

• Lockhart England 1-31 (Appendix 1) – This well was spudded in December 1950 and drilled to a total depth of 10,357 feet in March 1951 with oil and gas shows observed below a depth of 10,000 feet. A production casing string (5-1/2 inch) was set to 10,038 feet and cemented with 300 sacks of cement. The oil and gas show interval from 10,038 feet and 10,169 feet (plugged back total well depth) were tested by displacing the drilling mud with fresh water and then swabbing the well. Results were inconclusive and operations on the well were suspended by setting a cement plug in the 5-1/2 inch protection casing from 9,880 to 10,169 feet and filling the well with "heavy drilling mud". The top of the casing was also plugged with 10 feet of cement and was capped with a welded steel plate. The details are documented reported on Notice of Intention to Abandon Well - Form 108 (dated August 9, 1952). The abandonment was approved by the Division of Oil and Gas on October 27, 1952.

A Supplementary Notice – Form 123 was filed on August 28, 1964, with the intent of salvaging as much of the 5-1/2-inch production casing as possible from the well. The Division of Oil and Gas approved the plan on Report of Proposed Operations – Form 111, also dated August 28, 1964. A hand-written note dated 9/21/64 on this Report of Proposed Operations, indicates that very heavy mud was encountered during a bailer run at a depth of 1,045 feet, with the bailer becoming "stuck" in the heavy mud. The bailer was worked free and recovery of casing and final well plugging operations were conducted. The Special Report on Operations Witnessed – Form 109-D (prepared by Division of Oil and Gas Inspector F. L. Hill and dated September 25, 1964) indicates that the well was cleaned out to 1,045 feet where very heavy mud was encountered. Six sacks of cement were dumped at that point and additional plugs were placed at 987 to 1,045 feet (6 sacks), 744

to 794 feet (26 sacks), 552 to 629 feet (33 sacks), and 5 to 15 feet (14 sacks), with 5-1/2-inch production casing recovered from a depth of 792 feet in the well.

Work on the well had originally been suspended on March 19, 1952, so the encountered mud during final abandonment had been in place for approximately 12 years. The gel strength of the 12 year old column of mud was such that a bailer on wireline could not be advanced deeper that a depth of 1,045 feet let alone to the shallowest cement plug depth of 9,880 feet in the casing string.

• American Hunter Souza 1 (Appendix 2) – The well was drilled to a total depth of 7,332 feet in November/ December 1983, using Benex mud (BENEX is an organic polymer designed for use as a bentonite extender and selective flocculant in freshwater drilling muds) with a final density of 11.2 pounds/gallon and a funnel viscosity of 37 seconds. Production casing (5-1/2 inch) was run to 10,213 feet and cemented 2,287 cubic feet of cement. The drilling rig was released in mid-December 1983.

A completion rig was set up at the end of March 1984, three and one-half months following completion of drilling activity. The well history attached to the Well Summary Report notes that the drilling mud had to be reversed out w/fresh water every 1,000 feet below a depth of 8,400 feet and every 6 joints below a depth of 9,000 feet with "thick drilling mud" being circulated from the well.

• Bender Silver Creek 57X-18 (Appendix 3) – The well was initially drilled to a total depth of 7,500 feet in May 2, 1973, using Lignosulfonate mud with a weight of 74 pounds per cubic foot and a funnel viscosity 51 seconds. Following evaluation of the original borehole, the operator made a request on May 3, 1973, to sidetrack the well from a depth of 4,100 feet and redrill the open hole to approximately 7,300 feet. This request was approved by the by Division of Oil and Gas on May 4, 1973 (Report on Proposed Operations (Form 111)).

The well was sidetracked with a kickoff plug set at 4,300' feet with 100 sacks of cement. After setting the cement kickoff plug, the rig ran in the well to 3,700 feet but could not break circulation at that depth (History of Oil or Gas Well – Form 103, Page 2) due to the combination of the weight of the static mud column and the additive pressure due to the gel strength of the mud (i.e., could not displace the mud from that depth with the rig pumps). This demonstrates that the mud "set" quickly as the kickoff plug had only been set the previous day. The drill pipe was moved up to the shallower depth of 3,560 feet,

where pump pressures were sufficient to break the mud column and establish circulation. The drill string was then staged in hole to the top of the kickoff plug while conditioning and increasing the mud to a higher weight.

These area-specific well records of encountered mud conditions confirm the longevity and efficacy of static mud columns within wells in and near the Area of Review for PEC. The CalGEM records document that encountered static mud columns are stiff and thick, having set up such that they are difficult to circulate and handle. These static clay-based muds provide significant resistance to inter-formational fluid flow through an abandoned well.

FIGURES

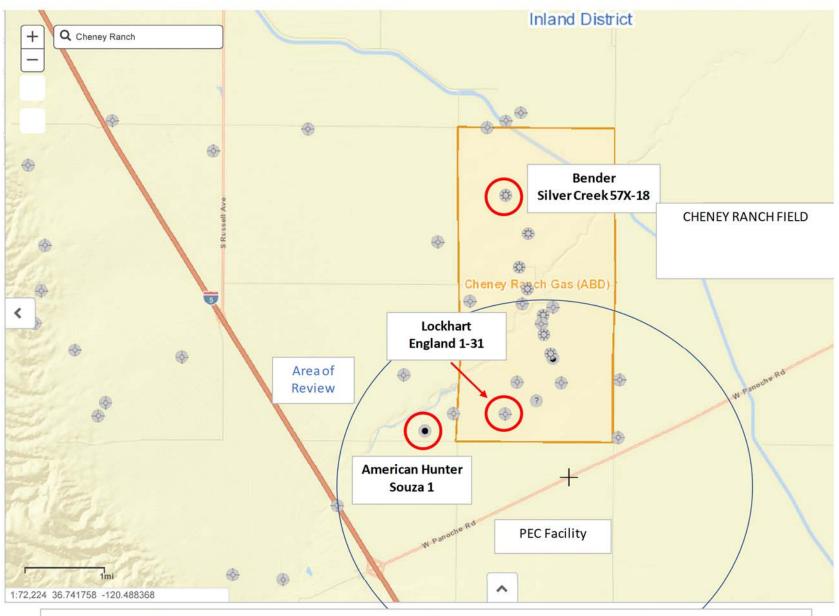


Figure 1 - Location map for Cheney Ranch Field - Wells with Documentation of Mud Characteristics



APPENDIX 1 CALGEM RECORDS - LOCKHART ENGLAND 1-31

STATE OF CALIFORNIA **DEPARTMENT OF NATURAL RESOURCES DIVISION OF OIL AND GAS**

REPORT OF WELL ABANDONMENT

TO PER TO PRESCHOR	Coalinga	California
TO THE PROPERTY OF THE PROPERT	September 29, 1964	
	,	
Mr. P D Elliston		
P O Box 536		
Avenal California		
Argent for ELLISTON OIL WELL SERV	ICING CO.	MSpecial
		O MASPECTION
Dear Sir:		
i. M	. LOCKHART	
Your report of abandonment of Wel	l No. "England" 1-3	1 ,
Sec. 31 , T. 14 s , R.13E , M D	B. & M., Cheney Ranch	field,
Fresno County,	dated September 24, 1964	, has been
examined in conjunction with records f	iled in this office.	
A review of the reports and records	shows that the requirements of	this Division.
which are based on all information filed		

No Bond Required

FLH:fd

cc: Conservation Committee

State Oil and Gas Supervisor

DH/Corum

Deputy Supervisor

STATUS

Completed Producing
Recompleted Producing
Completed Abandoned
Uncompleted Abandoned
Idle

Received	RECORDS	Neede	<u>.</u>
Lge_	Well Summary History Log & Core Sm Elec. Log(s Direct.Survey Other)Lge	Sm
Elevation Release F Hold Bond Final let 150b	Sond No Reason ter 2		<u>-</u>
card	25-64 25-64	0× 12	PAP

SUBMIT IN DUPLICATE

STATE OF CALIFORNIA

DEPARTMENT OF NATURAL RESOURCES

DIVISION OF OIL AND GAS

History of Oil or Gas Well

OPERATOR L. M. LOCKHART	FIELD Cheney Ranch
Well No. "England" 1-31	, Sec. 31 , T. 14 S. , R. 13 E. , M. D. B. & M
Date September 24 , 1964	Signed J. D. Clebon
	Title Contractor
(Address) (Telephone Num	mber) (President, Secretary or Agent)
drilling and testing of the well or during re-drilling, altering	y of the well. Use this form to report a full account of all important operations during the g of casing, plugging, or abandonment with the dates thereof. Be sure to include such items top and bottom of plugs, perforation details, sidetracked junk, bailing tests, shooting and
The $5\frac{1}{2}$ casing was cleaned out to	1045°, where the bailer encountered heavy mud.
6 sacks of cement was dumped into to 987 +.	the hole beginning at 1045, calculated to fill
The $5\frac{1}{2}$ casing was shot at 792^{9} a	and pulled to 782°.
26 sacks of cement was dumped int to 744°±.	to the hole beginning at 794°, calculated to fill
The 52" casing was pulled from th	ne hole.

Sept. 23

Date

1964

Sept. 22

Sept. 22

33 sacks of cement was dumped into the hole beginning at 629°, filling to 552°.

The 14" casing was filled with dirt from 552 to 15%.

A total of 14 sacks of cement was mixed and dumped on the bridge at 15, filling to 5.

DIVISION OF OIL AND GAS RECEIVED SEP 25 1964

COALINGA, CALIFORNIA

CALIFORNIA RESOURCES AGENCY DEPARTMENT OF CONSERVATION

DIVISION OF OIL AND GAS

Special Report on Operations Witnessed

No. T 564-256 P D Elliston P 0 Box 536 Coalinga Avenal, California September 25 1964 Agent for ELLISTON OIL WELL SPRVICING CO. DEAR SIR: L. M. Lockhart "England" 1-31 Sec. 31, T. 14 S., R. 13 E., M.D. B & M. Operations at well No.... Field, in Fresno Cheney Ranch _County, were witnessed Mr. F. L. Hill September 24. 1964 ____, representative of the supervisor was present from 9:30 a.m. to 10:30 a.m. There were also present P. D. Elliston. Contractor Present condition of well: 14" cem. 609; 53" cem. 10,038, four holes 10,017 W.S.O.: shot and recovered from 792°. T.D. 10,357°. Plugged with cement 10,286°-9880°+, 1045°-987°+, 794°-744°+, 629°-552°, and 15°-5°. The operations were performed for the purpose of plugging the hole in the process of abandonment. reported: Inspector Hill was present at the well from 11:00 a.m. to 2:00 p.m., on September 23, 1964, and Mr. Elliston reported: The 52" casing was cleaned out to 1045' where very heavy mud was encountered. On September 21, 1964, 6 sacks of cement was dumped into the hole beginning at 1045', calculated to fill to 987'.
The 5g" casing was shot at 792', and was pulled up to 782'. A wooden plug was driven to 794. The Inspector noted that 26 sacks of cement was dumped into the hole beginning at 794, calculated to fill to 744. Inspector Hill was again present at the well from 9:30 a.m. to 10:30 a.m., on September 24, 1964, and Mr. Elliston reported that on September 24, 1964, 33 sacks of cement was dumped into the hole beginning at 629, filling to 552. The Inspector noted: 1. The bailer was spudded on a plug at 552 and brought up a sample of set cement. 2. The 14" casing was filled with dirt from 552' to 15'. A total of 14 sacks of cement was mixed and dumped on the bridge at 15. filling to 5'.

THE CEMENTING OPERATIONS ARE APPROVED.

FLH: of

E. R. MURRAY-AARON State Oil and Gas Supervisor

By C. H. Diwin

Deputy

STATE OF CALIFORNIA DEPARTMENT OF CONSERVATION

DIVISION OF OIL AND GAS

REPORT ON PROPOSED OPERATIONS No. P. 564,-310

Mr. P D Filiston	
P 0 Box 536	Coalinga Calif
Avenal California 93204	August 28 1964
Agent for ELLISTON OIL WELL SERVICING CO.	
DEAR Sir:	L. M. Lockhart Well No. "England" 1-31
Section 27 T 14 C R 12F W D R & M	Chency Ranch Field, Fresno County
	is been examined in conjunction with records filed in this office.
Present conditions as shown by the records and the proposal a	
, 1 1	
THE NOTICE STATES:	
"The present condition of the well is	as follows:
Total depth 10,357, plugged with co	ement 10,357'-9,880', and 10'-surface.
Complete casing record including plu	g6.
14" cem. 609".	
5½" cem. 10,038*, four 3/8" holes	10,017' W.S.O. "
TIPMINAMAT	
PROPOSAL:	
We now propose Pull $5\frac{1}{2}$ casing from as deep as p	an la la la ma
If recovered from below 1400; 1	place compart plus 15001-13001
II recovered from parow 1700, 1	place 100° cement plug on the stub.
Cap 14" casing at the surface with	h 10° of cement."
and with unwinterfd me notes of the result in 1144 of	ing the state of t
DECISION:	
THE PROPOSAL IS APPROVED.	
19164 Elliston / Cormin	
on inde anamarial very heavy mild	
121/64 Fileston Corumic C.O. 1045, encountaged very heavy mud. Study batter, but finally worked laws.	
Will dump best before shooting of 5/2 cg.	
the state of the s	

No Bond Required CHC:ef & cc: P D Elliston

E. R. MURRAY-AARON, State Oil and Gas Supervisor

y C. H. Corwin , Deput

STATE OF CALIFORNIA
DEPARTMENT OF NATURAL RESOURCES

DIVISION OF OIL AND GAS

Supplementary Notice

	Coalinga	Calif	August 28	19 64
DIVISION OF OIL AND GAS				
Coalinga	Calif.			
A notice to you dated August 9	L. M. Lockhar	, 19_9; t "England"]=	2, stating the	intention to
(Drill, deepen, redrill, abandon)	well INo	Change	<u>ب ب</u> المسكوس	
(Drill, deepen, redrill, abandon) Sec. 31 , T. 14 S. , R. 13 E.	, M. D. B & M		13 16 17 18 V	Field,
Fresno	County,	should be amended	d because of chang	ed conditions.
The present condition of the well is as follows:				
Total depth 10,357°, plugged with	n cement 10,357'-9	,880°, and 10	O'-surface.	
Complete casing record including plugs.				
14" cem. 609". 5½" cem. 10,038", fo	our 3/8" holes 10,	017° W.S.O.		
We now propose				
Pull $5\frac{1}{2}$ " casing from If recovered from 11" Cap 14" casing at 12"	n below 1400°, pla above 1400°, pla	ce cement place 100° cemen	ug 1400°-1300 nt plug on th	esstub.
Reference to file of data Sorms 11- 121				
g + 2 cc to Elliston	Elliston	Oil Well Ser	vicing Co.	
(Address)			Operator)	77
(Telephone No.)	Ву	-6.d.	Lee	CO~

DIVISION OF OIL AND GAS

REPORT OF CORRECTION OR CANCELLATION

		Coalinga	California
Mr	P D Elliston	May 22 1957	
, A.C.	P D Elliston P O Box 536 Avonal Call formin		
-	Avenal California ELLISTON OIL WELL SERVICING CO.		
-	Minimalitation of the same research for one		
Dea	ar Sir		
T.	n accordance with your letter dated May	20 1957	
11.	r accordance with gas masses and		
the :	following change pertaining to yourswelland	L. M. Lockhart well No.	"England",
Sec.	31 , T. 14 S. , R. 13 E. , M. D. B. & M.	100 Non tan-uin non	field,
	Program Commanda N		1
	Fresno County, District No.	, is being made in	our records:
□ ′	The corrected location is		
	· · · · · · · · · · · · · · · · · · ·		
□ ′	The corrected elevation is		
	Report No, dated		, has been
	acquired as fallows.		
•	corrected as follows:		
	· · · · · · · · · · · · · · · · · · ·	; 1	
_			<u></u>
	supplementary Your/notice to abandon		
X	Your/notice to abandon (Drill, abandon, etc.)	datedMay 6, 1953	······································
á	and our report No. P. 553-128 , issu	ied in answer thereto, are her	eby cancelled
;	inasmuch as the work will not be done. If you	have a drilling bond on file	covering this
		<u>-</u>	covering time
J	notice it will be returned. No request for such	return is necessary.	:
	Other:		•
		•	
	111577.		1
	1952 W	elacar -	70
		E. H. Musser	
c:	Mrs J O England	State Oil and Gas Supervisor	
	was the second product of the second control	$\sim 11/3$	

52631 3-57 6250 SPO

Dept of Water Resources

M- OWW Deputy Supervisor 108 2

ELLISTON OIL WELL SERVICING CO.

201 WEST STANISLAUS AVENAL, CALIFORNIA

May 20, 1957

Division of Oil & Gas California Department of Natural Resources Coalinga, California

Gentlemen:

In answer to your letter of May 16, 1957 regarding my notice dated May 6, 1953 to pull casing from abandoned L.M. Lockhart well No. "England" 1-31, Sec. 31, T 115., R 13 E., M.D.B.& M, Fresno County, I would like to cancel this request temporarily, as I am planning to submit a request to do some exploratory work in that well prior to pulling the casing, provided I can get a lease.

I will contact your office prior to my doing any work on the well.

Very truly yours,

Elliston Oil Well Servicing Co.

P. D. Elliston

MALHAR HAHAMANA

Coalinga California

May 16 1957

Mr P D Elliston Elliston Oil Well Servicing Co P O Box 536 Avenal California

Dear Sir

Please refer to your notice dated May 6, 1953, to pull casing from abandoned L. M. Lockhart well Mo. "England" 1-31, Sec. 31, T. 14 S., R. 13 E., M. D. B. & M., Fresno County.

In the event that this work has not been started, and you do not plan to commence the work immediately, please furnish this office with a letter requesting cancellation of the notice.

Yours truly

C. H. Corwin

C H CORNIN Deputy Supervisor

5/17/57 Elliston phoned. Plan to so into well soon. Estate problems, Will send in letter requesting concellation.

STATE OF CALIFORNIA DEPARTMENT OF NATURAL RESOURCES

DIVISION OF OIL AND GAS

No. P 553-128

REPORT ON PROPOSED OPERATIONS

	Coalinga	Calif	May 15	19 53
MR. P D Elliston				
P O Box 536 Avenal	Calif.			•
Agent for ELLISTON OIL WE	LL SERVICING CO.			
a Comment of the Comm	***			
Dear Sir: Your supplementary propos	abandon	L. M. Lo		_31
				,
Section 31 , T. 145., R. 13E. , M. D.B. &	M., indicate the state of	Field,	Fresno	County,
dated May 6, 19 53, received May 14,	19_53., has been examin	ed in conjunctio	n with records filed	in this office.
Present conditions as shown-by the record	is and the proposal are as	follows:		
THE NOTICE STATES:	_			
"The present condition of the way	ll is as follows:			
1. Total depth. 10,3571, plu	gged with cement	10,3571-9,8	60', and 10'-	surface.
2. Complete casing record.				
5½" cem. 10,035, four 3,	/8" holes 10.0174	. W.S. U. "		
		Canada		
raurusku:	*** ₁	Bandan Marian Caranta	, LL I'M ET WEARING	~
"The proposed work is as follows Pull 5½" casing from as deep		Servery reverse return	I Salve to Grante July to State of the	
If recovered from below 1400	O', place cement	plug 1400!-	1300%.	
" " above 1400	0', place 1001 ce	ment plug o	n the stub.	
Cap 14" casing at the surface	and turn well ov	er to lando	wner før dise	as
a water well."		2		Commence of the Commence of th
DECISION:		6	·	and de service
THE PROPOSAL IS APPROVED PROVIDE	D THAT this Divis	ion shall b	e notified to	witness
the placing and location and h	ardness of the ce	ment plug.		& .
	•			
			ت	. ~
Location: 660 feet South and 660 :	feet East from ce	nter of Sec	tion 31.	W.
The landowner, Mrs. John O. England	_			ifornia,
to whom the well has been quito		sted in wri	ting that the	well be
left in condition to convert to	water.			- American
No Bond Required				
GGP:ef cc: Mrs J O England				
Division of Water Resources) _	
	R. D. BUSH	d. J. //	1)	
iork bot yet done 6-29-54	Scate Oil and	Gas Supervisor	for a m	
still plan to do it.	Ву	/ · / ·	June	Deputy
- respectively. The second			and the second s	

STATE OF CALIFORNIA DEPARTMENT OF NATURAL RESOURCES

DIVISION OF OIL AND GAS

Notice of Intention to Abandon Well

This notice must be given at least five days before work is to begin; one copy only

	Coalinga	Calif	May 6	19_53
DIVISION OF OIL AND GAS				
Coalinga	Calif.			
In compliance with Secs. 323 L. M. Lockl	nart	•	93, Stat. 1939, notic	ce is hereby given
that it is our intention to abandon well No.	"England"	<u>' 1-31</u>		
Sec. 31 /, T. 14 S. , R 13 E.	M. D. B. & M.	~	-	Field,
Fresno	County, com	imencing wor	k on the	day
of	19			•
The present condition of the well is as follows:				
1. Total depth. 10,357, plugge	ed with cement 10	0,3571-9,8	380', and 10'-	- surface.
	ALLEGO CONTRACTOR OF THE SECOND			
2. Complete casing record.		$\overline{}$		
14" cem. 609 '. $5\frac{1}{2}$ " cem. $10,038$ ', for	ur 3/8" holes <u>10</u>	,017' W.S.	.o. Ee/	
5		The state of the s		
- 49	6	parameter and the second	5	-/
3. Last produced.	2			12457
The proposed work is as follows:	Nepoli		ravity	Cut
	1400'-, place cer 1400', place 100	O' cement	plug on the	
Cap 14" casing at the sur	face and turn we			
	W 10 OT CERRENT	DIVIS R E	ION OF OIL AND	GAS
Reference to file of the		ſ.	AY 1 4 1953	.,
		COAL	ina, altorna	
	E	lliston O	<u>il Well Servi</u>	cing Co.
		(Name	of Operator)	
		1 2	H. Los	

May 4, 1953.

Division of Oil and Gas -- Attention Mr. Peirce: - Elm Street Coalinga, California

Dear Sir:-

We are owner of $Sec\frac{1}{4}$) of Sec 31- Township 14, South-Range 13 East. Mr. Lockhart has quick claimed the property back to us- "England No.#1."

We are selling the salvage-casing in the hole to Mr. Elliston's Company, the Oil Well Servicing Co. We want the well left in such condition so we can use it as a water well.

We appreciate Mr. Ellistons interest and thank you for any consideration in this matter.

Yours very truly,

Mrs. John O. England 649-45th Avenue

San Francisco, 21

California.

17.7 51953

CONTENTS IN A CONTENT

STATE OF CALIFORNIA DEPARTMENT OF NATURAL RESOURCES DIVISION OF OIL AND GAS

REPORT OF WELL ABANDONMENT

****	Coalinga	, California,	October 27	, 19_52
•				
Mr M H Fuller Agent L. M. Lockhart Box 165				
Burrel California				
Dear Sir				
Your report of aband	onment of Well No.	"England"	1-31	
Sec. 31 , T. 14 S., R. 1	<u>ЗЕ., М. D.</u> В. & М			oil field,
Freeno	County, dated	October 1	1, 1952	, has been
examined in conjunction w	ith records filed in th	is office.		
A review of the repo			irements of th	ie Division
				. DIVISIOII,
which are based on all info	mation med with it,	nave been fun	mea.	
	·			
	Lap Lap GH	le of deta		
Gwu:ef				
Orig: Company, L.A. cc: Mr M H Fuller		O. BUSH Oil and Gas Superviso	or	
er en		$\mathcal{L}_{\mathcal{A}}$	24	
	Ву	<u> 7.</u>	7. Je	UL Supervisor
			Depa	ity Supervisor

57615 2-52 12M SPO

SUBMIT LOG IN DUPLICATE

FILL THIS 5 TIM WITH TYPEWRITER. WRITE ON ONE SIDE OF PAPER U

STATE OF CALIFORNIA DEPARTMENT OF NATURAL RESOURCES

DIVISION OF OIL AND GAS

	,	,	LOG	OF OIL O	R G/	AS WI	ELL				
Operator	L. M. L	OCKHA	RT	F	ield Z	ANOCI	TE GR	EK A	REA,	FRESNO	COUNTY
Well No.	"ENGL	AND" /-	3/	Sec	3/	, T.	145.	, R. 13	E.	M.D.	В. & М.
record of Date Oct	GGO'S. A CENTER OF In compliance the present cor fober 11, M. Ear Engineer or Geolog	with the providition of the	31-14/13. risions of Chap well and all wo	ter 93, Statute rk done thereon	s ot 15	39, the ar as can Si	intormatio	n given he	rewith is all avails	a complete an able records.	2
				uperintendent)						dent, Secretary or	Agent)
Total de	pth 10,33	57 Plugg	- /950 ged depth 54	RFACE			EOLOGICAL			lling tools Ro	PTH
TE: WE	ced producing LL SUSPEN Z-51. (SEE NTARY NOTE G. MTED 1	NDED @ -	(date) Clean Oil bbl. per day	Gravity Clean Oil	(cross	g/gas lif out unneces Cent Water ding emulsio	T	Gas . per day	Alas San	Tubing Pressure	Casing Pressure
	Initial p roduction after							4			
		<u> </u>	C	ASING RECORD	(Prese	nt Hole	.)		1 1	Sen du	
e of Casing A. P. I.)	Depth of Shoe	Top of Casing	Weight of Casing	New or Second Hand		miess ipweld	Grade of Casing		of Hole landed in	Number of Sacks of Cement	Depth of Cementing if through perforation
14"	609'	SURFACE	47.54	NEW	SM	<i>15</i> .	SJ	2	0"	700	- through personation
5-1/2"	10,038	4/	20 [#] 8	"			N-80 E J-55		5/8"	300	
				,	and the second		<i>J</i> -33				,
				Perfor	ATIONS	}					
ze of Casing	Tros A7	То	Size	of Perforations		Numbe of Row		istance en Centers		-Method-of Peri	foretiess_
5-1/2"	10,017 ft.	ft.	4-3/8 he	okes gun p	erfo	ralea	for W	V. S.O.	(mtd. O	ff.
	ft.	ft.				ļ					· · · · · · · · · · · · · · · · · · ·
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	ft.	ft.		Th						-	
E	lectrical Log I	Depths 7	ECORDED	FROM 10	33	-g' -	609		(Attac	h Copy of Lo	eg)

DIVISION OF OIL & GAS

HISTORY OF OIL OR GAS WELL

Operator: L.M. Lockhort

Panache Creek Area - Fresno County

Well: England 1-31

Sec. 31 - TI45 - RIBE - MDB&M.

Date: October 11, 1952

Signed: Glemmokarl.

Title: ENGINEER

Location: 660'S. and 660'E. from center of Section 31-14/13.

NOTE: All depth measurements from Kelly Bushings.

Elevations: Ground 406.6' (Surveyed). K.B. 419.1'

Gleun M. Earl, Engr. - M. H. Fuller, Lockhart Supt. Fowler Drilling Co., Contractor - O.D. Chase, Supt. - Woldrip Most.

Casing & Hole Record:

11-26

Rigging up.

14" 47.54 ** New Smls. SJ Csg. cmtd. w/700 sax cmt. at 609' in 20" hole.
10-58" hole 609' - 7425'. (Changed from 4-1/2" to 3-1/2" drill-pipe at 7425\)
9-78" hole 7425' - 10,033'.
7-58" hole 10,033' - 10,357' (Total Depth)
5-1/2" 20* N-80 & 17* J-55 New Smls. Csg. cmtd. w/300 sax cmt. at 10,038'.

REMARKS DATE 1950 11-11 Surveyed Location - Andersen Surveyors, Fresno. Grading out sump; digging cellar; building road. 11-16 Pouring concrete for cellor. Laying concrete inotte for sub-base and Waldrip Mast. Lee Boyd, Contractor. 22" conductor pipe. 80 yards concrete. 11-17 Installed water line. Sump completed. 11-20 Moving Fowler Drilling Co. equipment from Burnel to location "England 1-31. Finished moving equipment from well "Burnel" 1-28. Rigging up. 11-22 II- 23 Rigging up. Installed water pump. 11-24 Rigging up . Houled GCI of 14" 17.54 surface csq. (16 joints) . 14" Brodenhead. 11-25

L.M. Lockhart "England" 1-31

WELL HISTORY (Cont'd.)

1950

Drilled rat-hole in sticky clay. Spudded in at 2:00 P.M., Nov. 27, 1950.

Drilled 20" hole to 255' Eastman Single Shot Survey at 100' @ 1/4".

with Smith Reamer Bit.

" " " 200' @ 1/4"

//-28

Drilled 20" hole 255' to Gog'. Survey at 300' @ 1° 00'
" " 400' @ 0° 50'
" " 500' @ 1° 00'
" " Goo' @ 1° 30'

Started to run 14" surface csg. but pipe would not go after 2 joints run, Pulled the 2 joints of casing - balled up with mud at shoe. Ron in hole with 20" Smith Reamer, reamed hole to bottom, and conditioned mud.

11-29 Ran 15 joints of 14" 47.54 new scamless slip-joint casing aguipped with Halliburton Float Shoe. Total pipe 613'. Casing landed at 609' and cemented with 700 sax Permanente Type-C Construction Cement treated with 2 sex Flosele. Mixing time 23 minutes. Displaced cement with 585 cu.ft. drilling fluid. Displacement time 38 minutes. Recovered approximately 120 sax cement to surface. Rotated casing through Cementing operations. Halliburton Power Equipment and bulk cement. Job completed 2:45 A.M.

Standing cmid. Landed 14° surface csg. and installed Shaffer B.O.P. equipment. Tested Double Control Shaffer Gate w/1000 to for 5 minutes. OK.

11-30 Ran in hole with 10-5/ bit on 4-1/2 drill-pipe and found top of cement in 14" csg. at 597". Drilled out cmt. plug, and shoe at 609'.

Tested B.O.P. with 1000 for 15 minutes. Test OK. Changed mud.

Drilled 10-5/8 hole 609'-1218'. Survey at 750' @ 1° 30'
" " 850' @ 1° 00'
" " 980' @ 1° 30'
" " 1090' @ 0° 45'

|2-1 Drilled 10-5/8" hole |218' - 1511'. Survey at 1280' @ 0° 10'.
" " 1380' @ 0° 30'.

Jumped a pin at 1511' and left a sub and two 6-3/4" drill-collars in hole. Ran Baash-Ross Socket and recovered fish on 3rd run.

Started taking Shaker Screen Samples at 1500' - every 30 feet.

" 2025' @ 0° 35'

L.M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

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1950

12-2 Drilled 10-5/6 hole 1511' - 2084', Survey at 1480' @ 1° 00'

" " 1580' @ 0° 50'

" " 1780' @ 1° 00'

" " 1900' @ 0° 30'
```

Pulled out of hole of 2084 to run 12-1/4" Hole Opener and open hole from 10-5/8" to 12-1/4" so that 8-5/8" cosing could be run. Security 12-1/4" Hole Opener would not go thru nipple above B.O.P. Tried 12-1/4" Security rock bit and it would not go thru.

Ron in with 10-5%" bit and drilled 2084'-2088'.

12-3 Drilled 10-518" hale 2088'-2835', (Taking drift shots inside drill-pipe with Eastman Single Shot Survey Instrument approximately every 100'.)

Survey at 2/25' @ 0° 35'
" " 2730' @ 0° 45'
" " 2335' @ 0° 45'
" " 2445' @ 0° 30'
" " 2595' @ 0° 45'
" " 2744' @ 0° 30'

Used four 10- 1/8" rock bits from 609' to 2775'.

NOTE: Began making Time Log at 2730': minutes per 10' of hale drilled.

- 12-4. Drilled 10-5/g" hole 2835' 3224'. Survey at 2835' @ 0°45'
 " " 2963' @ 0°45'
 " " 3186 @ 1°20'
- 12-5 Drilled 10-5" hole 3224' 3470'. Survey at 3296' @ 100'.
 " " 3400' @ 1015'.

Used seven 10- 1/8" rock bits from 609 to 3470; from shoe of surface casing to approximate Top Krayenhagen Shale.

12-6 Drilled 10-5% hole 3470 - 3597 . Survey of 3500' @ 10 05'.

Took Core No. 1 from 3597 - 3615'; Dunlap Conventional Core Borres; 8-1/2" Drag

Head. Reamed out 8-1/2" rat-hole to 10-3% from 3597' to 3615.

L.M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

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1950
                                                                 Survey at 3620' @ 1° 00'
" " 3734' @ 1° 00'
" " 3836' @ 0° 50'
 12-7
                 Drilled 10-5/8" hole 3615' - 4020'.
                                                                       " 3940' @ 0° 55'
                  Toking Shaker Screen Samples every 30 feet.
                Drilled 10-5/8" hole 4020' - 4350'.
                                                                  Survey of 4075' @ 10 00'
12-8
                Mud weight 15 - 77 # Viscosity 43 - 45
                                                                             " 4185 @ 1º 15'
                                                                             " 4300' @ 0° 55'
                Drilled 10-5/8" hole A350' - 4630'.
12-9
                                                                   Survey at 4405' @ 1° 00'
                Mud weight 15-78 # Viscosity 43-48 Sand Content 2 to 3%
                                                                               " 4510' @ 0° 35'
                                                                               " 4608' @ 0°55'
                Drilled 10-5" hole 4630' - 4754'. Survey of 4710' @ 0°35'.

Cored 8-1/2" hole 4754- 4774' with Dunley Conventional Bbl. @ 4-way drag head.
12-10
                Drilling with two 6-1/4" and two 7-1/4" drill-collars; total length 164.74'.
                Weight on bit 3 to 4 tons; 175 - Zoo r.p.m.; 800-900 psi pump pressure. 4-1/2" full-hole drill-pipe. Hughes OSC-3 and Smith 2-cone bits.
                Cored 8-1/2 hole 4774 - 4787 with same tools as above. Opened up 8-1/2" rat-hole 4754-4787 to 10-5/2".
12-11
                Drilled 10- 3/ hole 4787' - 4950'.
                                                                              Survey at 4820' @ 1° 00'.
                Drilled 10-98" hole 4950' - 5150'.
12-12
                                                                       Survey at 4950' @ 100'.
                Measured out of hole. Corrected
                Measurements 5143'. Ran in hole
                with new 10-48" rock bit; found tight hake at 4970; reamed to bottom @ 5143'.
               Drilled 10- 1/2" hole 5143' - 5387' (244').
12-13
                                                                       Survey at 5182' @ 0° 45'.
                                                                             " 5300' @ /° 30'.
               Drilled 10- 1/2 hole 5387' - 5451.55'.
12-14
                                                                              Survey at 5413' @ 0°30'.
              Ran Schlumberger Electrical Log and cheeked bottom @ 5451', and recorded from 5450' - Gog'. Ran Schlumberger Sidewall Sampler; recovered 16 samples from interval 5350'- 2695'.
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Drilled 10-5/ hole 5451 - 5480 .

12-24.

12-25

full.

L.M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

1950 Drilled 10-5, hole 54 - 5636' (156'). 12-15 Survey of 5514 @ 1º - 30. " " 5630 C 0°-40' Drilled 10-5/8" hole 5636' -5895' (259') 12-16 Survey at 5713' @ 0°00' (?) " 5844' @ 1º 00'. Drilled 10- 1/8" hole 5895' - 6110' (215') 12-17 Survey at 5953' @ 0° 35. " " 6085' @ 0° 00'. Drilled 10- 58" hole 6110' - 6140'. Cored 8-1/2" hole from 6140' - 6172'. 12-18 Caring with Dunlap Wire-line core barrel , 8-1/3" four-way drag head. Cored 8-1/2" hole 6/72' - 6202'. Opened up 8-1/2" rot-hole 6/40' to 6202' to 10-5/8". Drilled 10-5/8" hole 6202' - 6263'. Survey at 6263' @ 2° 00'. 12-19 Prilled 10-7g" hole 6263' - 6410' (147'). Survey at 6380' @ 2° 10'
Ran in hole with Hughes Two-Cone bit at 6387' in endeavor to straighten hole after above coring. 12-20 Survey at 6380' @ Zº 10' . Drilled 10-5/" hole 6410' - 6556' (146'). 12-21 Survey at 6500'. @ 2º 30'. Drilled 10-1/9" hole 6556' - 6647' (91'). Using Hughes LW3 Two-Cone bit. 12-22 Survey at 6598' @ 1º 30'. Drilled 10-5/8 hole 6647' - 6704' (57'). Survey at 6686' @ 1º 30'. /2-23 Instrument Co., 2200 W. Mabama, Houston, Texas.) Welded Detector to flow line. Macco mud tests at GG86: Weight 74-1/2"; Viscosity 55; Filtrate @ 30 minutes @ 7.2 c.c. woter loss; Filter cake 3/32"; Sheer -Initial 0, Shear - 10 minute 7; Sand Content @ % X Volume 1.5. Mud has good test properties.

Drilled 10-5/8 hole 6704'-6730'. Shut down rig at 8:00 A.M. @ X-MAS.

Watchman mixed mud and Kept hole

Depth 6730'. Rig shut down.

L.M. Lockhort "England" 1-31 WELL HISTORY (Cont'd.)

1950

Started operating rig at 8:00 A.M. Went in hole with Smith K2-P rock bit; circulated and conditioned mud; reamed tight spots; reamed 300' of tight hole at bottom with the Smith cross-section bit; circulated and conditioned mud from bottom at C730'.

Drilled 10-5%" hole 6730' - 6733' in 2-1/2 hours before midnight.

Adjusted Gas Detector and storted it operating.

12-27 Drilled 10-5/8" hole 6733' - 6791' (58').

Replaced Emsco Tail Clutch.

12-28 Drilled 10-5/8" hole 6791'-6938' (147'). Survey of 6800' @ 1005'.

12-29 Drilled 10-9/8" hade 6938' - 7070' (132'). Survey of 7030' @ 0° 55'.

Macco mud tests at 6979': Weight 15#; Filtrate @ 30 minutes @ 8.5 c.c. water loss; Filter cake 2/32"; Shear - Initial 0, Shear 10 minutes 6; Sand Content 1.7%. Sulphates in drilling water 50 9/9; Salt 20 9/9.

12-30 Drilled 10-5 hole 7070' - 7090'. Circulated and checked intensity reading on Gas Detector. Measured out of hole: Corrected Measurement 7091.68'.

Ron 2nd Run Schlumberger Electrical Log and could not get below 6976. Recorded from 6975' to 5450'.

Ran in hole with Dunlop wire-line core barrel equipped with Hughes 8-1/2" rock head, Cored 8-1/2" hole 7091'-7111'.

- 12-31 Cored 8-1/2" hole 7111' to 7124'. Pulled out to make Open Hole Formation Test of interval 1112'-7124' in 8-1/2" rat-hole. Depth of well @ 7124'.
- (7112'-7124') FORMATION TEST NO. |. Ran Johnston Formation Tester on 4-1/2" full-hole drill-pipe. Tester equipped with 4-1/2" Suffiff Hydraulic Jars and Homco 4-1/2" Safety Joint. Used 2 8" x 21/8" x 30" straight wall packers. Set packers at 7103' and 7112' with 12' of 5-1/2" anchor. No water cushion used. Tester Value with 1/2" bean opened at 12:01 p.m. & remained open for 40 minutes. 1/4" bean at top. Packers held OK with only 1-1/2 loss of fluid during tast. There was a medium steady blow of air after 1 minute, which continued with gas to surface in 14 minutes, which continued during the remaining 25 min. of test with no increase in blow. Recovered a fluid rise of 15', consisting of slightly gas-cut medium drilling fluid. No saft water. The 2 pressure bomb charts indicated tool operated properly, the tester valve being open during the entire test. Pulled tester and ran back with Dunlop 8-1/2" wire-line core-bbl. with new Hughes rock head.

Cored 8-1/2" hole 7/24'- 7/26'.

L.M. Lockhort "England" 1-31 WELL HISTORY (Cont'd.)

1951

Cored 8-1/2" hole 7/26'-7/50'. Pulled out of hole to make Open Hole Formation Test of interval 7/04'-7/50' in 8-1/2" rat-hole. Depth of well@ 7/50'.

FORMATION TEST NO. 2. Ron Johnston Formation Tester on 4-1/2"
full-hole drill-pipe. Used Sutliff Hydraulic Jars & 4-1/2" Homeo Sofety Joint. Two
8" x 2-1/8" x 30" straight wall packers were set at 7095' & 7104' with 46' of 5-1/2" onchor. (7104'-7150') No water cushion used. Tester valve with 3/4" boon was opened at 4:00 p.m. Flow period @ I hour . Shut - in period @ 15 minutes. Packers set I hour & 15 min . & held ok. C I hour. Shut-in period C 15 minutes. Packers set I now a 15 min. & held ok.

There was a medium, steady blow for I hour. Gas to surface in 22 minutes and continued for remainder of the hour. Recovered 2000 feet of fluid of which the top 180' was slightly gas-cut medium drilling fluid, and the remaining 1820' consisting of salt water. The 2 pressure bomb charts in dicated the tool operated properly. The abouts showed a flow pressure of 1000 at the end of the I hour flow period. During the 15 min. shot in period, the pressure rose abruptly to 3100 and had fairly well leveled off at 3300 at the end. Pulled & broke down Tester Tools. Ran in hole w/8-1/2 Dunlap w/L Core Bbl. Reamed and cleaned out from 7140'-7150'.

1-2 Cored 8-1/2" hale 7150 - 7240'.

1-3 Ron in hole with 10-5 rock bit and opened up 8-1/2" core-hole to 10-5/1" from 1091' to 7240'. Survey of 7240 @ 1º00'

Drilled 8-1/2 hole with Hughes OSC-3 rock bit 7240'- 7299'.

1-4 Drilled 8-1/2" hole 7299' - 7344'.

Ran 3rd Run Schlumberger Electrical Log and found bottom at 7339.

Recorded from 1338 to 6975. Ron Schlumberger Sidewall Sampler and recovered 10 samples from interval 7303-5488.

Installed heavy duty Rotory Toble, and put in new floor around table.

Ran in hole with Hughes 10- 1/8" OSC-3 bit and opened up 8-1/2" hole from 7240' to 7262'.

Finished opening up 8-12" hole @ 7262' - 7344'. Drilled 10-5/g" hole @ 1-5 7344 - 7425 . Survey of 7384 @ 1005

Started laying down 4-1/2" drill-pipe.

Finished laying down 4-1/2" drill-pipe. Made up string of 3-1/2" Reed 1-6 & Hydrill drill-pipe and ran in hele with 9-1/8 Hughes OSC-3 bit.

Drived 9- 1/g" hole 1425' - 1435. Hole reduced from 10-8 to 9-1/g at 1425'.

Drilled 9-1/2 hole 1435'- 7500'. Pulled out. Changed drill-pipe 1-7 rams from 4-1/2" to 3-1/2" on B.O.P. Picked up 8-1/2" Dunlap wire-line core bbl. and started measuring in hole.

L.M. Lockhart "England" 1-31

WELL HISTORY (Cont'd.)

1951

1-10

Finished measuring in hole. Corrected measurement @ 1499.

Could not break circulation to core. Pulled pipe and found inner barrel stuck in the 3-1/2 Hydrill drill-pipe. Layed down W/L core bbl.

Ran in hole with 8-1/2" Dunlop Conventional Core Barrel with rock head. Cored 8-1/2" hole @ 7499' - 7519. Core No. 33.
Pulled pipe. Depth of well 7519.

1-9 (7480'-7519') FORMATION TEST NO.3 (MIS-RUN)

Ron in hole with Johnston Formation Tester on 3-1/2" Reed drill-pipe to make Open Hole Formation Test of interval 1480'-7519'. The 9" packer stopped 50' off bottom at 1469'. Pulled J.F.T. Ron in 9-1/8 bit and reamed tight hole 1450'-7499'. Opened up 8-1/2" core-hole 7499'-7519' to 9-1/8". Circulated hole clean and conditioned mud. Pulled pipe and made up J.F.T. to test interval 1480'-7519'. Depth of Well 7519'.

FORMATION TEST No. 3-A (7480'-7519')

Ran Johnston Formation Tester on Reed 3-1/2" I. F. drill-pipe". Sutliff Hydraulic Jars & Homeo Safety Joint. Two 9" x 2-7/6" x 30" straight wall packers. Set packer at 7480' w/39' of 5-1/2" drill-collar anchor to 7519'. No water cushion used. Tester valve with 3/4" bean was opened at 2:15 AM. Packers set 2 hours, 30 minutes. Flow period 2 hrs., 15 min. Shut-in period 15 min. There was a light blow of air to surface in 1 minute, which continued in a light steady blow from 2:16 AM to 2:45 AM. At 2:45 AM, gas to surface in a light blow; gas burned with a 2-feet flame; continuous light blow of gas with weak heads from 2:45 AM to 3:45 AM. At 3:45 AM, fluid to surface, consisting of medium drilling-mud fluid flowing in regular heads. Well flowed fluid in regular heads at estimated 125 Hate from 3:45 AM to 4:30 AM. At 4:30 AM, fluid had thinned down to watery drilling fluid and muddy water, and was beginning to taste salty (estimated @ 400 9/9). Made shut-in pressure test from 4:30 AM to 4:45 AM.

Pulled tester. The Z pressure bomb charts indicated tool operated properly.

Ran in hole w/Hughes OSC bit, reamed to bottom, and drilled 9-1/8 hole @ 7519'-7586'.

- 1-11 Drilled 9-1/8" hole @ 7586'-7685' (99').
- 1-12 Drilled 9-7/8" hole @ 7685' 7775' (90').
- 1-13 Drilled 9-7, hole @ 7775' 7843' (68'). Survey at 7813' @ 1°00'.
- 1-14 Drilled 9-7/8" hole @ 7843'-7896' (53'). Survey at 7896' @ 100'.

L.M. Lockhart "England" 1-31 WELL HISTORY (Contid.)

1951

Drilled 9-7, hole 7896 - 7899 (3'). 1-15 Retary table broke down; bearing roce retainer broken. Pulled out of hole at 7:30 A.M. Dismantled and repaired rotary table. Started in hole at 10:00 P.M. with Smith 2- Cone bit.

Drilled 9-1/8 hole 1899 - 1955 (56). Smith 2-cone bit drilled from 1-16 7896" - 7930' (34') and was pulled dull , Ran in at 7930' with Reed LT Type rock bit,

Drilled 9-1/8" hole 7955' - 8107' (152'). Survey of 8107' @ 100'. 1-17

Drilled 9-1/8" hole 8107' - 8274' (167'). 1-18

Drilled 9-7," hole 8274' -8377' (103'). Survey at 8277' @ 0° 35'. 1-19

Macco mud analysis by Clem Thompson:

(Reaming to bottom at time of fest). Depth: 8280 Weight: 80-1/2 lbs/cu.ft. Viscosity: 1500/Qt. @ 130 (Mud had not been conditioned). Filtrate: 30 min. @ 10.5 c.c. water loss. Filter cake 3/32" Shear: Initial O

": 10 min. G.5

Sand Content: 4.5%.

Salt: 150 gr./gal.

NOTE: Sand content is up. Salt content is up from 20 gr./gallon

@ Jan. 5, 1951 to 150 gr./gal. today.

- Drilled 9-7," hole 8377 8442' (65'). Measured out of hole @ 8406'; used 1-20 corrected measurement @ 84/1. Re-lined brakes.
- Drilled 9-1/8 hole 8442'-8513' Mode Run No.4 @ Schlumberger Electrical 1-21 Log to 8503', & recorded 8502 - 7338', No side wall samples taken . Drilled 9-78" hole 8513'-8518'.
- Drilled 9-18" hole 8518' 8593 . Made trip & changed bits. 1-22
- Drilled 9-1/8" hale 8593' 8637', Survey of 8637' @ 1°00', 1-23
- Drilled 9- 1/8 hole 8637'-8704'. 1-24
- Drilled 9- 1/8 hole 8704 8760. 1-25

L.M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

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1951
            Drilled 9- 7/8" hole 8760' - 8795'.
 1-26
                                                           Survey of 8781' @ 1º30'
            Drilled 9-7 hole 8795' - 8833'.
 1-27
            Drilled 9- 1/8" hole 8833' - 8857'.
 1-28
            Drilled 9-1/8" hole 8857'-8909'
1-29
            Drilled 9-1/2 hole 8909'-8954'.
1-30
                                                          Survey of 8921' @ 1º45'
            Drilled 9- 1/8" hole 8954 - 8985'. Took wire-line cores in interval 8985'-8995'.
 1-31
            Cored 7- 1/8" hole 8995'- 9007'. Reamed core-hole (8985'- 9007') to 9-1/8" & drilled 9-1/8" hole 9007'- 9022'.
 2-/
            Drilled 9-1/8" hole 9022'- 9068'
2-2
2-3
            Drilled 9-1/8" hole 9068'- 9125'
            Drilled 9-7/8" hole 9125' - 9165'
2-4
                                                          Survey of 9165' @ 1º45!
            Drilled 9- 1/8" trole 9165' - 9209'
2-5
            Drilled 9-1/8" hole 9209' - 9261'.
2-6
            Drilled 9-1/8" hole 9261' - 9305'
2-7
                                                          Survey at 9305' @ 1000.
            Drilled 9-1/8" hole 9305'- 9351'
2-8
            Drilled 9- 1/8" hole 9351' - 9413'. Flow-line mud temperature @ 138.
2-9
2-10
           Drilled 9-1/8" hole 9413' - 9474'.
                                                         Eastman D. P.S.S. Survey@ 9426'@ 0°30'.
           Drilled 9-1/8 hole 9474' - 9511'. Measured out of hole: Corrected
2-11
                    Neasurement 9504'. Ran Run No. 5 @ Schlumberger Flectrical Log 8 found bottom at 9504'. Recorded from 9503' up to 8502'.
           Drilled 9-1/ hole 9504' - 9558'
2-12
           Drilled 9-1/8" hole 9558' - 9590'.
2-13
                                                           Survey at 9570 @ 1.00.
           Drilled 9-1/2 hole 9590' - 9635'
2-14.
           Drilled 9-1/8 hole 9635' - 9674'
2-15
           Drilled 9-1/2" hole 9674' - 9707'
2-16
           Drilled 9-1/8" hole 9707'-9738.
2-17
                                                         Survey at 9711 @ 1°00'
           Drilled 9-1/ hole 9738' - 9784'.
2-18
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L.M. Lockhart "England" 1-31

WELL HISTORY (Cont'd.)

1951	
2-19	Cored 7- 9 hole 9784' - 9807'. Dunlap wire-line; Hunt Bol; 7- 9 Hughes rock head
2-20	19 ¹⁰ 11 19807 - 9827 . " " " " " " " " " " " " " " " " " "
2-2/	" " 9827'-9836'. " " " " " " "
	Ran in hole w/ Hughes 7- %" rock bit & drilled @ 9836'- 9849'.
2-22	Drilled 7-5/8 hole 9849'- 9903'.
2-23	Cored 7-5/g" hole 9903'-9938'. Dunlop W/L; Hunt Bbl.; Hughes rock head.
<i>7-24</i>	" " " 9978-10,002. " " " " " " " " "
2-25	" " 10,002 - 10,011 As ABOVE. Pulled out of hole to run Schlumberger and found 7-56" rock core head bodly worn and all 4 cutters missing.
	Ran No. 6 Schlumberger Electrical Log & found bottom @ 10,008. Recorded 10,007'-9503'. Ran Mª Cullough Magnetic Fishing Tool to recover rollers from core head. Stuck tool coming out of hole at 6594'. Pulled wire-line loose and came out of hole; leaving body of Magnet, approximately 3' in length, in hole.
2-26	Installed new drilling line and measured in hole w/MS Cullough overshot. Tool would not go below 3000'; hole too tight. Pulled out & ran Security 9-1/6" Hole Opener to 6592' where top of fish located. Fried to knock magnet loose, where apparently key-seated where hole has greatest deviation of 2-1/2. Hole rough. Pulled pipe. Made up Baker Expansion Scroper with 12-1/2" blodes.
z-27	Ran in hole wiscroper and was unable to open same. Pulled out and made up new scroper. Ran in and scraped above fish and below fish to 6899. Pulled out & made up Security Hole Opener. Ran hole opener to 6600', cleaned out bridge 6600' to 6620', and reamed 9-78" hole to 7704.
2-28	Reamed 9-7/8" hole 7704' - 9784'. Opened up 7-5/" rat-hole 9784'-9835' to 9-7/8" w/ Security Hole Opener. Fish apparently dropped to bottom.
3-/	Opened 7-5% hole to 9-7% from 1835' to 9857'. Pulled out and ran back with 9-7% Hughes OSC-2 bit.
3-2	Opened 7-5/ hole to 9-7/" from 9857 to 9995. 9-7/ X 7-7/ shoulder at 9995.
3-3	Pulled out of hole and ran book with ME Cullough Socket. Fishing for

Recorded down to 10,007 with Basket & tried to pick up cones. Pulled out . No recovery - Rom in withughes 7-76" bit & record tight hole 10,000-10,007. Con-3-4 ditioned mud & pulled out. Made up 7-14" Glabs Junk Basket & ran in hale. Drilled 10,007'-10,008 w/Basket Pulled out. No recovery comes or core.

ME Cullough Magnet at 10,006'. Pulled out of hole. Recovered Magnet. Broke down ME Cullough Tools. Made up Globe Basket and ran in hole to fish for cutters from Core Bbl. head.

L. M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

1	9	51	,	

- 3-5 Serviced Basket & ran back in hole. Drilled 10,008 10,009.50 with Basket.

 Recovered 2-1/2 cones. Ran in w/ Hughes OSC 7-5/8" bit and hit junk at 10,010's.

 Found 2 pieces of junk above bit cones.
- 3-6 Drilled & worked junk, w/7-1/2" bit 10,010 10,013' and pulled out. Ron in hole w/7-1/4" Globe Junk Basket, and cored 10,013' 10,015' with Basket. Pulled Basket & recovered 1.5' hard gray Sandstone. (See Core No. 69-A). Made up 7-5/2" Dunlap Wire-Line Core Bbl. and ran in hole. Conditioned mud.
- 3-7 Cored 7-98 hale 10,015' -10,025'. Cored on junk first 5' (10,015'-10,020').
 Pulled core-bbl & ran 9-58 Hughes OSC bit. Drilled 7-58 hale 10,025-10,036'.
- 3-8 Drilled 7-5 hole 10,036' 10,085'
- 3-9 Drilled 7- 8 hole 10,085' 10,125', Ran Dunlop 7-8 Core Barrel and cared from 10,125'-10,145'. (Wire-line, rock head).
- 3-10 Cored 7-5/8 hole 10,145'-10,165'. Made trip.
- 3-11 Cored 7- 96" hole 10,165' 10,202. Circulated & conditioned hole for Electrical Log. Ran Schlumberger & checked Drillers' bottom @ 10,202'. Recorded from 10,201' up to 10,007' @ Schlumberger Run No. 7.

 Ran Schlumberger Microlog and recorded from 10,200' up to 9730'. Device did not register properly. Results N.G. Did not re-run Microlog.
- 3-12 Ran to bettom w/7-9/g" bit. Struck bridge at 10,147 and cleaned out to bottom @ 10,202'. Circulated & conditioned mud. Pulled out. Ran Homco Side wall Sampler and took side wall samples in interval 10,119' 10,088'.
- 3-13 Took Homeo side-wall samples in intervals . 10,082 10,045 & 10,177 10,124.

Ran in hole w/1- 3/8" Dunlap Core Bbl. Circulated and cleaned out 10,164 - 10,202 (bottom). Circulated, added new mud, and conditioned hale for formation test. Pulled pipe. Depth of well @ 10,202'. To make open hole formation test in 7-5/8" rat-hole of interval @ 10,142' - 10,202'.

3-14 <u>FORMATION TEST No. 4</u> (10,142'-10,202')

Ran Johnston Formation Tester on Read 3-1/2" I.F. drill-pipe. 4-1/2" Sutliff Hydraulic Jars & 4-1/2" Homeo Safety Joint. Two 7" x 2-7/6" x 30" straight wall packers set at 10,133' & 10,142' with 60' of 4-1/4" drill collor anchor to 10,202'. Used 1200' of fresh water custion. Tester valve with 1/2" bean was opened at 11:14 AM and remained open I hour. There was an immediate weak steady blow decreasing to dead in 9 minutes @ 11:23 AM. Dead for 5 minutes. At 11:28 AM, a week steady blow of air again, increasing to a fair steady blow at 11:35 AM. From 11:35 AM to 12:14 PM, a fair blow with long heads. No gas to surface. Rocovered 240 net rise of medium, gassy drilling fluid; no free water. The 2 pressure bomb aborts indicated tool operated properly.

L.M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

1951

3-15 Ran in w/ Dunlap 7-5/8 wire-line core-bbl. and cored interval 10,202'- 10,253'.

3-16 Cored 7-5/8" hole @ 10,253' - 10,297'. Conditioned mud & hole for Formation test of interval 10,202' - 10,297'. Pulled pipe.

3-/7

FORMATION TEST No.5 (10,202'-10,297')

Ran Johnston Formation Tester on 3-1/2" full-hole D.P. 4/2" Sutliff Hydraulic jars & 4-1/2" Homeo Safety Joint. 1300' of fresh-Hoter cushion. Set two 7" x 2-7/6" x 30" Straight wall packers at 10,193' & 10, 202' with 95' of anchor to bottom @ 10,297'. Tester valve with 1/4" bean on bottom was opened at 7:42 MM. There was a medium, steady blow for 5 minutes; then fluid began drapping in annulus as packer started to leak. Attempted to re-set packer during which time (7:47 MM to 7:50 MM) fluid went away at an increased rate; may have opened equalizing valve in this operation. At 7:50 AM closed shut-in valve to take B.H. closed-in pressure. Let stand 5 minutes. At 7:55 AM opened equalizing valve; and then pulled packers loose, requiring a 160 ton pull. Charts indicated a 5 minute flow period with a pressure rise to 950 during that interval. (100 * p. @ water cushion indicated an charts.) Packers may have been set in fractured rock and fluid leaked around packers thru fractures.

Recovered a net rise of 660 of very gas-cut fluffy oily mud. Gas bubbled and furned at top of fluid and blew mud fluid out of drill-pipe, cleaning out 1-1/2 to 2 stands at a time. No free or salt water in net rise in drill-pipe or in tool.

Ran in hole with 7-5/8" Dunlap wireline core-bbl. Conditioned mud.

3-18 Cored 7-5/ hole @ 10,297' - 10,342'

3-19 Cored 7-5/8" hole @ 10,342'-10,357'. TOTAL DEPTH OF WELL @ 10,357'. Conditioned mud and hole. Pulled out. Tested B.O.P. -OK. To make open-hole fermation test of interval 10,297'-10,357' in 7-5/6" rat-hole.

FORMATION TEST No. 6 (10, 297'-10, 357')

Ran Johnston Formation Tester on 3-1/2 F.H. drill-pipe, equipped as above. 1500 fresh-water cushion. Set double straight hole packer at 10,297 & 10,288, with 60 of 4-1/4 drill-collar anchor to bettem at 10,357. Tester valve with 1/2 been was opened at 6:05 PM & remained open I hour. There was a medium steady blow for 13 minutes, then dead for 5 min., then a light steady blow for remainder of test. Closed valve at 7:05 PM and took shur-in pressure for 10 minutes. Packers set I hour, 10 min. Recovered 4-1/2 stands (405) net rise of gas-cut drilling fluid. Medium salty taste; tested properly and did not plug.

L.M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

1951

3-20 Ran to bottom w/7-5/g" bit. Circulated and conditioned mud for Electrical Log. Salinity of mud @ 50 grains per gallon.

Made Schlumberger Electrical Log Run No.8. Recorded from 10,359' to 9,960' (See Field Print).
Total Depth of Well @ Schlumberger 10,360'.
"" " Driller 10,357'.

Started back in hole wopen-end drill-pipe to place coment plug in bottom.

- Ran open and drill-pipe to 10,297'. Circulated & conditioned mud for plug job. With open-and drill-pipe hanging at 10,286' Inixed and pumped in 50 sax Permanente Hi-Temp. Coment, using 50 cu.ft. Water ahead and 10 cu.ft. water behind. Displaced cement with 420 cu.ft. of drilling fluid. Halliburton Power Equipment. Job completed at 10:00 AM. Pulled out of hole. Ran in hole width-collar and Hughes 7-78" OSC rock bit. After 12 hours felt for plug with bit at 10:00 PM. Found cement stringers at 10,123'; took 2 to 3 tons weight. Found set cement at 10,135'; took 6 tons weight.
- Icamation Test No. 7 (10,034-10,135') Mis-Run

 Circulated & conditioned mud from 10' above plug for open-hole formation test in 7-5," rat-hole from 10,034' to top of cement plug at 10,135'.

 Ran Johnston Taster on 3-1/2" F.H. drill-pipe. 1200' fresh-water cushion.

 Used double straight hole packer with bottom of packer at 10,034'. 101' of anchor to 10,135'. Tried to set packer at 10,034'. Dropped bar to open valve and cement plug gave way when valve opened. Packer slid down hole & would not hold. Pulled tester.
- 3-23 Ran in hole widrill-pipe & 7-7 bit & cleaned out coment from 10,129' to 10,203'. Circulated and conditioned mud & hole for another plug job. Pulled pipe.

 With open and drill-pipe hanging at 10,203', pumped in and displaced 25 sax modified coment with Halliburton Power Equipment. Coment in place 3:00 P.M. Standing comented.
- 3-24 Ran in hole with two 5-74" drill-collars & 7-76" Hughes OSC rock bit. At 3:00 AM felt for plug. Found cement at 10,140" which pumped away. Cleaned out to 10,150'. At 7:00 P.M. Set weight on cement plug at 10,150'. Held 25,000#.

WELL HISTORY (CONT'd.)

1	4	5	1
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- 3-18 In hole w/9-18" bit. Reamed fight hole 7450' 7709'.
 Reamed 9-78" hole to 8372'.
- 3-29 Reamed tight 9-1/g" hole 8372'-8491'. Opened up 7-5/g" hole from 9995' to 10,033'. Circulated & conditioned mud to run 5-1/2" casing.
 - Ran 231 Joints 5-1/2" Casing as follows:

1966' OF 20 # N-80 8TR on Bottom.

8076' OF 17 # J-55 8 TR including 1 Jt. 20 # N-80 on top.

10,047' = Total Pipe on Hook with shoe at 10,038'.

Float Collar at 9993'

- 3-30 Cemented with 300 sax Permanente Modified Cement.

 Mixing Time 16 minutes. Used 2 Top Rubber plugs.

 Displaced with 1293 cubic feet drilling fluid. Displaced 93 cubic feet over normal computed displacement.

 Displacement time 39 minutes. Final Pressure 500 .

 Job completed 1:45 AM, 3-30-51. Halliburton Power Equipment and Bulk Cement. Casing Centralizing Guides were set at 10,029.50, 10,008.80', and 9992.00'.
- 3-31 Standing Contd. Landed 5-1/2" csg. Installed B.O.P.
- 4-1 Laying down 3-1/2" drill-pipe. Making up 2-3/8" tubing.
- 4-2 Ran in hole with 4-1/2" Hughes Tricone Bit on 2-3/8" fbg. Brake circ. at 3900', 6400', & 7400'. Found rubber plugs at 9992'. Drilled out plugs and F.G. to 9994'. Drilled out cement to 10,030'.

 Tested casing & B.O.P. with 800# for 15 minutes. OK.
- 4-3 Shot 4-3/ holes at 10,017' in 5-1/2" esg. w/M=Cullough 3-1/2" Mech. Gun Perforator for W.S.O. Test.

W.S.O. TEST: Ran Johnston Formation Tester on 2-3/8" tubing with 1395' of fresh-water cushion. Packer was set at 9947' w/tailpiece to 9964. Tester valve with 1/2" bean was opened at 7:29 AM and remained open I hour. There was a light steady blow for 16 minutes, and then light heads for the remainder of test. Recovered a net rise of 3099' of gassy drilling fluid. Fluid was very gassy and would occasionally unload, blowing 60 to 70 feet into the air. The pressure bomb charts indicated the tester valve was open during the entire test. Water shut-off test was witnessed and approved by Mr. G.W. Hunter of the Division of Oil & Gas, Coalingo.

L.M. Lockhart "England" 1-31

WELL HISTORY (Cont'd.)

1951

- 1-3 (Cont'd.) Ran in hole w/1-1/2" Hughes Tricone rock bit on 2-3/6" they found top emt. at 10,079'. Drilled out emt. to shoe found at 10,038'. Z' of emt. below shoe. Cleaned out to top of cornent plug (new bottom) which was located at 10,169. (irculated & conditioned mud.
 - 1-4 Circ. & conditioned mud midnight to 8:00 A.M. Ran 2-3/6 tog. & landed shoe at 10,020'. Removed B.O.P. and installed X-mas tree. Changed mud to fresh water. Circulated well with fresh water.
 - 4-5 Swabbed well beginning at 10:00 A.M. At 5:00 P.M. swabbing from 5960; fluid level 4760; no fluid rise.

 Removed X-mas tree; flanged up B.O.P.; checked open
 hole to bettom witubing OK. Removed B.O.P. and installed
 X-mas tree. Swabbing.
 - 4-6 Swabbed from midnight to 9:30 A.M. when fluid level 4474' & swabbing from 5474'. Removed X-mas tree & flanged up B.O.P. Changed water to mud.

Hung open-end they at 10,167'. Mixed and pumped in 50 sax modified coment. Displaced with 214' cu.ft. drilling fluid. Top of plug approx. 9880'. Job completed 7:30 P.M. by Halliburton Comenters.

4-7 Left 5-1/2" casing in place as comented with Bradenhead level with top of cellar.

Hole filled w/heavy drilling fluid from 9880 to surface.

- 4-12-51 Bolted steel plate over top of casing at surface. Suspended well in above condition.
- 2-21-52 Plugged top 10' of casing with coment.
 Welded steel plate over top of casing.
 10-11-52 Well is abondoned.

L.M. Lockhart "England" 1-31 WELL HISTORY (Cont'd.)

1951

3-25 FORMATION TEST No. 8 (10,049 - 10,150') MIS-RUN

Ran Johnston Formation Tester on 3.1." I.H. drill-pipe to make open hole test in 7-36" rat-hole. 1200' fiesh-water cushion. I side-wall packers at 10,040' & 10,049' with 101' of D.C. anchor to top of Gritplug at 10,150'. Packers failed to hold.

FORMATION TEST No. 9 (10,041'-10,150') MIS-RUN

Ron J.F.T. as obove. 1200' fresh water cushion. 2 side wall packers at 10,032' & 10,041' with 109' of D.C. anchor to top of cement plug at 10,150'. Plug slid down to 10,166'; then packers failed to hold.

3-26 Ron in hole w/7-9/" bit to 10,166'. Conditioned mud & hole: —
Mud Weight 85-88#. Viscosity Go-75 seconds.
Sand Content 2%. Water Loss 8 c.c. Coke Thickness 2/32.

FORMATION TEST NO. 10 (10,013'-10,166') MIS-RUN

Ran J.F.T. on 3-1/2" D.P. 1200' fresh-water cushion. 2 side-wall packers at 10,004' & 10,013' with 153' of D.C. anchor to top of cmt. plug at 10,166'. Packers failed to hold. Pulled tester.

3-27 Ran in hole w/7-5/8" bit & conditioned mud to 85# 8 50 Vis.

Measured in and found top of cement plug at 10,163' Corr. Meas.

FORMATION TEST NO. 11 (10,002'-10,163') MIS-RUN

Ran J.F.T. on 3-1/2" D.P. 1/2" bean. 1200' fresh water cushion. 2 side-wall packers at 9993' & 10,002' with 161' of D.C. anchor to top of cement plug at 10,163' (Corrected Measure ment). Fluid dropped in annulus. Packers would not hold.

L.M. LOCKHART

Core #7 6170-6180

Core #8 6180-6190

101

9t

Rec. 10'

Rec. 91

Shale, same.

Shale, same.

"England" #1-31

Section 31-14S/13E (MDBM)
Panoche Greek-Cheney Ranch Area

Location: 660' S. and 660' E. of center of Section

Elevation: 419 (K.B.)

CORE DESCRIPTION

Core #1 3597-3615 Rec. 19' 191 Siltstone, medium brown, hard, weathers to crumbly, medium gray pokerchip shale, rough hackly fracture, massive, rare light brown inclusions, indicating +6° dips, common forams, Dentalina, et al, scattered fish scales, rare echinoid spines, no petroleum shows. Core #2 Missing. 3615-4774 Core #3 4774-4787 Rec. 21 6" Sandstone, medium gray, fine grained, massive, very hard, cemented, very common micas, tight, no petroleum shows. 116" Silt, light-medium gray, very coarse, massive, very soft, friable, micro-micaceous, scattered larger crenulated biotite, very poor porosity and permeability, no petroleum shows. 4787-6140 Core gap - drilled. Core #h 6140-6150 21 Sand, very light grey, fine grained, very silty, kaolinitic, massive, firm-friable, fairly poor porosity and permeability, no petroleum 31 Shale, medium to dark brownish grey, soft, very brittle and easily fragmented into wafer thin fragments, very silty, rare pyrite, forams. Core #5 6150-6160 Rec. 10 6ª Sand, as in last core but mixed with drilling mud. 916H Shale, as in base last core, rare well preserved plant remains, local numerous large forams, Siphogenerinoides, scattered small forams, one possible ostracod valve. Core #6 6160-6170 101 Shale, same, with rare 3"-4" Sand (same) streak with rare 57° dipping calcite veins. Sand is friable, very light to light grey with brownish cast, no petroleum shows, poor porosity and permeability.

L.M. Lockhart - "England" #1

Core #9 6190-6200

Rec. 10'
Shale, similar to above, medium-dark brown to brownish grey, platy
to locally wafer parting, floods of large forams (7), local common
Dentalina to nearly 1/2" long, scattered large fish scales and remains,
rare sandy streaks showing 4" dips.

Gore #10 6200-6202

Rec. 1' Shale, same,

6202-7091

Drilled interval, core gap.

Core #11 7091-7096

Rec. Frags.
Fragments Sand, light grey, scattered medium, friable, very silty, scattered biotite, poor porosity and permer bility, no petroleum shows.

Core #12 7096-7106

Sand, medium to light grey, firmly friable to hard, fine grained, fair sorting, local scattered medium and rare coarse grains, silty, massive, fairly poor sorting, sub-angular grains, quartzose, scattered credulated biotite, rare pyrite, fairly low porosity and permeability, no petroleum shows.

Core #13 7106-7116

Sand, medium grey, fine with scattered medium grained, very silty, difficultly friable to firm-friable, massive with local interbeds of siltstone, dark grey, biscuit parting, to 5° poor dips, common forams, hard, poor porosity and permeability, no odor, stain or cut.

Core #14 7116-7124 8'

Rec. 8' Sand, as above.

Core #15 7124-7129 5'

Rec, 5' Sand, same.

Core #16 7129-7134

51

Rec, 5!

Sand, same, becoming friable, kaolinitic, very poor porosity and permeability.

Core #17 7134-7139

Rec. 6' Sand, same.

Core #18 7139-7144

61

Rec. 6 Sand, same, friable to hard, local very carbonaceous streaks with fairly good 10 dips, no shows.

Core #19 7144-7150

Rec. 6'
Sand, same, with local interbeds to l' of siltstone, as above, fair 5° dips, no shows.

7230-7240

and arenaceous forams.

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ore #20
  7150-7155
                Missing.
  Core #21
  7155-7160
                Rec. 51
        51.
                Sand, same, no siltstone, no shows.
  Core #22
  7160-7165
               Rec. 31
      31
               Ditto.
  Core #23
  7165-7170
               Kec. 31
      3'
               Ditto.
  Core #24
  7170-7175
               Rec. 5
      51
               Ditto.
  Core #25
  7175-7180
               Rec. 231
      21
               Mitto, becoming slightly coarser grained and cleaner, fairly poor
               porosity and permeability.
 Core #26
 7180-7185
               Rec. 51
      51
               Sand, same as cores above - Core #26 (7180-7185)
 Core #27
 7185-7195
              Rec. 10
     101
              Sand, same, with rare interbeds of very hard carbonaceous siltstone,
              dirty dark brown to black, fracture surfaces show 80% of surface =
              carbonaceous fragments to 3/8" rounded and to 13" elongate fragments
              with matrix of sandy silt, cemented, massive, scattered to locally
              abundant micro-micaceous, Sand = very low porosity and permeability,
 Core #28
 7195-7205
              Rec. 10'
    101
              Sand, as in above cores, rare streaks of siltstone, dark grey, massive,
              dipping 6-8°; becoming very kaolinitic and altered biotite, very poor
              porosity and permeability, no shows.
 Core #29
7205-7215
             Rec. 71
    71
             Sand, same, local biscuit parting.
Core #30
7215-7220
             Rec. 61
   14'
             Sandstone Shell.
   43.
             Sand, same.
Core #31
7220-30
             Rec. 11'
   111
             Sand, same with local interbeds and laminations of siltstone, dark
             gray, micro-micaceous, dips very wavy, nearly flat, no shows.
Core #32
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Sand and Silt interbeds, same, Siltstone locally slows common fish scales

7240-7499 Core gap - drilled.

Core #33

7499-7519 Rec. 61 Sand. 1

Sand, light grey, medium and fine grained, difficultly friable to local hard, massive, broken, silty, fairly poor sorting, sub-angular grains, scattered biotite and green grains, rare small clot dark brown petroleum residue, fairly tight, no odor, stain or cut.

Cores #34 & #35 - Missing.

Core #36 8995-8997

Rec. Frags.

Fragments Sand, light grey, very fine, very firm, silty, well sorted, fairly tight and siltstone, medium grey.

Gore #37

8997-9002 Rec. 31

1' Sand, as last core.

2' Siltstone, as last core, medium grey, hard, fragmented, rare forame?

Core #38

9002-9007 Rec. Frags.

Fragments Siltstone, same.

Core #39 9007-9787

787 Missing.

Core #40

9787-9793 Rec. Fragments

Fragments Siltstone, dark grey, very hard, locally very fine sandy, wavy laminations.

Cores #41 thru #44 - Missing.

Core #45

31

9810-9813 Rec. 31

Laminated Sand, stone light grey, very fine grained, nearly silt, finely laminated with nearly black carbonaceous material, wavy dips give 0° to 5° dips, very hard, very tight, no shows.

Core #46

9813-9816 Rec. 3'

3' Laminated Sandstone, same, dips nearly flat to locally nearly 20°, tight.

Core #47

9816-9821 Missing.

Core #48

9821-9827 Rec. 31

3' Siltstone, dark gray, massive with local wavy laminations the, very hard to locally crumbly.

Core #49

9827-9830 Rec. 21

2. Siltstone, same, laminations are very fine sand, light grey, as in Cores #45 & #46.

51

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Core #50
9830-9836
            Rec. 5'
   51
            Ditto.
Cores #51 & #52
                   Missing
Core #53
9912-9915
            Kec. 1
    11
            Sand, light to medium grey, fine with scattered medium, silty, massive,
            local thin beds siltstone as above, tight.
Core 454
            Missing.
Core #55
9920-9925
            Rec. 1'
    11
            Sand, medium grey, fine and scattered medium, massive, difficultly
            friable to hard, very common biotite crenulated, rare white muscovite.
            fairly poor sorting, sub-angular grains, silty, tight, no shows.
Core #56
9925-9930
            Rec. 21
    21
            Sand, same.
Core #57
            Missing.
Core #58
9935-9938
            Rec. 21
    21
            Sand, same.
Core #59
9938-9940
            Rec. 1'
    1'
            Sand, same but friable.
Core #60
9940-9946
            Rec. 61
    61
            Sand, same, but very fine grained and fine, firm-friable to hard, locally
            very common crenulated biotite, rare streaks dark brown siltstone, tight.
Core #61
9946-9956
            Rec. 4'
    F.
            Siltstone, dark grey, hard, brittle, massive, scattered brown biotite,
            rare streaks light grey sand as above, dips nearly flat.
Core #62
9956-61
            Rec. 3'
   31
            Sand, as above cores with rare streaks siltstone.
Core #63
            Missing.
Core #64
9966-9971
            Rec. 5'
    51
            Sand, same.
Core #65
            Missing.
Core #66
<del>9978-9988</del>
            Rec. 5
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Sand, similar to above, medium grey, fine with medium grains, difficultly friable to hard, massive with rare wavy nondiagnostic dip, very biotite,

tight, locally somewhat cemented, no shows.

Core #67

9988-9998

1'

Sand, same, one silty streak gives poor 4-8° dip.

Gore #68

9998-10,008 Rec. h'

Siltstone, dark grey, very hard, locally sandy, very gilsonitic locally, rare amber material, locally very wavy streaks of light grey coarse siltstone, dips very poor +8-10° - locally interbedded with sand, medium grey, fine with scattered medium, very firm to hard, somewhat silty, massive, very common biotite, very low porosity and permeability, no petroleum shows.

Core #69
10008-10011 Rec. frags.
Sand and Siltstone, as above.

Core #70 Missing.

Core #71
10020-10025 Rec. 1'
1' Siltstone, medium grey, hard, dense, with rare fragments sand, same as Core #68.

10025-10125 Core gap - drilled.

Core #72 10125-10130 Rec. 3' 3' Sand, as above but hard, nearly tight.

Core #73 10130-10135 Rec. 5' 5' Sand, same.

Core #74

10135-10145 Rec. 3'

Sand, same but locally difficultly friable, interbedded locally with silt, same.

Core #75

10145-10150 Rec. 3'

Sandstone, as above but very hard, cemented, tight, core flashed for 3 seconds, one foot flash.

Core #76 10150-10155 Rec. 3' 3' Sand, same.

Core #77

10155-10165 Rec. 8'

8' Sand, same but not cemented, very poor porosity and permeability with local interbeds of siltstone, dark grey - (see above). 10" flash 4 sec. burn.

Core #78

10165-10175 Rec. 2'

Laminated Sand and Silt, same, but tight.

Core #79
10175-10182 Rec. 1*
Ditto, tight, 25 sec. 2' flash, poor 5° dips.

Core #91

Core #80 10182-10187 Jand, medium gray, fine grained with scattered medium, fairly poor 31 sorting, sub-angular grains, massive, hard, very common crenulated biotite, rare beds siltstone, dark gray, hard, massive, very fine abundant micro-micaceous, no petroleum shows except good flash. Core #81 10187-10197 Rec. 31 31 Sand, same, with local siltstone streaks, same, good dips = 5°, rare clots siltstone, same, good 15 sec. Flash, no other shows. Core #82 10197-10202 Rec. 3' 31 Sand and Silt, same, no flash, one yellow stain at bottom of core. Cores #83, 84 - Missing. Core #85 10217-10218 Rec. 1' Siltstone, dark grey, very hard, massive, very micro-micaceous, local 1' sand grains, good 15 second flash. Core #86 10218-10223 Rec. 451 79, Siltstone, same, no flash. Core #87 10223-10232 Rec. 8 1' Sand, light grey to medium brown where very biotitic, silty, very fine grained, locally approaching silt, hard, massive but locally very wavy, dips average about 10°, hard, difficultly friable, kaolinitic, very poor porosity and permeability. 4 Siltstone, as above cores, local 10° partings. 1. Siltstone, light grey, coarse, approaches very fine sand, kaolinitic, hard to difficultly friable, very biotitic, local scattered pink and green grains, tight, no odor, stain or cut. 21 Siltstone, same as h! above, no flash. Core #88 10232-10242 Rec. 81 8. Interbedded dark grey siltstone and light grey coarse siltstone to very silty sand, very kaolinitic, local dips appear fair, to 8°, locally core is very carbonaceous, locally clotted light and dark gray silt. Bottles containing very fine silty sand, same, at 10234, 10236 and 10240, no odors, 15 sec. flash, no petroleum odor or stain. Core #89 10242-10252 Rec. 51 51 Ditto, as above, one bottle of fine silty sand from 10251, no odor, 25 sec. flash, no petroleum odors or stain. Core #90 10252-10253 Rec. 2' (Pickup ?) 21 Sandstone, light-medium gray, fine grained, comented, massive, very hard, 10 sec. flash.

10253-10258 Rec. 1'
1' Siltstone, dark gray, local carbonaceous, micro-micaceous, hard, massive.

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Core #92
10258-10264
              Rec. 2'
    21
              Sand, with local beds silts one, same as Core #68 (10232-42).
              no flash.
Core #93
10264-10274
             Rec. L'
    · 41
              Sand, same, flashed.
Core #94
10274-10279
             Rec. 1'
     1"
              Sand, same.
Core #95
10279-10289
             Rec. 5'
      51
             Vitto.
Core #96
10289-10297
             Rec. 1'
      1'
             Ditto.
Core # 97
10297-10302
             Rec. frags.
             Sand, same.
Core #98
             Missing.
Core #99
10307-10309
             Rec. frags.
             Di tto.
Core #100
10309-10317
             Hec. 3'
      31
            Ditto.
Core #101
10317-10327
             Rec. 6"
     6n
             Vitto.
Core #102
10327-10332
             Rec. 1"
    1"
             Nubbins, ditto.
Core #103
10332-10342
             Rec. 31
     31
             Ditto, with rare beds siltstone, same.
Core #104
10342-10352
             Rec. 61
      61
             Sand, ditto, with interbeds of Siltstone, same, light 10 sec. flash.
Core #105
10352-10357
             Rec. 2'
    21
             Siltstone, with rare beds light greyish silt, 20 sec. flash, bottled
             streak sand at bottom Core #105 in bottle (10357), no odor.
```

HOMCO SIDEWALL SAMPLES

(No petroleum shows unless otherwise indicated)

#11	10,045	R. 3" fine gray silty sand, no odor.
#10 ·	10,059	Rec. 3" Ditto
#9	10,064	Rec. 5" fine, silty, medium grey sand, good kerosene odor, no apparent stain.
#8	10,070	Rec. 3" fine silty medium grey sand, no odor.
#7	10,075	Rec. 2gm Ditto.
#6	10,082	Rec. 3" Ditto.
#5	10,088	Rec. 3" Ditto, sand, hard, very tight.
#14	10,096	Rec. 3" Ditto, as above.
#3	10,100	Rec. 22 Sand, fine medium grey, name, no odor.
#2	10,115	Rec. 3" Sand, same.
#1	10,119	Rec. 3" Sand, same.
A-3	10,124	Rec. 5" Sand, same, fair Kerosene odor.
A-2	10,143	Rec. 3" Ditto, faint kerosene to light petroleum odor.
A-1	10,177	Rec. 5" Sand, same, faint to doubtful odor.

SCHLUMBERGER SIDEWALL SAMPLES

- 2695 Rec. 2" silty clayey Sand, medium green, no petroleum odor.
- 2732 Silty Sand, very fine grained, light-medium green, well sorted, pebbly, firm, very low porosity and permeability, no shows.
- 2737 Ditto, last above.
- 2778 Silty Sand, greenish, mixed with limonitic brown silt.
- 3200 Siltstone, medium grey, firm-friable.
- 3225 Siltstone, medium brown.
- 4304 Sand, light grey, fine grained, scattered rounded coarse, very friable, fair porosity and permeability, silty, no odor.
- 4330 Siltstone, light greenish grey, massive.
- 4508 Medium-dark green glauconite Siltatone, very fine grained.
- 1735 Medium-dark green glauconite Sand, fine-grained.
- 4831 Medium gray Siltstone, friable, very abundant altered biotite.
- 4832 Ditto, as above, but slightly coarser grained.
- 4896 Siltstone, medium grey, friable.
- 5140 Siltstone, light grey, otherwise as above.
- 5165 Ditto very common biotite.
- 5350 Sand, light grey, silty, fine grained, low porosity and permeability, firm-friable.
- 5486 Rec. 2" Silty Sand, light grey, very fine grained, no odor.
- 7050 Rec. 1" Silty Sand, same, no odor.
- 7059 Rec. 1" Ditto.
- 7245 Rec. 1" Ditto.
- 7255 Sample gone
- 7269 Rec. 12" Ditto.
- 7285 Rec. 1" Sand, light grey, very kaolinitic, no odor.
- 7296 Rec. 1" Sand, as last above.
- 7299 Rec. lan Ditto.
- 7303 Rec. 3" Ditto.

DIVISION OF OIL AND GAS

REPORT ON PROPOSED OPERATIONS

				• •	No. P 552-3	808
		Coalinga	Calif	October	141	<u>52</u>
Mr. M. H. Fuller			-			
Box 165, Burrel,		Calif.				
Agent for L. M. L	OCKHART					
Dear Sir:						
Your	proposal to	abandon	Well	No. "Engla	md" 1-31	,
Section 31 , T. 14S., R. 13E.	М.D. B. & M.,		Field,	Fres	no Co	ounty,
dated August 9, 19 52, received 0	ctober 9 ₁₉ 52	, has been examined	in conjuncti	on with recor	ds filed in this	office.
Present conditions as shown b	y the records and tl	he proposal are as fo	llows:			
RECORDS IN ADDITION TO OR 5-1/2" cem. 10,038', four	_			NOTICE:		
THE NOTICE STATES: "The present condition of l. Complete casing real 47.54# New States" 14" 47.54# New States 10" 20" 10" 10" 10" 10" 10" 10" 10" 10" 10" 1	cord. mls. SJ Casin & 17# J-55 N 357'. Production with cement f with cement f of the zone 7'. g is in place the cellar. asing is plug of same.	g cmtd. to surew Smls. Csg. rom bottom @ rom 10,169' u tested and the as cemented, ged with 10'	cmtd. w/ 10,357' u p to appr e W.S.O. with the	p to 10,1 oximately holes in bradenhe	69'. 9880', whether 5-1/2" ead about 1	nich ! Level
PROPOSAL: "The proposed work is as We propose to abandon		e condition."				
DECISION: THE PROPOSAL IS APPROVED	•					
Bond No. 965734						

R. D. BUSH

State Oil and Gas Supervisor

....Deputy

Orig: Company, L.A. cc: Mr M H Fuller

DIVISION OF OIL AND GAS

ULT 0 - 1952

Notice of Intention to Abandon Well

COALLIA, CALLIANA

This notice must b	e given at least five days before wor	rk is to begin; one copy only	
•	LOS ANGELES	Calif. AUGUST	J

DIVISION OF OIL AND GAS		
COALINGA	Calif.	
In compliance with Secs. 3228, 32	229, 3230, 3231 and 3232, Ch. 93, Stat. 1939, notice is hereby	given
that it is our intention to abandon well No.	ENGLAND" 1-3/	-
	D. B. & M. PANOCHE CREEK AREA	Field,
FRESNO	County, commencing work on the 10 TH	da y
of APRIL		
The present condition of the well is as follows:		
1. Complete casing record.		
14" 47.54 # NEW SMLS. S. S. SAX AT 609'.	SJ CASING CMTD. TO SURFACE W/TOO	
5-1/2" ZO# N-80 & 17# J-5:	5 NEW SMLS. CSG. CMTD. W/200 SAX	٢
TOTAL DEPTH 10, 357.		
2. Last produced.	No PRODUCTION	
Date	Net oil Gravity Cut	
The proposed work is as follows:		
2 6 111 6 1 1	a *	

3. Condition of hole;

HOLE IS PLUGGED WITH CEMENT FROM BOTTOM @ 10,357 UP TO 10.169'

HOLE IS PLUGGED WITH CEMENT FROM 10,169' UP TO APPROXIMATELY 9880', WHICH CEMENTS OFF ALL OF THE ZONE TESTED AND THE W.S.O. HOLES IN THE 5-1/2" CASING AT 10,017.

THE 5-1/2" CASING IS IN PLACE AS CEMENTED, WITH THE BRADENHEAD ABOUT LEVEL WITH THE TOP OF THE CELLAR.

THE TOP OF THE CASING IS PLUGGED WITH 10' OF GEMENT, AND A STEEL PLATE WELDED OVER TOP OF SAME.

ALL UNPLUGGED PORTIONS OF HOLE ARE FILLED WITH HEAVY DRILLING FLUID.

4. WE PROPOSE TO ABANDON WELL IN ABOVE CONDITION.

.M. LOCKHART To is file of dat

DIVISION OF OIL AND GAS

REPORT ON PROPOSED OPERATIONS

			No. P	5-9122
	Coalinga,	Calif	April 12,	₁₉ 51
MR. M. H. Fuller	-			
Box 165, Burrel, Ca	lif.			
Agent for L. M. LOCKHANT				
DEAR SIR:			, p	
Your supplementary proposal to	drill	Well	No."England" 1	-31
Section 31, T. 14S., R. 13E., M.D.B. & M.,	*** 70 fit els 24	Field,	Fresno	County,
dated April 10,19 51, received April 12,19 51,	has been examined	l in conjunct	ion with records filed	in this office.
Present conditions as shown by the records and the THE NOTICE STATES: "The new conditions are as follows: Hole plugged from bottom > 10,357' 5-1/2" casing cemented at 10,038' w W.S.O. test made through 4 - 3/8" h Oil and gas shows between 10,038' a drilling fluid and circulating w Results inconclusive."	up to 10,169 with 300 sax noles shot at)'. cement. t 10,017'	ed by displaci	ng the
PROPOSAL: "We now propose To plug with cement from 10,169' up of zone tested and cover the W.S. To leave the 5-1/2" casing in place 2' below top of cellar and with a To leave hole full of drilling mud To suspend well in above condition.	0. holes in as cemented steel plate from 10,000	the 5-1/ 1,with the bolted	2" casing at 1 e Bradenhead a over top of sa	0,017*. bout
DECISION: THE PROPOSAL IS APPROVED.				

Bond No. 965734

GGP:ef

Orig: Company, L.A. ec: Mr. M. H. Fuller

R. D. BUSH

State Oil and Gas Supervisor

_Deputy

DIVISION OF OIL AND GAS

Supplementary Notice

	Los Angeles	Calif. Apri	11 10 ₁₉ 51
		· · ·	
DIVISION OF OIL AND GAS			
Coalinga,	Calif.		
Our notice to you dated	March 28	, 19. 51 , stati	ing our intention to
Coment 5-1/2" casing (Drill, deepen, redrill, abandon)	in well No.	"England# 1-31	
Sec. 31 , T. 14S , R. 13E ,	M • D • B. & M.	Panoche Area	Tala,
Fresno	County, mu	ast be amended on account of	changed or recently
discovered conditions.			
The new conditions are as follows:			
drilling fluid and circulat Results inconclusive.			
We now propose			
To plug with cement from 10,1 of zone tested and cover the To leave the 5-1/2" casing in 2' below top of cellar and	e W.S.O. holes in n place as cement	the 5-1/2" casing a	t 10,017.
To leave hole full of drillin	g mud from 10,000	· to surlage.	Allan on on walter
To suspend well in above cond	ition.	3	RECOUVED.
			APR 12 1955
CONTRACTOR OF SERVICE			
Santa and Santa	ा है। विक्रम	L. M. LOCKHART	
The second secon	By	Name of Operator)	asl
9766 9-48 8M SPO		Engineer	<u> </u>

DIVISION OF OIL AND GAS

Report on Test of Water Shut-off (FORMATION TESTER)

No. T 5-5435

	Coalinga,	_Calif	April	9,	19 51
Mr. M. H. Fuller	·				
Box 165, Burrel, Calif.					
Agent for L. M. LOCKHART					
DEAR SIR:					
Your well No. "England" 1-31	, Sec. 31 , T. 14	: S.,	R. 13 E.	, MD	•B & M.
Field, in	Fresno	C	County, was 1	ested for w	vater shut-off
on April 3 , 19 51 Mr. G.	W. Hunter		, desig	nated by tl	he supervisor,
was present as prescribed in Secs. 3222 and 3223, Ch. 93	, Stat. 1939; there were al	so present	13 G 1 3 G	CLALACT 4	トン・メナノリカ
	and Ole	MIN 12.	sarı, sin	Tueer.	10 050 4
Shut-off data: 5-1/2 in 12 & 20 lb. casing was on March 30 , 1951 in	s cemented	1 • 1	300	at:	10:000 ft.
on	in, ho	ble with	13.70	sac	ks of cement
Casing record of well: 14" cem. 609; 5-1/2"	cem. 10,038', fo	our 3/8	" holes	10,017	art in casing.
	(10,038 (10,03	50			
Present depth 10, 357 ft. Bridged with cement from	(10,357 ft. to 10,16	3 ft. (leaned out t	0.10,03	oft. for test.
A pressure of 1000 lb. was applied to the inside of o	easing for 15 min.	without lo	ss after clea	ning out to	10,030 ft.
A Johnston	tester was run into the	hole on	2 - 3/8	in.7dÆill	Kpipe-tubing,
with 1395 ft. of water-mudicushion, and	packer set at 9947	ft. v	ith tailpiece	to99	64 ft.
Tester valve, with 1/2 in. bean, was opened	lat 7:29 a.m.				and remained
open forhr. andmin. During th	is interval thore was	i a lig	ht stead	y blow	for 16
minutes and then a light heading blo	w for the remaind	er of	the test	В	
THE IMSPECTOR WAS PRESENT AT THE URL REPORTED:	J, FROM 11:00 a.m.	TO 12	:15 p.m.	AND MR	. HARL

- 1. The 5-1/2" casing was shot-perforated at 10,017' for the test of shut-off.
- 2. All except 1620' of the tubing was removed and 1395' of water cushion and 1479' of gas cut drilling fluid was recovered.

THE INSPECTOR NOTED:

- 1. When the remainder of the tubing was removed, 1620° of very gassy drilling fluid was found above the tester valve. The gassy drilling fluid would occasionally unload, blowing 60 or 70 feet into the air.
- 2. The pressure recorder charts indicated that the tester valve was open during the entire test.

THE SHUT-OFF AT 10,017' IS APPROVED.

GWH: of

Orig: Company, L.A. cc: Mr. M. H. Fuller

R. D. BUSH, State Oil and Gas Supervisor

By Quel

Deputy

DIVISION OF OIL AND GAS

REPORT ON PROPOSED OPERATIONS

					No. P.	5-9110
		***************************************	Coalinga,	Calif	March 30,	19 51
MR. M.	, H. Fuller					
_	Box 165,	Burrel,	Calif.			
	Agent for	L. M. LOCKHART				
DEAR S	Sir:					
	Your supple	mentary proposal	to drill	Well	No."England" 1	-31
Section	31 , _{T.} 14S.	R. 13E., M.D.B. & M		Field, _	Fresno	County,
dated_	March 28, 19 51	, received March 28, 1	951, has been examined	in conjunc	tion with records filed	l in this office.
11-17-1	14" cem. 609'. 9-7/8" hole t 7-5/8" " t	ions are as follow T.D. 10,357', p to 10,033'.	lugged with cemen	t 10,357	" to 10,163".	
ग शुः		1/2" casing at 10, vision to Witness production."				
	e proposal is	APPROVED PROVIDED				

above the cementing point, prior to drilling out the cement below that depth.

Bond No. 965734 CHC:ef Orig: Company, L.A. cc: Mr. M. H. Fuller

R. D. BUSH

28489 6-50 19M SPO

DIVISION OF OIL AND GAS

Supplementary Notice

COMMISSA, CALIFORNIA.

	Coalinga,	Calif. March	28, ₁₉ 51
DIVISION OF OIL AND GAS			
Coalinga,	Calif.		
Our notice to you dated	November 22	, 19 <u>50</u> , st	ating our intention to
Drill	well No. "Eng	gland" 1-31	
(Drill, deepen, redrill, abandon) Sec. 31 , T. 14 S. , R. 13 E.	, <u>М. D.</u> В. & М.	*** *** *** *** **** **** **** **** ****	Field
Fresno	County, must	be amended on account of	of changed or recently
discovered conditions.			,
The new conditions are as follows:			
609' 14" cem. 612'. T.D. 10	0,357', plugged with o	cement 10,357' to	10,163'.
9-7/8" hole to 10,033	t.		
7-5/8" " to 10,357	† .		
Encountered oil and gas	s shows below 10,000'		
We now propose			
1. Cement 5-1/2" casir 10,163'.	ng at 10,033' to test	showings between	. 10,033' and
2. Notify Division to	witness shut-off test	t through holes a	t 10,015'.
3. Test for production	1.		
		·	
A STATE OF THE STA	TO MAKE THE WASHINGTON TO THE STATE OF THE S		
HARD HOLD TO THE	350		

L. M. LOCKHART

(Name of operator)

By Henn M Carl.

Engineer

17988 11-49 8750 SPO

DIVISION OF OIL AND GAS

REPORT ON PROPOSED OPERATIONS

			No. P 5	-9002
	Coalinga,	Calif. Nove	ember 24,	19 50
Mr. M. H. Fuller				
Box 165, Burrel,				
Agent for L. M. LOCKHART				
DEAR SIR:				
Yourproposal	to drill	Well No. **	Ingland" l-	-31
Section 31 , T. 148. , R. 13E. , M. D. B. & M.				
dated Nov. 22, 19 50, received Nov. 24, 19				-
Present conditions as shown by the records a THE NOTICE STATES: "Legal description of lease S. E. The well is 660 feet S., and 660 Elevation of ground above sea levall depth measurements taken from ground. We estimate that the first product depth of about 7000 feet."	. one-quarter of feet Z. from cer vel 406.6 feet. n top of Kelly B	Section 31-14 nter of Sec. ! ushing, which	31-14/13 is 12.5 fe	
PROPOSAL: "We propose to use the following at them as herein indicated: Size of Casing, Weight, Inches Per Foot 14 47.54 8-5/8 32 It is understood that if changes you before cementing or landing	Lb. Grade and Type Smls SmlsT&c in this plan be	Depth SJ 600 600 7000	Landed Cemente Cemente Cemente	or d
THE PROPOSAL IS APPROVED PROVIDED 1. Water suitable for irrigation 2. Mud fluid of sufficient weights shall be used in drilling, and to the surface at all times, 3. Adequate blow-out prevention operation at all times. 4. The 14" casing shall be cement casing from the shoe to the grading or cement (a) Before landing or cement.	a shall be proted to and proper condition of particularly who equipment shall ated with sufficience ground surface. IED: ting any casing	nsistency to provided she provided state to the content to below the sur	prevent blo all be main ne drill pi and kept re	w-outs tained .pe. ady for of this
(b) To witness a test of each Bond No. 965734 CHC:ef Orig: Company, L.A. ce: Mr. M. H. Fuller	ch possible wate: R. D. BUSH State Oil and G		D.	•

28489 6-50 19M SPO

RECEIVED NOV 2 4 1950

DIVISION OF OIL AND GAS

COALINGA, CALIFORNIA

019 00193

Notice of Intention to Drill New Well

This notice must be given and surety bond filed before drilling begins

		Los Angeles	Novembe	er 22 50
DIVISION OF OIL AND	G AS		Calif	19
Coali	nga	Calif.		
commence the work of drilling R. 13E., M.D. B. & Legal description of lease	mg well No	, Statutes of 1939, notice is gland" 1-31 reek Area Field r of Section 31-14/13 feet E. Field	enter of Secundarision)	County.
Size of Casing, Inches	Weight, Lb. Per Foot	Grade and Type	Depth	Landed or Cemented
14	47.54	SmlsSJ	6001	Comented
8-5/8	32	Smls T&C - J55	70001	Cemented
Address 824 Wilshin Los Angeles	changes in this plan become Boulevard 17, California 1588	nome necessary we are to notify Lack	you before ceme M. LOCKHAR! (Name of Operat	P
Address One Co	PY*OF*NOT*CE*TO DIVIS	SION OF OIL AND GAS IN DISTR	RICT WHERE WEL	L IS LOCATED

		DESCRIPTION OF THE PARTY OF THE			in the second	District the second	v.			
Many		Mass.	Orose Secuen	Caree	FETBS					
		MAG-4P.F	Section	/RES - F-E	114	1選/	3			
E	11/24/50 11/2			Andrew Control		to description of	Section Contraction			

•			
Recent to			
Pliocene			
Miocene?	•		
Focene	Kreyenhagen Domengine		
Eocene and Paleocene	Lodo		
Paleocene	Martinez		
Cretaceous	Moreno	Brown MT.Sd. Rassed Volley Siltele Joaquen Redgess.	723
		6380	-0 8 2 S

APPENDIX 2 CALGEM RECORDS - AMERICAN HUNTER SOUZA 1

RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION DIVISION OF OIL AND GAS

REPORT OF WELL ABANDONMENT

	Coalinga	California
	<u>January 29, 198</u>	36

T. CC O		
Jeff Greening, Agent		
AMERICAN HUNTER EXPLORATION, LTD.		
306 Pescado Circle		
Rancho Murieta, CA 95683		
Your report of abandonment of well "	'Souza" 1	
	(Name and number)	
A.P.I. No. 019-21924 , Section 3	36 , T. 148 , R. 12E , M. I	B. & M.,
	field, Fresno	County,
4-4-4		
dated July 5, 1984 receive	d July 13, 1984	has been
examined in conjunction with records filed in	n this office, and we have determi	ned that all of
the many series of the series		
the requirements of this Division have been ful	lfilled.	
GWM/bcm	· · · · · · · · · · · · · · · · · · ·	
cc: Conservation		
Company, Canada		

M.G. MEFFERD, State Oil & Gas Supervisor

State Oil and Gas Supervisor

By Richard F. Curtin

Company american Hunter	Vell No. Bouna	
API No. 019-21924 Sec. 36,	T. 14 , R. 12	,B.&M
CountyField		
RECORDS RECEIVED DATE	STATUS	em a filte
Vell Summary (Form OG100)	MARKATCH COLON PARAMETER PROTECTION AND COLON PARAMETER PROTECTION PARAMETER PRO	STATUS
distory (Form OG103)		_ Water Disposal _
ore Record (Form OG101)		Waterflood .
irectional Surveyidewall Samples		Steamflood Fire Flood
	Abandoned - Dry Hole	Fire Flood Air Injection
ther	Producing - Gas	_ Gas Injection _
ate final records received	Idle - Gas	_ CO ₂ Injection
lectric logs:		_ LPG Injection
	Gas-Open to Oil Zone	Observation
	Waterflood Source	
	DATE	"well Yes□ N
	RECOMPLETED	
	REMARKS	
ENGINEER'S CHECK LIST	CLERICAL CHE	CK LIST
Summary, History, &	1. Location change	_(F-OGD165)
Core record (dupl.)	Elevation change	(F-OGD165)
	2. Elevation change 3. Form OGD121	1/29/86
Operator's Name	4. Form OG159 (Final	Letter) //29/8
A TRING COLD	5. Form OGD150b (Rele	
Well Designation	6. Duplicate logs to	archives
Elevation	7. Notice of Records	
	8. EDP (F-OGD42A-1, 2)	A STATE OF THE PARTY OF THE PAR
"T" Reports	publicance Ray	
castile vector	Hish Res Diameter .	
Plugs	*	
Surface Inspection 11-1-84 TSB 4-7-85 47 Production	hillsel Electron IV	
Production	ath Den-compreh, 1	
E Well on Prod. Dir. Sur	Cyberlook 1 24	- 5
	Dillsel 1	•
	Borehole com/sonic IV	
	microlos forebole com fonce IV S	
	Borefule com/Source IV 7	1 4 2
	A 1	
	Sodewall Sample Log 1	
	and Gameric Runs	
Shall Charles Colored	DE 3+5 V	.1 8 4
med state espies		See Affiched
CORDS NOT APPROVED	records approved 6 0	M 10-16-85
	RELEASE BOND/	
^	Date Eligible	PROPERTY OF THE PROPERTY OF TH
rocks Dighter 1015	(Use date last needed	records were
· Void	received.)	65h
	MAP AND MAP BOOK 🔶 🗸	3-8 10-16-85
	83=1021	

API No. Sec.	, T. , R. B. &M.
WORK PERFORMED	STATUS DATE
Drill Redrill Deepen	Producing "E" well Yes No
Plug Alter Casing	Recompleted Producing
Waterflood Water Disposal	Waterflood
Abandon	Water Disposal
Other	
Control and the Control of Contro	
	$0 the r_{\tt majority distribution distribut$
	MAP AND BOOK Engineer
RECORDS FILED AND DATE Clerk	RECORDS & REQUIREMENTS CHECKED Engineer
Summary	
Log and Core	
History	
E-log	Constitution when the disconnect tensor the supercharge and supercharge the disconnect and the supercharge
Directional Survey	
Other Control of the	
(Check records for signature and	Surface Inspection
correct name of operator or well,	Data Needed
section, township, range, and field.)	Request Records OGD170
Location Notice states	Correct records OGD165 (Specify)
	EDP(OGD42A-1, 2)
	DONTO
	II-14 December
Elevation Notice states	
	Tod overfine trees
	Release requested
	Check One)
Production Reports	Well abandoned
	Environmental Inspection Engineer
(If production reports not received,	FINAL LETTER OG159
make notation and inform Senior Stenographer when received.)	and File cleared OGD121

RECEIVED

RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION DIVISION OF OIL AND GAS

JUL 13 1984 API No. 019-21924

WELL SUMMARY REPORT DIVISION OF OIL & GAS

The state of the same of the s	MERICAN	HUNTER E	XPLOF	ATION LT	D.		Well	SOUZA #1						
Field		\$60 KW \$50 BOO	CON)		in the commence of the commenc	TOTAL MANAGEMENT AND	County	Fresno	a vi sant te transmitti (SABLANNE ANA PERANGANA ANA PERANGANA		Sec. 36	T. 145	R. 12E	B.&M M.D.
O.	21.00	ast aron	y sec	tion line	8			or California		es)	Elevat	ion of gro	und above	.1
Commence	d drilling (d 3-11-04	late)			tal de (2nd)	pth	3rd)	Depth meas	urement		n from to otary Tab	op of:	8 ft. Kelly Bus	hina
8:	drilling (da 3 -12-13		Prese	217° nt effective o				Which is	26	fee	et above	ground	DEPTH	IIIII
N,	ig 🔲 Pu	umping	Junk Note	N/A	***************************************	ole - 17	log i	See At	tachme	ent i	1			
Gas lif	ft oducing zon	e(s)	*****)le - T.						1		
N/	'A							Formation of Lathro		at tota	l depth	İ		Military was a new party of the second
<u>liilliilliilliilliilliilliilliilliilli</u>		Clean Oil (bbl per day)	Gravity Clean Oil		Percent including		Gas		Ti	ubing Pre	essure	Casing F	⁾ ressure
Producti Producti	on	N/A			·								-	
After 30 a	ays	N/A			7 4 6 1 4	0 D==0					A		West of the second of the seco	**************************************
Size of Casin (API)	Top of Cas	sing Depth o	f Shoe	Weight of Casing	ı	G RECORI Grade and Ty of Casing		nt Hole) New or Second Hand	Size o Dril		or Cu	r of Sacks bic Feet Cement	Depth of ((if thro perforat	u ah .
9 5/8"	Surface	170	91	36#	K55	, LT&C		New	12 1/	'4"		cu.ft.	lead	slurry
5 1/2"	Surface	1021	31	20#	AC-	80, LT&C	2	New	8 3/	4 "		cu.ft.	lead taile	slurry d
PERFORAT	ED CASINO	Size, top,	pottom,	perforated inte	rvals,	size and spa	icing of p	erforation and	method.)			- Angelija de		Orthodox 6th + / 4 / A brook-reasons are
		achment (
L Tes	X No	lly drilled?	If yes,	show coordi	nates	at total de	pth				The same are the same and the same are the s	OPPANIANIANIANIA PERUNTANIANIANIANIANIANIANIANIANIANIANIANIANIA		
Electrical lo Other survey	See Att	achment {	3											
n compliance	e with Sec.	3215, Divisi	on 3 of	the Public I	Resou	rces Code,	the info	rmation given	herewit	h is a	comple	te and coi	rect recor	d of the
Name	Don L. 1		work do	ne thereon, s	so far	as can be o	Title	ed from all av	vailable —————	record	S.			
Address		Fourth					City	Calgary,					Zip Code T2P 3	
Telephone Νι	_{Imber} 260-1740		Sign	ature	Ź	MA					ite 2	. O. F	1011	
G100 (3/82/		/-				11 1 1 g					s	SUBMIT I	N DUPL	ICATE

WELL SUMMARY REPORT

Attachment #1

Souza #1 - Fresno County, California

FORMATION TOPS	(KB 452)		
<u>Formation</u>	Sample top	E-log top	Sub-sea <u>(E-log)</u>
	(Spud in Quater	nary beds)	
Pliocene	(In surface hol	e)	
Miocene(?)	2578	2574	- 2122
Kreyenhagen	2977	2992	- 2540
Domengine	3654	3655	- 3203
Glauconitic	4185	4192	- 3740
Upper Dos Palos	4596	4598	- 4146
Cima	4658	4662	- 4210
Lower Dos Palos	5126	5130	- 4678
Dosados	5906	5909	- 5457
Blewett (morenu)	6512	6512	- 6060
Ragged Valley	7341	7342	- 6890
Tracy	7435	· 7440	- 6988
Sawtooth	7987	7990	- 7 53 8
Lathrop	91.56	91.5 7	- 8705
Total Depth	10,217	10,212	
	(Driller)	(Logger)	
LOGGING SUMMARY	(Logging by S	Schlumberger)	
RUN NO. 1 (at 7332')		•	
Dual Induction - SFL		7298 - 1709	
BHC Sonic Log		7304 - 145	
Litho-Density - Comper	nsated Neutron	7304 - 145	

History of Oil or Gas Well Attachment #1 Drilling History

RECEIVED

JUL 13 1984

DIVISION OF OIL & GAS

AMERICAN HUNT	ER/SOUZA #1	SW 1/4, SE 1/4, SEC 36, T14S, R12E MDB & M FRESNO (CO CALIFORNIA
83-11-03		Rigging up. Rig to raise derrick. Estimate spud tomorrow - P.M.	(MONT. 19)
83-11-04		Rig to Spud. Rigging up - 18 hrs.	(MONT. 19) (63,289)
83-11-05 (1)	1602 Ft	SPUD TIME: 08:30 Hrs 83-11-04	(MONT #19)
	Surface	Progress: 1602 Ft.	(71,374)
83-11-06 (2)	1652 Ft	Wait on Casing.	(MONT # 19)
	Surface	Progress: 50 Ft	(78,612)
83-11-07 (3)	1709 Ft	W.O.C. Progress: 57 Ft Run 44 jts, 9 5/8" 36#, K-55, LT&C casing. Cemented w/ 82 bbls 2:1:2 poz, tailed in w/ 60 bl + 2% CaCl ₂ . Plug down Time: 01:30 Hrs 83-11-07. Total Length of csg run 1713 '. Set @ 1709' KB.	(MONT # 19)
	Surface		(99,972)
83-11-08 (4)	1731 Ft	Drilling	(MONT. 19)
	Surface	Progress: 22 Ft	(109,486)
83-11-09 (5)	2809 Tremblay	Drilling Progress: 1078 2339 - 1 1/4°	(MONT. 19) (159,532)
83-11-10 (6)	4004 F†	Drilling	(MONT. 19)
	Eogene	Progress: 1195 Ft	(169,460)
83-11-11 (7)	4911 Ft	Drilling	(MONT. 19)
	C/Sand	Progress: 907 Ft	(183,948)
83-11-12 (8)	5758 F† M/Shale	Drilling. Progress: 847 Ft 5661 - 1°	(MONT. 19) (193,450)
83-11-13 (9)	6061 Ft M/ Shale	Ream to Bottom Progress: 303 Ft 6061 - 2°	(MONT. 19) (207,230)
83-11-14 (10)	6249 Ft	POH for DST.	(MONT. 19)
	Dosado/S	Progress: 188 Ft	(217,811)

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AMERICAN HUNTER/SOUZA #1 SW 1/4, SE 1/4, SEC 36, T14S, R12E MDB & M FRESNO CO CALIFORNIA
 83-11-15 (11)
                 6373 F+
                            Circ. sample
                                                                                (MONT. 19)
                 Bluitt
                            Progress: 124 Ft
                                                                                (228,763)
                            DST # 1: (6249 - 6202) 10/60/90/180
                            Results to follow.
83-11-16 (12)
                 6373 Ft
                            RIH with bit.
                                                                                (MONT. 19)
                 Bluitt
                            Progress: Nii
                                                                                (242,579)
                            6373 - 2°
                            DST # 1:
                                      (6201.5' - 6249') 10/60/90/180
                                      PF: Strong air blow - NGTS
                                      ISI: GTS after 10 mins. 5' flare
                                      VO: GTS immediately - 6' flare, decreasing to 1' flare
                                           in 25 mins and steady - Charts show plugging.
                                      REC: 5' thick drilling mud
                                      IHP 3003 PS1
                                                        PFP
                                                              22 - 22 PSI
                                                                             ISIP
                                                                                   1506 PSI
                                           3003
                                                        FP
                                                              22 - 22
                                                                                   1506
                            DST # 2:
                                      (6308' - 6373') 10/60/60/120
                                      PF: GTS - 4 mins, est. 750 MCF
                                      VO: GTS immediately - max. 682 MCF, levels off to 435
                                           MCF - stabilized.
                                     REC: 15' thick slighly gassy cut drlg mud.
                                                       PFP 208 - 167 PSI ISIP 2747 PSI
                                      IHP 3108 PSI
                                           3108
                                                             146 - 62
                                                                                   2641
                                      Charts show slight plugging.
                                      BHT: 152° F
83-11-17 (13)
                6512 Ft.
                           POH with DST # 3
                                                                               (MONT. 19)
                Bluitt
                           Progress: 139 Ft.
                                                                               (252.041)
                           6512' - 2°
                           DST # 3: 6463' - 6512' 10/60/90/180
                           Results to follow.
                           DST # 3:6463'- 6512' 10/60/90/180
                           PF: GTS - 4 mins, 15-20' flare, est. 400 MCF descreasing
                               to 10' at end.
                           VO: 10' flare decreasing to 3' in 40 mins - stabilizing
                           REC: NII
                           PF 66 - 55
                                         IHP 3183
                                                      ISIP 1195
                           FF 22 - 22
                                              3183
                                                            1195
                           BHT - 162° F
                           Charts indicated plugging.
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AMERICAN HUNTER	R/SOUZA #1 S	SW 1/4, SE 1/4, SEC 36, T14S, R12E MDB & M	FRESNO CO CALIFORNIA
83-11-18 (14)	6915 Ft Bluitt	Drilling Progress: 403 Ft	(MONT. 19) (264,159)
83-11-19 (15)	7286 F† Bluit†	Drilling Progress: 371 Ft 6940 - 1 1/2° BGG - 20 units	(MONT. 19) (281,755)
83-11-20 (16)	7332 Ft D/Valley	Ream to Btm. Progress: 48 Ft 7332 - 2°	(MONT. 19) (317,933)
83-11-21 (17)	7699 Ft Tracy	Drilling Progress: 367 Ft	(MONT. 19) (326,396)
83-11-22 (18)	8080 F† SWTH/Sh	Drilling Progress: 381 Ft BGG - 20 units.	(MONT. 19) (337,108)
83-11-23 (19)	8525 Ft SWTH/Sh	Drilling Progress: 445 Ft 8402 - 2°	(MONT. 19) (347,476)
83-11-24 (20)	8615 Ft. SWTH/Sh	Wash to bottom. Progress: 90 Ft. 8615 Ft - 2°	(MONT. 19) (359,091)
83-11-25 (21)	8730 Ft Sawtooth	POH. Progress: 115 Ft	(MONT. 19) (371,759)
83-11-26 (22)	8815 Ft Sawtooth	Drilling. Progress: 85 Ft 8730' - 2°	(MONT. 19) (386,589)
83-11-27 (23)	9019 Ft Sawtooth	Drilling Progress: 204 Ft	(MONT. 19) (395,574)
83-11-28 (24)	9159 Ft Lathrop	POH to core Progress: 140 Ft	(MONT. 19) (405,333)
83-11-29 (25)	9200 Ft Lathrop	POH w/ DST Progress: 41 Ft CORE # 1: Lathrop 9159' - 9200' Rec: 40 1/2' Core. 9159' - 2°	(MONT. 19) (416,024)

	- 1, 0002/1 FT	SW 1/4, SE 1/4, SEC 36, T14S, R12E MDB & M FRESNO	CO CALIFORNIA
83-11-30 (26)	Lathrop 9200 Ft	POH w/Test tools. Progress: Ni! DST # 4: 9156' - 9200' (Lathrop Sand) PF WAB - inc. SAB Lost packer seat in 2 mins Used and recovered 1200' water cushion & 523'	(MONT. 19) (426,089) drlg. mud.
		DST # 5: 9160' - 9200' (Lathrop Sand) Used 2000' water cushion Bottom hole conventional PF: Lost packer seat immediately, attempt to reseat again.	reset, lost packe
83-12-01 (27)	9317† Lathrop	Circ. sample Progress: 117	(MONT. 19) (439,527)
83-12-02 (28)	9433† Lathrop	Pick up DST # 6. Progress: 116 Ft. DST #5: Used and rec. 2000' water cushion IHP 5287 PSI 5213 Miscun, lost packer sort immediately	(MONT. 19) (450,672)
83-12-03 (29)	9480 Ft Lathrop	E 4 D 4	(MONT. 19) (469,803) 287 PSI
33-12-04 (30)	9726 Ft Lathrop	RIH to Core. Progress: 246 Ft. 9689' - 3 3/4° CORE # 2: 9726' - 9778' (L/Lathrop) Cut 54' Rec - 45'	(MONT. 19) (478,458)
3-12-05 (31)	9778 Ft Lathrop	POH w/test tools. Progress: 52 Ft DST # 7: Results to follow.	(MONT. 19) (488,584)

DRILLING HISTORY

AMERICAN HUNTER/SOUZA #1 SW 1/4, SE 1/4, SEC 36, T14S, R12E MDB & M FRESNO CO CALIFORNIA

83-12-13 (39) 10,217' TD Tear out BOP's

(MONT. 19)

Progres: NII

(830,653)

Ran 257 jts 5 1/2", AC-80, 20#, LT&C csg. Landed @ 10,213 KB. Followed by 1532 cu ft. + .8% D-60, + .3% D-13, +.3& D46, followed by 755 cu ft. + .2% D-46 + .2% D-60. PDT: 0310 Hrs

83-12-13.

83-12-14 (40)

Tear out BOP's and cut casing.

(MONT. 19)

RIG RELEASE: 16:00 Hrs 83-12-13

STATUS: POTENTIAL GASWELL

(851,516)

History of Oil or Gas Well Attachment #2 Completion History

AMERICAN HUNTER SOUZA # 1

THERETORIA HOLLING SOUZA # 1		
84-03-30 (1)	Rigging up. Move in rig and equipment. Rigging up.	(GAMACHE # 1) (7,180)
84-03-31 (2)	Run tubing. Finish rigging up. Unload 2 3/8" N80 tubing. Cut Install BOP. Fill tanks with 800 bbls fresh water	(GAMACHE # 1) off casing. (51,517)
84-04-01 (3)	Run tubing. RiH with 25 joints 2 3/8" tubing with 4 5/8" bit. drilling mud with fresh water. High winds and hear	(GAMACHE # 1) Reverse out vy rain. (56,434)
84-04-02 (4)	Run tubing. RIH with bit to 8400'. Circulate out drilling mud water every 1000'.	(GAMACHE # 1) with fresh (60,232)
84-04-03 (5)	RIH with scraper. RIH with bit to 10165'. Break circulation every 6 9000'. Circulate down to PBTD at 10177'. Circulate drilling mud. POH. RIH with bit and scraper on 40 Gray oil tool arrived with primary seal. POH. Pictubing spool. Install primary seal and tubing seal seals to 5000 PSI. Held good.	ed out thick) jts tubing.
84-04-04 (6)	Schlumberger. Run CBL-VDL-CNL-GR log from PBTD to	(GAMACHE # 1) CL. POH. Rig 2400 ft. (68,198)
84-04-05 (7)	log and TDT logs from PBTD to 2400 ft. Bond logs in	(GAMACHE # 1) Ran CET-GR-CCL nidcate no (71,909)
84-04-06 (8)	RIH to PBTD with tubing. Haul in chemicals to mix	(GAMACHE # 1) mud. (110,073)
84-04-07 (9)		(GAMACHE # 1) (113,633)

84-04-08 (10)

Est. circ between perfs.

Pressure test casing to 5000 psi for 15 mins. Held O.K. Displace hole to 11.2#/gal gel mud. POH w/tbg. Fill hole. Perforate intervals 10060 - 10061 and 9870 - 9871' w/ 4" HSC casing gun @ 90° phasing w/ big hole charges @ 4 SPF. RIH with 4 jts tubing, retrievable packer and 2 3/8" tubing. Set packer @ 9915' KB.

Pump down tubing @ 1/6 BPM @ 3000 psi w/returns up annulus. Pump 1/2 bbl. S.I.F.N. (124.143)

84-04-09 (11)

Run tubing and stinger.

Pump mud down annulus and up tubing starting @ 1/6 BPM @ 3300 psl. Pump total of 95 bbls. Final rate of 3/4 BPM @ 2800 psi. Recovered small amounts of gas and solids. No loss to formation. Unseat packer and lower tall pipe to 10112' KB. Reverse circ hole clean w/ 50 bbls mud. POH w/tubing and packer. Rig Schlumberger and set EZ drill cement retainer @ 10056' KB. Pick up stinger and RIH w/ 206 jts tubing. S.I.F.N. (130.270)

84-04-10 (12)

Running free point. (GAMACHE # 1) Finish RIH w/tubing and stinger. Stab retainer and pressure test to 1000 PSI. Est. circ rate of 3/4 BPM @ 1800 PSI w/8 bbis mud. Rig Howco to cement w/65 sxs Class "G" + 30% silica flour + 5% KCL + 1/4#/sxs D-Air + 0.1% HR-7 + 0.75% FDTC - 322. Pull out of retainer. Circ 10 bbls mud flush, 17.7 bbls slurry, 2 bbls fresh water and 7 bbls mud to bottom of tubing. Stab retainer and displace w/27.5 bbls mud @ 1 BPM @ 3000 PSI. Bleed off tubing and casing pressure. Pull out of stinger and pull 10 jts tubing to 9745'KB. Reverse circ clean w/61 bbls mud. Recovered 11 bbls cement. Start cement @ 1205 hrs. Flnish reverse circ @ 1350 hrs. Attempt to pull tubing. Would not move. Work tubing - no movement. Circ mud for 30 mins @ 1.5 BPM @ 1200 PSI for 3 hrs. Pull tubing to 80,000# - no movement. Land tubing in slips and pressure casing to 500 PSI. S.I.F.N. (137, 136)

84-04-11 (13)

Bleed off 500 PSI wellhead pressure. Rig Schlumberger and run free point tool. Found free point @ 9360 KB. Reverse circ hole to fresh water. SIFN. (145,456)

84-04-12 (14)

Pull tubing.

Rig Halliburton and circ 750 gals 15% HCL + inhibitor down tubing and up casing annulus. Wash acid past tubing by alternately pumping down tubing and casing. Work tubing, no movement.

Backwash acid w/fresh water. Acid partly spent w/ small volume of acid gas. Rig McCullough and cut tubing @ 9355' KB w/ chemical cutter. Pull tubing w/drag on first joint then pulled free. Pull 200 jts tubing. SIFN. (154,516)

84-04-13 (15)

Pull washover pipe.

Pull remainder of tubing and lay down cut off joint. Pick up 4" washover mill and 217' of 4" x 3 3/8" washpipe, jars, bumper sub and RiH on 2 3/8" tubing. Tag obstruction @ 8936' KB. Rig Power Swivel and mill out cement stringers to 9226' KB. Pipe torquing up. Circ. hole clean. Start POH w/washover pipe. (158,676)

84-04-14 (16)

Washing over tubing. (GAMACHE#11)
POH with remaining tubing and washpipe. Pick up 4 5/8" bit and
RIH to 9226' KB. Rig up power swivel and ream out cement to top
of fish at 9355' KB. Circulate hole clean. POH with tubing and
bit. Pick up washover mill, 245' washpipe, jars and bumper sub
and RIH to 9355' KB. Rig up power swivel and washover fish to
9460' KB. Fine ground cement returns. (165,250)

84-04-15 (17)

POH with washpipe.

Washover fish to 9600' KB. Circulate clean. POH with tubing and washpipe. Pick up tubing cutter and grapple and RIH with tubing. Made cut at 9572' KB. POH and lay down 7 joints tubing and 2 cut off stubs. RIH with washover mill and washpipe to 9600' KB. Washover fish to 9745' KB. No progress in 20 mins. Should be at top of cement stinger. Circulate hole clean. (170,790)

84-04-16 (18)

Drilling on cement retainer.

POH with tubing and washpipe. Pick up overshot. RIH and latch fish at 9572' KB. POH with tubing and overshot and recovered 6 joints tubing and retainer stinger. Pick up 4 5/8" bit, six 3 1/2" drill collars. RIH and tag cement at 9745' KB. Drill through cement to 9885' KB. Pressure test upper perfs to 2000 psi. Held O.K. Run down and tag cement at 10,051' KB. Drill through cement and tag retainer at 10,056' KB. Drill on retainer. (176,150)

84-04-17 (19)

Rigging out Schlumberger.

Drill out cement retainer and cement to 10,062'KB. Clean out to 10,177'KB. Circ hole clean. Pull tbg and lay down DC's. Pick up casing scraper and RIH to 10,177'KB. Work scraper from 8920 - 10,070'KB. PT csg to 2000 PSI. Held 0.K. Displace hole to 3% KCL water. POH. Rig Schlumberger and run CBL-VDL-CCL and CET-CCL from PBTD to 9200'KB. Made 2 passes with zero pressure and 2000 PSI

84-04-18 (20) Lathrop

Pull FWG plug. (GAMACHE #11) Pick up Van gun assembly, firing head, $4! \times 2 3/8"$ pup, 2 3/8"tubing release w/1.81" latch, $10^{\circ} \times 2^{\circ} 3/8$ " pup, 1.81 "F" nipple, $2.3/8" \times 10!$ pup, $2.3/8" \times 10!$ pup, 2.3/8" flow disc assembly, Brown Hughes M-1 packer, 2 3/8" x 2' pup, Baker EL-2 on-off too! w/1.875 profile w/blanking plug in place, 1 jt 2 3/8" tubing, RA Marker Collar, 6' pup and RIH w/ 2 3/8" tubing and space out pups. Position gun wSchlumberger GR tool. Set packer in 9000# compression. Re-check position w/GR tool. Release and re-set packer @ 9924' KB w/gun positioned to perforate Lathrop formation inervals 10,035 - 10,045!, 10,014! - 10,026!, 9990 - 9999!, 9975 - 9986', 9967 - 9971'. Pressure test packer to 500 psi. Held O.K. Remove BOP's and install wellhead. Rig Baker to pull FWG plug. (221.742)

84-04-19 (21) Lathrop

Assemble guns.

Pull equalizing prong and Mandril from EL-2 profile @ 9920' KB.

Drop detonating bar to fire guns. No positive indication of firing. Slight air blow up tubing. PT annulus. Circ hole @ 1.5 BPM @ 200 PSI. Indication of packer failure. Rig wireline and attempt to pull detonating bar. No success. Install BOP's.

Unseat packer and POH. Top 3 sections of gun fired at low order detonation. Bottom 2 did not fire. Order new guns, install new FWG plug in EI-2 on-off connector. Redress packer.

84-04-20 (22) Lathrop

Rig up braided line.

RiH w/ new gun assembly, 2 3/8" x 10' pup, 2 3/8" x 4' pup, tubing release, 2 3/8" x 4' pup, 1.81 "F" nipple, 1 jt 2 3/8" tbg. Fill disc assembly, M-1 packer, 2 3/8" x 2' pup, EL-2 on-off tool with FWG plug in place, 1 jt 2 3/8" tubing, RA marker collar, 2 3/8" x 6' pup on 2 3/8" tubing. Position gun with Schiumberger. Set packer @ 9905' KB. Re-check depth with wireline. O.K. PT annulus to 500 PSI. O.K. Install wellhead. Rig Baker and pull equalizing prong from FWG plug. RiH and latch plug. Unable to pull plug. Attempt to shear from pulling tool. W/L parted @ surface. Fish wire and drop cutter bar to cut @ rope socket. Rig out slick line. (234,397)

84-04-21 (23) Lathrop

Pulling tubing.

Rig up braided line. RIH and recover cutter bar. RIH and latch FWG plug. Jarred for 3 hrs. Unable to pull plug. Pulled out of rope socket and rig out braided line. Remove WH and install BOP's. Unseat packer. POH w/tubing and assembly. Dogs on FWG plug were broken. RiH w/open ended tubing to PBTD. Rig Howco N2 unit and blow hole dry w/N2. Start POH w/tubing.

(247.898)

84-04-22 (24)	Lathrop	Swabbing. (GAMACHE#11) 0800 hrs (10 hrs S.I.). No measurable pressure on wellhead. Bleed off - very light gas flare to pit. Well dead. Pick up and RIH w/the following: 1.79 Otis "XN" nipple, 1 jt tubing, 1.87 Otis "X" nipple, 2 3/8" x 4' pup, M-1 packer, 2 3/8" x 2' pup, Otis tubing seal divider w/1.87 profile and 2 3/8" tubing to surface. Set packer @ 9902.6' KB w/XN nipple @ 9940.3'KB. Fill annulus w/3% KCL water and PT to 500 PSI for 30 mins. Held 0.K. Rig to swab. iFL @ 8600'KB. Pulled 2 swabs to 9890' to recover 3 bbls mud and muddy water. FFL @ 9600'. S.I.@ 1400 hrs. (260,310)
84-04-23 (25)	Lathrop	Swabbing. 0700 hrs (17 hrs S.I.) No measurable pressure on Wellhead. Rig to swab. IFL @ 8300'. Pulled 3 swabs over 9 hrs to recover 6 bbls water. No gas flow. Salinity by refractometer 9600 PPM. S.I. @ 1700 hrs. (263,190)
84-04-25 (26)	Lathrop	Swab testing. (GAMACHE #11) 0700 hrs (14 hrs S.i.) No measurable pressure on wellhead. Rig to swab. IFL @ 8950'. Swab total of 6 bbls water throughout day. No gas flow. FFL @ 9875'. Total new fluid recovered 15 bbls. S.I. @ 1700 hrs. (265,750)
84-04-26 (27)	Lathrop	Swab testing. (GAMACHE#11) 700 hrs 14 hrs S.I.) SITP 15 PSi. Bleed off gas head. Rig to swab. IFL @ 9500' KB. Swab a total of 3.1 bbls water throughout day. FFL @ 9800'KB. Total new water swabbed to date: 18.1 bbls. S.I. @ 1700 hrs. (268,310)
84-04-27 (28)	Lathrop	Running tbg ostinger. (GAMACHE#11) 0700 hrs (14 hrs S.I.) SITP: 10 psi. Bleed off and rig to swab. IFL @ 9000'. Pull 2 swabs to recover 1 bbl water. FFL @ 9400'. Fill tbg w/ KCI water. Press tbg to 4500 psi. No feed. Remove wellhead and install BOP's. Unseat packer and POH w/ tubing and packer. Rig Schlumberger and set EZ drill cement retainer @ 9862'KB. SIFN. (271 070)

84-04-28 (29) Lathrop

Running tubing and packer. (GAMACHE #11) Pick up stinger and RIH on 2 3/8" tubing. Stab retainer and Rig Howco and establish feed rate of 1 BPM @ 8200 PSI w/3 bbls water. Pull out of retainer and batch mlx 50 sxs cement. Circ. to bottom and sting Into retainer. Squeeze 6 bbls cement to perfs to max. pressure of 9000 PSI. Bleed off to 4000 PSI and pull out of retainer. Backwash excess cement. Rig in No unit and blow hole dry. POH w/ tubing and stinger. Rig Schlumberger and perforate the following w/4" csg gun @ 2 SPF: 9828 - 9832', 9821 - 9826', 9816 -98191, 9798 - 98111, 9784 - 97911, 9768 - 97831, 9740 -97521, 9723 - 97351, 9707 - 97121, 9698 - 97051. Total of 172 shots. Slight air blow after perforating. S.I. well @ 2400 hrs. (298.353)

84-04-29 (30) Lathrop

Swab testing. (GAMACHE#11) 0700 hrs (7 hrs S.I.) SIWHP 5 PSI. Bleed off gas head to pit. Pick up and RiH w/ the following" 1.79 Otis "XN" nipple, 1 jt 2 3/8" tubing, 1.875 Otis "X" nipple, 2 3/8" x 4' pup, Otis Permalatch packer, 2 38" x 2' pup, 1.87 tubing seal divider on 2 3/8" tubing. Set packer @ 9630' KB w/ "XN" nipple@ 9672.5 m, "X" nipple @ 9640.0' KB, tubing seal divider @ 9625.8' KB. Fill annulus and PT packer to 500 PSI for 30 mins. Held 0.K. Rig to swab. IFL @ 6800! KB. Pulled 7 swabs over 3 hrs to recover 21 bbls gas cut water. FFL @ 9200'. Sait content by refractometer 9600 PPM. S.I. @ 1700 hrs. (304.127)

84-04-30 (31) Lathrop

Swab testing. (GAMACHE #11) 0700 hrs no pressure on W.H. Rig to swab. IFL @ 3800' KB. Swab total of 34.7 bbls formation water throughout day. 9600 PPM sait by refractometer. Slight trace of gas breaking out of water. FFL @ 9400'. S.I. @ 1700 hrs. Total New Fluid Recovered: 55.7 bbls. (306.687)

84-05-01 (33) Lathrop

Pressure test bridge plug. (GAMACHE #11) 0700 hrs SITP 5 PSI. Rig to swab. IFL @ 4300'. Pull 5 swabs to recover 18.5 bbls formation water. Total new fluid recovered: 74.2 bbls. Fill tubing and establish feed rate of 0.2 BPM @ 4000 PSI. Pressure bled to 2500 PSI in 3 mins. Unseat packer and POH. Rig Schlumberger and set bridge plug @ 9670' KB. SIFN. (309.247)

84-04-02 (34) Lathrop

Circ. hole. (GAMACHE#11)
Press test BP to 5000 psl for 15 mins. Held OK. RIg
Schlumberger and perforate intervals 9467 - 68 and 9351 -52
w/4" HSC csq qun @ 90 degrees phasing, Big hole charges @ 5
shots/interval. Pick up retrievable packer and RIH on
2 3/8 tbg. Circ hole to 3% KCL water. Set packer @
9375'KB. Break circ down tbg @ 2500 psi. Attempt to
circ down annulus w/no success. Re-establish circ down tbg
@ 2.1 - 2.8 BPM @ 2500 - 3000 psi. Circ. hole for 6 hrs
until clean. Recovered sand, shale, and cement. Unseat
packer and pull above top perfs. SIFN (314,687)

84-05-03 (35) Lathrop

0700 hours SIWHP: 1100 psl. Bleed off to recover 1/2 BBL water. Circ hole clean. POH w/ tbg & packer. Rig Schlumberger & set cement retainer @ 9460' KB. Pick up stinger & RIH w/tbg & stab into retainer & establish circ. Mix 50 sxs cement (13.3 BBLS slurry) & displace between 2 sets of perfs w/KCl water @ 3.5 BPM @2800 psi. Pull out of retainer to 9210' KB & backwash excess cement. Pull tbg to 8960' KB & press up wellbore to 2000 psi. S.I. well. (334.129)

84-05-04 (36) Lathrop

0700 hours SIWHP: 1300 psi. Bleed off & POH w/tubing and stinger. Pick up 4 5/8" bit and drill collars and RIH to tag top of cement @ 9226'KB. Rig up power swivel and drill out cement and stringers to top of retainer @ 9460' KB. Circ hole clean. Press test upper perfs to 2500 psi. Held O.K. SIFN.

(337,289)

84-05-05 (37) Lathrop

Running tubing.
0700 hrs SIWHP: 1350 psi. Bleed off to recover 1 bbl KCl water. POH w/ tubing & lay down DC's. Press test upper perfs (9351-52) to 5000 psi. Press bled off to 4800 psi in 15 mins. Pick up bit & csg scraper & RIH to top of retainer @ 9460'KB. Reverse circ hole clean. POH w/ tbg & scraper. SIFN. (340 349)

84-05-06 (38) Lathrop

RIH w/ seal assembly.

0700 hrs SIWHP: 600 psi. Bleed off water head & RIH w/ 2 3/8" tbg to 9457'KB. Rig up Howco N₂ unit & blow hole dry w/ N₂. POH w/ tbg. Rig Schlumberger and perforate Lathrop interval 9380-9423 w/ 4" HSC csq gun @ 2 SPF. Total of 86 shots. 5 min air blow after shooting lower 23' and 5 min air blow after shooting upper 20'. Pick up 1.79 Otis "XN" nipple, 2 3/8 x 10' pup, 2 3/8 x 4' pup, Otis permatrieve packer & set packer on W/L @ 9357'KB. "XN" nipple @ 9378'KB.

SIFN. (360 690)

84-05-07 (39) Lathrop

Swabbing.

0800 hrs no press on WH. RIH w/ Otis anchor seal assembly 6' x 2 3/8 pup, tubing seal divider w/ 1.875 "X" profile. Latch packer, space out and land dognut. Fill annulus w/ 150 bbis water & press test to 500 psi for 15 mins. Held OK. Rig to swab. IFL @ 8550'KB.

Pulled 2 swabs from 9350 to recover 1.75 bbls water.

FFL @ 9000'. S.I. @ 1600 hrs. No trace of gas.

(363 609)

84-05-08 (40) Lathrop

Swabbing.
0700 hrs SITP: 0 psi. Rig to swab. IFL @ 6460'KB.
Pulled 9 swabs throughout day from 9350'KB to recover
12.5 bbls water. Trace of gas with swabs. FFL @ 8200'.
Difficulty swabbing dry due to swab cups wearing out.
Water salinity by refractometer 9600 ppm. Total new fluid recovered 14.25 bbls. S.I. @ 1700 hrs. (366 709)

84-05-09 (41) Lathrop

Swabbing.

0700 hrs SITP: 25 psi. Rig to swab. IFL @ 6600' K.B. Pulled 9 swabs over 9 1/2 hrs from 9330' K.B. to recover 7.5 bbls water. Trace of gas w/ swabs. FFL @ 8600' K.B. S.I. @ 1700 hrs. New mluid recovered: 21.75 BBLS.

(369,809)

84-05-10 (42) Lathrop

Swabbing.

0700 hrs SITP: 10 psi. Bleed off and rig to swab. IFL: 7920'KB. Pulled 5 swabs over 10 hrs from 9330'KB to recover 3.75 bbls water. FFL @ 9000'KB. Total new fluid recovered 25.5 bbls. S.I. @ 1700 hrs. (372.709)

84-05-11 (43) Lathrop

Pull tubing.
0730 hrs no measurable pressure on wellhead. SiCP
remaining @ 170 psi. Bleed off annular pressure. Fluid at
surface. Re-test to 500 psi. No leak off. Rig to swab.
IFL @ 7920'KB. Swab total of 3.75 bbls water throughout
day. FFL @ 9100'KB. Total new fluid swabbed: 29.25 bbls.
Fill tubing with KCI water. Pressure tubing to 4500 psl.
Annular pressure started increasing indicating we have
broken down cement between main perfs and upper squeeze
perfs @ 9350-51'. Bleed off pressure and prepare to pull
tubing. (375.709)

84-05-12 (44) Lathrop

Cement squeeze.

Puil anchor seal assembly from packer & POH. RIH w/ packer releasing stinger to top of packer. Circ hole, latch packer & unseat & POH w/ packer and tailpipe. Rig Schiumberger & set EZ drill cement retainer @ 9340'KB. PT to 3000 psi. Pick up stinger & RIH w/ 2 3/8" tbg. SIFN. (384 509)

84-05-13 (45) Lathrop

Perforating.

Sting into retainer @ 9340'KB. Est. feed rate of 1 BPM @ 5800 psi. Pull out of retainer. Mix 50 sxs cement - total of 10 bbls slurry - circ cement to bottom of tbg & sting into retainer. Pump 5 bbls slurry @ 1 BPM @ 6100 psi. Stage squeeze 1 bbl slurry to standing pressure of 6500 psi. Pull out of retainer and backwash excess slurry. Rig Howco N2 unit & blow hole dry w/ N2. POH w/ tbg. (394 649)

84-05-14 (46) Lathrop

Pulling tbg & packer.

Rig Schlumberger & perforate Lathrop intervals 9192-9199, 9182-9185, 9159-9176 KB w/ 4" HSC csg gun @ 2 SPF.
Total of 57 shots. Weak air blow after shooting 9192-99 & 9182-85 and fair blow after shooting 9159-9176.
Pick up tailpipe & packer & RIH on 2 3/8" tbg. Attempt to set packer several times without success. Start POH w/ tbg & packer. (402 349)

84-05-15 (47) Lathrop

Swabbing

0700 hrs (13 hrs S.i.) Well head press: 40 psi. Bleed off pressure w/ lazy 2 - 3' flare. POH w/ remaining tbg and packer. Re-dress pkr & RIH w/ 1.79 "XN" nipple, 1 jt 2 3/8 tbg, 1.87 "X" nipple, 2 3/8 x 4' pup, OTIS premaiatch packer, 2 3/8 x 6' pup, On - Off tool w/ 1.87 "X" profile on 2 3/8 tbg. Set packer @ 9081' w/ "XN" nipple @ 9123', X nipple @ 9091', and On-Off tool @ 9073'KB. Fili annulus w/ 80 bbls KCL water & press test packer to 500 psi. Held OK. Rig to swab. IFL @ 4850' KB. Pulled 7 swabs over 4 hrs. to recover 16 bbls water. FFL @ 8500'KB. Trace of gas w/ swabs. S.i. @ 1700 hrs.

(407.854)

AMERIC	CAN	HUNTER	SOUZA	# 1

84-05-16 (48) Lathrop Swabbing 0700 hrs SITP: 300 psi. Bleed off gas head. Rig to swab. IFL @ 2060 KB. Pulled 14 swabs over 10 1/2 hrs to recover 46 bbis water. Trace of gas with swabs. No gas flow after swabs. FFL @ 8000' KB. S.I. @ 1700 hrs. Total new fluid recovered: 62 bbls. (414.154)84-05-17 (49) Lathrop Swabbing 0700 hrs SITP: 145 psi. Bleed off and rig to swab. IFL @ 3000' KB. Pulled 16 swabs over 10 1/2 hrs from 9050' to recover 38.2 bbls water. Trace of gas with swabs. No after flow. FFL @ 7900'. S.I.@ 1800 hrs. Total new fluid recovered: 100.2 bbls. (414.354)84-05-18 (50) Lathrop Pull packer. SITP 120 psi. SICP 100 psi. Pressure annulus to 500 psi for 15 mins. Bled annulus down to 175 psi. Bled off tubing. Rig to swab. Fluid level at 3300 ft. Pulled 16 swabs over 10 hrs to 9050 ft to recover 38.85 bbls of gassified water. No gas after swabs. Final fluid level at 8400 ft. New fluid recovered 138.85 bbls. Shut in at 1800 hrs. (417.454)³4-05-19 (51) Lathrop Set packer. (GAMACHE #11) 0700 SITP 150 psi. SICP 150 psi. Bled off tubing. Fill tubing with 16 bbls 3% KCI water. Unseat packer. Circulate hole. Pull and lay down 85 joints of tubing. POH. Lay down packer. Rig Schlumberger. Set Halliburton bridge plug at 9145 ft. Pressure test plug to 3500 psi for 20 mins. Held good. Perforate intervals 6552-6553 and 6410-6411' at 4 SPF with 4" HSC gun using 22 gm charges. RIH with packer to 6329'. (426.454)84 - 05 - 20 (52)Pull packer. (GAMACHE #11) 0700 SITP and SICP 640 psi. Bled off. Circulate with 3% KCI. Well flowing. Mix 200 bbls 7% KCI. Displace hole. RIH and set packer at 64251. Squeeze 10 bbls down annulus at 1/2 BPM at 2200 psi with no returns. Squeeze 12 bbis down tubing at 3/4 BPM at 2200 psi with no returns. (431,554) 84-05-21 (53) Cement squeeze. (GAMACHE #11) 0700 SITP 580 psi. SICP 380 psi. Bled off.

Unseat packer. Pull 2 joints. Circulate hole. POH. Lay down packer. Rig Schlumberger. Set Halliburton EZ-SV cement retainer at 6545'. RIH

(438.954)

with stinger on 2 3/8" tubing and set into

retainer.

84-05-22 (54)

W.O.C. (GAMACHE #11) 0700 SITP 400 psi. SICP 100 psi. Bled off. Rig Halliburton. Establish feed rate down tubing at 1/2 bb!/min at 3600 psi with 3 bbis. Pull out of retainer. Mix 50 sxs oilwell class "G" cement plus additives. Slurry volume 10 bbls. Circulate to bottom. Stage squeeze 7 bbls to formation to standing pressure of 2250 psi. Pull out of retainer. Backwash excess cement. Pull to 63981. Establish feed rate into perforations at 6410-64111 at 1/2 bbi/min at 2100 psi. Mix 50 sxs of same cement as above. Siurry volume 10 bbls. Circulate cement to bottom. Pull tubing to 5775'. Stage squeeze 8 bbls to 2200 psi. Shut in on squeeze at 1600 hrs. (445,754)

84-05-23 (55)

Pull tubing. WOC. SIP 1950 psi at 1800 hrs.

(448.454)

84-05-24 (56)

Finish pulling tubing.
0700 hrs. SIP 1800 psi. Bleed off. POH. RIH with bit and drill collars on 2 3/8 tubing. Tag cement @ 6338 feet. Drill out cement and clean out to top of retainer at 6545 feet.
Circulate clean. Pressure squeeze to 2000 psi for 20 minutes.
Hold good. POH. SDFN with 10 joints of tubing and drill collars and bit left to lay down.

(451.454)

84-05-25 (57)

Pick up tubing.
Finish POH. Lay down drill collars. Unload new 2 3/8" N80
EUE tubing. RIH with bit and scraper. Tag top of retainer.
POH laying down tubing. Lay down bit and scraper. Pick
up and run 130 joints new tubing.

(454 554)

84-05-26 (58) Moreno

Fishing casing gun. Continue running in hole with new tubing. Land tubing at 6543'. Displace to nitrogen. POH. Rig Schlumberger. RIH with 4" HSC csg gun with 25' at 2 SPF. Log gun into position to cover interval 6466-6491'. Shot interval 6491-6481' with good kick. Gun did not appear to fire over interval 6481-6466'. Tool stuck. Worked for 1 hour. Pulled line off at gun. POH. Bottom of line covered with cement, colored material. Ordered out fishing tools. RIH w/ grapple overshot with jars and bumper sub on tbg. Took weight at 62451. Worked down and latch onto fish at 64621. Unable to hold onto latch onto fish. Pull 20 jts. Pump 32 bbls down tubing. SDFN. (458,554)

84-05-27 (59) Moreno

Run packer.

0700 SIP 50 psi. Circulate out sand and mud from
6245' to top of fish at 6461'. Latch onto fish
and pull loose with 8000 lbs. POH. Lay down
fishing tools and perforating gun. Gun had
completely fired. RiH with tubing to 6545'.
Circulate clean with 7% KCl water. POH. RIH w/
1.79 "XN" nipple + 1 joint tubing + 1.875 "X"
nipple + 4' pup joint + Perma-latch packer +
6' pup + 1.875 on-off tool on 105 joints tubing.
SDFN. (497.045)

84-05-28 (60) Moreno

Swabbing.

0730 SIP zero. RIH with packer. Unable to set packer. POH. Lay down packer. RIH w/ 1.79 "XN" nipple + 1 joint tubing + 1.875 "X" nipple + 6' pup joint + Guiberson Uni-V packer on 2 3/8" tubing. Set packer at 6367' with XN nipple at 6408'. Land tubing in dognut. Pressure annulus to 1000 psi. Held good. SDFN. Temp. 95 °F. (504.115)

84-05-29 (61) Moreno

Swab test 0830 SITP 50 psi. Rig to swab. Fluid level at surface. Pull 13 swabs over 4 1/2 hrs to 6300 feet to recover 28.8 bbls. Final fluid level at 5500 feet. Runs 9 to 13 had swab problems due to heavy drilling mud. Gas blow after swabs 9 to 13. New fluid 2.8 bbls. RIH with sinker bars to 6000 feet. POH Tools covered with heavy drilling mud and sand. SDFN at 1630 hrs

.(506,915)

84-05-30 (62) Moreno

Run coiled tubing.
0730 SITP 480 psi. Bled off. Rig to swab.
RIH and tag fluid. Level at 5500'. Unable to go deeper. Pump in 3 bbls KCI water. RIH with swab bar and work bar from 5000 to 6300'. Pull 3 swabs to 6000'. Final fluid level at 5900'. RIH with sinker bars to 6500'. POH. Tools covered with viscous drilling mud. Pulled 5 dry swabs. Si.

(510915)

-d4-05-31 (63) Moreno

Swabbing 0700 hrs SiTP: 380 psi. Bleed off & rig in OTIS coiled tbg unit RiH to 6540' KB while pumping N2. Very little fluid returns. Nitrogen appears to be by-passing fluid. Pull coiled tbg to 5000' & fill hole w/ KCL water. Break circ w/ KCL water & clean out to 6540' KB until clean returns. Rec'd approx. 5 bbis thick. mud with traces of sand. Pull coiled tbg to 6493' & spot 500 gal 15% MCA to perfs. Pull coiled tbg & squeeze acid to perfs @ 2.5 BPM @ 2450 psi. ISIP: 1750 psi bleeding to 1250 psi in 15 min. Open well to tank to recover 1.5 bbis KCL water in 30 mins. Leave open to tank w/ slight flow of water. (521,430)

84-06-01 (64) Moreno

Swabbing 0700 hrs rig to swab. IFL @ surface. Pulled 13 swabs over 9 1/2 hrs. from 6300' to recover 26.5 bbls KCL water and acid water. FFL @ 6000'. Waited 1 hr between swabs 9 and 13. Fair gas blow after swab #12. No blow after swab 13. S.I. @ 1700 hrs. LFLTR: 9.7 bbls.

(525, 180)

84-06-02 (65) Moreno

Swabbing.

0700 hrs SiTP: 240 psi. Bleed off and rig to swab. IFL @ 4800'. Pull 5 swabs over 2 hrs from 6300' to recover 4.25 bbis fluid. Good gas blow after 5th swab. Unable to get past 5200' on swab #6. RIH w/ sinker bar and unable to get past 5200'KB. Fill hole w/ KCI water. Unseat packer and reverse circ hole clean to bottom @ 6545'KB. Recover thick mud with sand and silt. Reset packer @ 6367' with tailpipe @ 6408'KB. Press test packer to 1000 psi for 15 mins. Held OK. Rig to swab. Pull 4 swabs to recover 13.75 bbis KCI water. LFLTR: 13 bbis. Si @ 1945 hrs.

84-06-03 (66) Moreno

Swabbing.

0700 hrs SITP: 340 psi. Blow down and rig to swab. IFL @ 2700 KB. Pull 9 swabs throughout day from 6000 to recover 16.5 bbls fluid.

Good gas blow after swab #3. Unable to get past 4700 on swab #4. Pump 3 bbls KCl water down tbg & work sinker bar from 4000-6000 Recovering very thick muddy fluid. FFL @ 4900 Sel. @ 1700 hrs. New fluid recover: 3.5 bbls.

(531,830)

84-06-04 (67) Moreno

Swabbing

0730 hrs SiTP: 650 psi. Blow down & rig to swab. IFL @ 3900'. Unable to get down w/ swab and sinker bar. Pump 3 bbis KCI water down tbg & work sinker bar from 3900-6300'.

Re-run swab. Recovered 7 bbis fluid in 4 runs. Fluid gassy w/ after blow. Unable to get down on swab #7. Pump 6 bbis KCI water down tbg. Unseat packer & circ hole w/ 2% KCI water to 6520'KB to recover heavy mud. Re-set packer @ 6376'KB.

Press test packer to 1000 psi for 15 mins. Held 0.K. Rig to swab. Pulled 5 swabs to recover 15.5 bbis KCI water. FFL @ 3600'. S.I. @ 1830 hrs. New fluid recovered prior to filling hole 7.5 bbis.

84-06-05 (68) Moreno

Swabbing.

0700 hrs SITP: 400 psi. Bleed off & rig to swab. IFL @ 2700'
Pull 5 swabs over 2 hrs to 5500' to recover 10 bbls KCL water &
mud. Unable to get past 5500'. Pump 10 bbls KCL water down tbg.
Unseat packer and rig to swab. Pull 21 swabs over 8 hrs to
recover 90 bbls. KCL water, mud and sand. Mud is dark grey
with sand in suspension. Wt. 11.9 #/gal. FFL @ 5200'.

S.I. @ 1900 hrs. LFLTR: 29 bbls.

(537,645)

34-06-06 (69) Moreno

Rig N₂ unit
0700 hrs SITP: 95 psi, SICP: 115 psi. Bleed off tbg & rig to
swab. IFL @ 4600'. Pull 6 swabs over 2 hrs to 6300' to recover
15 bbis muddy water w/ trace of sand. FFL @ 5600' very little
gas. Pump 10 bbis KCL water down csg annulus. New FL @ 5000'.
Pull 14 swabs over 7 hrs from 6300' to recover 15 bbis muddy
water. RIH w/ sinker bar to 6540'. No fill. FFL @ 5800'.
Very little gas S.I. @ 1700 hrs. LFLTR: 9 bbis
(540,305)

84-06-07 (70) Moreno

Displace hole with N2 0700 SICP: 245 psi, tbg press 0 psi (tbg left open for nite). RiH w/ swab to tag fiuld @ 5700 KB. Lower tbg to 6498. Rig N_2 & reverse circ hole to recover 7 bbls heavy mud and sand. Continue pumping N2 w/ no fluid recovery. Pull up & set packer so tailpipe at 6408'. Inject 20000 SCF N_2 to formation to 4500 psi. ISIP 4400 psi bleeding to 3100 psi in 15 mins. Open on 1/4" choke and recovered large amounts of sand. Tubing plugged off. Fill annulus w/ KCl water. Release packer and reverse circ hole with water. Recover 5 bbls heavy mud & sand. Re-set packer. Pull 2 swabs and flared gas for 30 mins with fair gas blow and tbg plugged off. Release packer & reverse w/ N_2 to recover 3 bbls heavy mud and sand. Ran out of N_2 . Set packer. Swab water from tbg Good gas blow for 15 mins then tbg plugged off again. Left tbg open to tank for nite. New fluid recovered to date 6 bbis.

84-06-08 (71) Moreno

Circulate hole w/ N₂
Tubing unloaded 5 bbls mud & sand @ 0400 hrs.
Faint blow of gas. RIH w/ sinker bar & unable to pass 100'KB. Unseat packer & reverse hole w/ N₂ to recover 5 bbls mud & sand. Lower tbg to 6490'KB & reverse out 2 bbls mud w/ N₂. Set packer @ 6458' & pump 50 MCF N₂ to perfs @ 4500 psi. Open to flow on 1/8" choke @ 1120 hrs. Pressure dropping steadily w/ trace of gas mixed w/ N₂. At 1800 hrs TFP 180 psi. Open on 1" choke. Well periodically died & flowed muddy water till 2300 hrs. S.I. @ 2300 hrs. Approx. new fluid rec'd today: 17 bbls. (555 941)

AHEL SOUZA #1 - FRESNO COUNTY, CALIFORNIA

(GAMACHE #11)

84-06-09 (72) Moreno

SI for B.U.

0700 hrs SITP: 614 psi (8 hrs S.i.) Blow down
on 1" choke for 2 hrs to recover approx. 3 bbls
watery mud & sand with trace of condensate. S.I. for
1 hr. Tbg built to 155 psi. Blow down on 1" choke
unseat packer and reverse hole w/ N2 to recover 2 bbls
watery mud. Reset packer leaving 960 psi N2 pressure
on annulus. Leave tbg open on 1" choke. TFP less than
10 psi, est. rate 50-75 MCFD. S.I. @ 1330 hrs & record
surface B.U. pressure as follows:

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30 mins - 120 psi
                      9 hr - 585 psi
1 he
        - 190 psi
                      10 hr - 630 psi
2 hr
        - 275 psi
                      11 hr - 675 psi
3 hr
        - 310 psi
                      12 hr - 690 psi
4 hr
        - 390 psi
                      13 hr - 730 psi
5 hr
        - 445 psi
                      14 hr - 750 psi
6 hr
        - 490 psi
                      15 hr - 790 psi
7 hr
        - 530 psi
                      16 hr - 800 psi
8 hr
        - 550 psi
                      17 hr - 820 psi
                      18 hr - 840 psi
                              (559 286)
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84-06-10 (73). Moreno

Running tbg. (GAMACHE #11)
Well S.I. total of 19.5 hrs. SITP: 890 psl. Blow
down on 1" choke. No fluid recovered. Unseat packer
& blow hole around w/ annular N2 pressure. No fluid
recovered. Reverse circ hole w/ 2% KCl water. POH w/
tbg. Rig Schlumberger & set EZ Drill BP @ 6400.7'KB.
PT to 2500 psi. Held OK. (562 251)

84-06-11 (74) Moreno

RIH w/ overshot.

RIH w/ tbg to 6400'. Rig Howco & blow hole dry w/
N2, POH w/ tbg. Rig Schlumberger & position gun
to shoot 6315-6330'KB. Pressure csg to 1000 psi w/
N2. Gun misfired. Reposition gun and shoot interval
6310-6315' @ 4 SPF. Unable to pull gun free. Bleed
off pressure and gun pulled free. Gun covered w/ mud.
Had small trace of gas at surface. Re-run gun and shoot
interval 6315-6330' @ 4 SPF. Gun blew uphole and
sheared off line leaving gun in hole. Gas blow increased
after shooting 6315-6330'. Flow well up casing on 1/8"
prover plate. Well died off in 1 hour. S.I.

(574 086)

.HEL SOUZA #1 - FRESNO COUNTY, CALIFORNIA

(GAMACHE #11)

84-06-12 (75) Moreno

Running Overshot

0700 hrs SITP: 15 psi. Bleed off to 0 psi. Pick up overshot & RiH on 2 3/8 tbg. Tag obstruction @ 6250' KB POH. No fish. Re-run overshot & circ. w/ KCL water to 6314' KB. Recovered mud & sand. POH. No Fish. Recovered strands of wire. RiH w/ barbed spear. POH, no fish (578.813)

84-06-13 (76) Moreno

Running tbg.

0800 hrs no press on WH. RIH with concave mill & mill over fish to cut line. Circ bottoms up. Recover pieces of electric line and gassy fluid. POH w/ tubing. Pick up overshot & RIH w/ 60 jts tbg. S.i. well to change out drilling line. (581 539)

84-06-14 (77) Moreno

Clean up well.

RIH w/ overshot. Attempt to latch fish without success.

POH & recover pieces of wire. RIH w/ overshot & jar down onto fish. POH w/ fish. RIH w/ Otis "XN" nipple, 1 jt tbg, Otis X nipple & reverse circulation hole w/ 2% KCI water to PBTD @ 6400' to recover mud & sand. Reland tbg @ 6285'. Rig in N₂ & displace hole with nitrogen. Open well to tank @ 2100 hrs. (589 222)

4-06-15 (78) Moreno

Clean up well. 0700 Gas TSTM. SICP 15 psi. Blow down with nitrogen. Recovered trace of mud. Displace 60,000 ft³ nitrogen into formation at 3700 SCF/min at 3800 psi. ISIP 3750 psi bleeding to 3510 psi in 15 mins. Bled down tubing. No flow from tubing when annulus pressure down to 250 psi. No formation gas. Bled off annulus. Unable to lower tubing. Pull 4 joints tubing with 40,000 lbs over string weight. Fill hole with KCI water. Clean out to 63501. Unable to go deeper. PBTD at 6400'. Steady gas to surface while reversing out sand, mud and drill cuttings. Land tubing at 61001. Displace with nitrogen. Inject 10,000 ft³ to formation at 3600 psi. Open on 1 inch choke. No fluid recovered. Tubing plugged off with 400 psi on annuius. Pressure annulus to 2500 psi. No flow. Left tbg open for night. (592 402)

AHEL SOUZA #1	- FRESNO COU	NTY, CALIFORNIA	(GAMACHE #11)
84-06-16	Moreno	Circulating well. 0700 Tubing dead. SICP 2500 psi. Blowith gas TSTM. Pull 12 joints at 20,0 over string weights before pulling out Establish circulation with KCI water. to 6440. Unable to go deeper. Circumud and chunks of cement and formation with foamed KCI water. Recovered large sand, chunks of rock and cement from px 1" in size. Circulate with foam to with nitrogen to 0400 hrs. Tubing plushut down. SICP 800 psi.	000 lbs t of debris. Circulate down llate out sand, rock. Circulate ge volumes of mud, bea size to 1/2" 0100 hrs. Circulate
84-06-17 (80)	Moreno	Well shut in. Crew released. 0800 SITP and SICP 800 psi. Cleaned of from choke and surface lines. Open tutwo inch. Tubing plugged with 400 psi Circulate with KCI water. Pull 60' wi over string weight. Circulate down 63 to go deeper. Tubing sticking. Pull tubing. Secure well. Release rig cre	ibing on on annulus. th 10,000 lbs 3351. Unable 16 joints
94-06-18 (81)	Moreno	Well shut in. Well shut in. Rig crew released.	(GAMACHE #11)
84-06-19 (82)	Moreno	Pull tubing. Well S.I.	(GAMACHE # 11)
84-06-20 (83)		Remove BOP's. 0800 hrs SITP 290 PSI. SICP 40 PSI. lower tubing to tag fill @ 6355' KB. Rig Howco and spot 6 bbls cement plug tubing to 6100' and backwash excess cement plug and pressure well to 800 PSI and tubing and tag top of cement plug @ 61 75 bbls 10.8 #/gal mud to 1500' KB. Pu Schiumberger and perforate 1399 - 1400 Howco and break circ up surface casing set plug from 1400' to 1200' in 9 5/8 Displace with 23 bbls water and 2 bbls 5' to 30' in 5 1/2 casing. SIFN. NOTE: Above operation witnessed by Ca	Reland tubing @ 6330'. across perfs. Puil ment. Pull tubing to WOC for 4 hrs. Lower 55' KB. Displace hole w/ li tubing. Rig ' w/4" casing gun. Rig Pump 15 bbls cement to and 5 1/2 casings. cement to set plug from

Commission.

NOTE: Above operation witnessed by California Oil & Gas

(634,039)

AHEL SOUZA #1 - FRESNO COUNTY, CALIFORNIA

84-06-21 (84)

Well plugged and abandoned. (GAMACHE # 11)
Remove BOP's and tubing spool. Cut off 9 5/8 and 5 1/2 casings
6' below ground. Weld plate on casings. Dug out conductor pipe
and fill cellar. Rig out rig. Transfer 231 jts tubing, packers
and nipples to R&R Transport and transfer wellhead and casing
bowl to Gray tool. Clean up location. Well abandoned.
FINAL REPORT. (641,000)

DRILLING HISTORY

07 10 04		SW 1/4, SE 1/4, SEC 36, T14S, R12E MDB & M FRES	NO CO CALIFORNIA
83-12-06 (32)	9778 Ft. Lathrop	POH w/DST # 8 Progress: Nil DST # 7: 9694' - 9777' (L/Lathrop) Times: 10/60 VO: 45 mins - lost packer seat - Misrun Used and rec. 3000' water cushion 1500' gas cut drig. mud. PF 1380 PSI IHP 5461 PSI ISIP 5590 PSI I 5238 Leaking at end. BHT - 227 ° F.	(MONT. 19) (497,424) F 1398 PSI 1586
83-12-07 (33)	9819 Ft Lathrop	Cut Core # 3 Progress: 41 Ft. CORE #3: Results to follow. DST # 8: 9652' - 9778' (L/Lathrop Used 3000' water cushion, lost packer seat im MISRUN. Rec: 3000' water cushion 793' gassy cut mud. IHP 5498 PSI 5350	(MONT. 19) (512,923) med. on preflow
		Trip gas after 8 mins was 9300 units.	• • •
83-12-08 (34)	10,000 Ft Lathrop	Drilling. Progress: 181 Ft. CORE # 3: 9778' - 9838' (L/Lathrop) Cut 60 Ft Rec. 60 ft	(MONT. 19) (535,256)
83-12-09 (35)	10,217' TD Lathrop	Rig to log. Progress: 217 Ft. 10,217' - 4 3/4°	(MONT. 19 (546,571)
33-12-10 (36)	10,217 Ft Lathrop	Logging. Progress: Nil	(MONT. 19) (554,104)
33-12-11 (37)	10,217 Ft Lathrop	Side cores. Progress: Nil	(MONT 19) (564,676)
33-12-12 (38)	10,217 Ft Lathrop	Lay down drill string. Progress: Nil	(MONT. 19) (619,742)

WELL SUMMARY REPORT

Attachment #3

Souza #1 - Fresno County, California

ELECTRICAL LOGS

DATE	RUN NO	HOLE DEPTH	LOGS RUN
Drilling Dep	oth - 7332	ft.	
Nov. 19/83	1	145 - 7257'	BHCS
Nov. 19/83	1	1709 - 7298'	DI-SFL
Nov. 19/83	1	145 - 7301'	LD-CN
Drilling Der	oth - 10,21	17 ft.	
Dec. 8/83	2	5900 - 10171'	BHCS
Dec. 8/83	2	1709 - 10137	NGR
Dec. 8/83	2	5900 - 10206	DI-SFL, DI-Linear Correlation Log
Dec. 8/83	2	5900 - 10203	LD-CN, Down Mud Log
Dec. 8/83	2	1709 - 10208	Dipmeter
Dec. 8/83	2	2400 - 10170	Microlog
Dec. 8/83	2 .	1709 - 10165	Electromagnetic Propogation Log
Drilling Dep	th - 10,17	7 ft.	
Apr. 3/84	1	2400 - 10149	CBL w./Neutron Waveforms
Apr. 3/84	1	2400 - 10149	CBL w./Neutron Variable Density
Apr. 4/84	2	2400 - 10149	CBL(B.I. + Waveforms)
Apr. 4/84	2	2400 - 10149	CBL(Amplitude + VDL)
Apr. 4/84	3	2400 - 10154	Acoustic Caliper Log w./Gamma Ray
Apr. 4/84	3	2400 - 10154	Cement Evaluation Log w./Gamma Ray
Apr. 4/84	4	2400 - 10153	Thermal Neutron Decay Time Log
Apr. 5/84	1	2400 - 10137	CNL
Apr. 10/84	1 (8000 - 9800 Depth-Driller 9800')	Free Point Indication Log
Apr. 14/84	4	2400 - 10153	TDT Quicklook
Apr. 16/84	3	9195 - 10150	CB-VD Waveforms
Apr. 17/84	3	9196 - 10150	Cement Evaluation Log/Acoustic Calipers

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EXPLORATION, LTD
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WOT EXPLICE VIEW NEW TIME.	SOUZA #1	Wildcat	Sol-Phon
	Well:	Field:	Drilling Fluid:

California	Fresno	Sec 36-T145-R12E
State:	Counts:	Location:

Date: 01 Jan 1984 TTCS File #: 423 Elevation: 451.8 KB

DEAN-STARK PLUG ANALYSIS

								The same area of the sa
		Permeability		OB Para	OB Para Porocity	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	£	The same streets desired analysis market control to the same streets and same same same same same same same same
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	(reet)	(Pd) (pd)	(F#)		\ <u>\</u>			
		:	2		(%)	(%) (%)	(00/85)	

LATHROP FORMATION

RECEIVED	APR 2 3 1984 BWISION OF OIL & TASE	1/shy	
Sd.vf-massltu.mic Sd.vf-massltu.mic Sd.vf-massltu.mic Sd.vf-fassltu.mic	Sd, vf-ma, sltw, mic Sd, vf-fa, sltw, mic Sd, vf-fa, sltw, mic Sd, vf-fa, sltw, mic Sd, vf-ma, sltw, mic	Sd.vf-mg.sltw.mic Sd.vf-mg.sltw.mic Sd.vf-mg.sltw.mic.sl/shw Sd.vf-mg.sltw.mic Sd.vf-mg.sltw.mic	Sd.vf-mas.slta.mic Sd.vf-ma.slta.mic Sd.vfa.lmu.slta.mic
2.65 2.65 2.65	2.65 2.65 2.65 2.65 2.65	2.65 2.65 2.65 2.65	2.65 2.72
61.8 68.3 71.6 77.7	72.8 82.0 74.0 78.1	77.0 76.4 81.7 79.3	77.6 79.1 83.2
8 7 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000	00000	0000
14.5 13.5 13.6	14.1 14.6 14.0 14.7	15.1 14.9 13.5 13.7	13.5 13.0 1.8
0.36 1.6 0.78 0.39	1.8	1.3	0,53
2.6 2.8 1.7 0.81	1.3 0.41 0.82 1.0	2.9 2.0 0.07 1.8 0.80	1,2 0,84 <0,01
3.7 3.7 2.0 0.88	2;1 3;1 3;8	2.6 0.69 2.6 1.2	1.5
9159.0-60.0 9160.0-61.0 9161.0-62.0 9162.0-63.0	9163.0-64.0 9164.0-65.0 9165.0-66.0 9166.0-67.0 9167.0-68.0	9168.0-69.0 9169.0-70.0 9170.0-71.0 9171.0-72.0	9173.0-74.0 9174.0-75.0 9175.0-76.0
→ 0 10 4	N 2 V 8 P	110	15 16 17

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AMERICAN HUNTER EXPLORATION,LTD Well: SDUZA #1

Date: 01 Jan 1984

TTCS File #: 423

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DEAN-STARK PLUG ANALYSIS

-									
elanes	Derth	Perme: Horz	Permeability Horz Vert	OB Perm	Porosity	Satur	Saturation		Lithology
Number	(feet) 	(pag)	(Bad)	2	(%)	(%)	17) (%)	vensity (sm/cc)	
ç					: -		 		enden erann spran erann james beneg erinne trades endes endes endes endes endes endes
æ •	9176.0-77.0	<0.01	0.01		4.		7	r	
19	9177.0-78.0		0.26		· M	•	0 (•	Sd,vfg,lmy,slts,mic
20	9178.0-79.0	0.56	0.45	•	? (0 0	9	4	Sd. < 1 - mas s 1 t.c. min
21	9179.0-80.0	0.44	3	CT *0	12.3	0.0	α	2.65	8 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
22	9180.0-81.0	+ c	₹		(0.0	82,8	9	UP-Pascitions
!	•	711	7.7		14.3	0.0	79.0	2,65	
23	9181.0-82.0	0.0	u						(8) TG (G) (A)
24	0182 0-01 0) ·	٠ ن		14.4	0.0	76.1	2.64	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	0.02.0-03.0	7.1	1.5		14.0	0.0		•	第6の27の27回 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1
C7	7183.0-84.0	1,00	1.4			•	•	ō	Sdrvf-marslts,mic
26	9184.0-85.0	0.87	70		7 .	0.0	-	~	-
27	9185.0-86.0	20.0	0 ? ?		12.6	0.0	_	~0	
	?	?	0000		2.1	0.0	92.9	2.69	v. maruskurmir Venfaseltaspin.lp
28	9184 0-07 0	r							TATELON TABLE
200	0.40.0.017	0.31	0.34		9.8	0.0	93.0		
4 1	110/10-88-0	0.12	60.0	0.02	13.4	0			1515151
20	9188.0-89.0	0.61	0.31	•		•	ч .		Sd,vffg,slty,mic
31	9189.0-90.0	0.10	0		7:11	0.0	_		Sdyvf-fs,slts,mic
32	9190.0-91.0	200) () (7.2	0.0	92.3	2.67	d, vf - fq, <] + u · m ·
		```	2		8 • 9	0.0	<b>M</b>	2.67	0,00 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -
33	9191,0-92,0	0.84	0.72		,				
34	9192.0-93.0	20.0	4		11.4	0:0	74.0	2,65	Sd. of fast 1 tuesio
35	9193.0-94.0	3 6	· · ·	•	11.8	0.0	73.0	2,65	**************************************
36	0104 A-05 A	7.0	0.13	0+02	11.2	0.0	•	2.68	
12	0.000.0000	***	0.45		11,1	0.0		57.6	
ò	0.94-0.6414	1.4	1+1		12.4		_	20,0	VI-BS/SIts/BI
II Î					- - -	•	_	2,65	Sd, vf-mg, slty, mic
00   10 1	196.0-97.	0.83	1.0		12.7	<	•	•	!
5.0	9197.0-98.0	1.4	<i>y</i>		, 11 -	•		ō	Sd, vf-fg, sltw, mic
			<b>b</b> .		T	0.0	76.1	2+65	

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AMERICAN HUNTER EXPLORATION,LTD Well: SOUZA #1

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DEAN-STARK PLUG ANALYSIS

Sample	Derth (feet)	Permes Horz (md)	Permeability Horz Vert	OB Perm 4900 PSI (md)	Forosity (X)	Satura Oil (%)	ration H20 (%)	Grain Density (Sm/cc)	
J	0108 0 - 0 000			     					ands only was been man man one that the train of the same was the same
. •									Shale
40	-0	0.47	0.11			•			Drilled Interval
41	9727.0-28.0		7		12.4	0	72.4	2+65	() Slts, mi
4	9728 0-20 0	) (	· ·		12.1	0.0	82.7	2.64	
7 V	0220.0277	٠. ا	1.4		11.7	0.0	79.7	2,63	
? F	7727+0-20+0	1.7	1.7	0.12	12.1	0.0	85.3	2.63	
44	9730.0-31.0	0.49	0.41		4			•	
45	9731.0-32.0	0.1	70		12.0	) )	6.6/	2.64	Sd,f-ma,slts,mic
46	0.77-0.0226	? c			12,1	0.0	80.6	2.63	f-mays]ts,m;
47	0.725 0.725 0	717	\\\·0		11.8	0.0	82.8	2.64	P-84.61+0
) (I	0.140101017	0.0	0.05	< 0.01	12.2	0.0	75.0		
r D	7/34.0-55.0	£0.0	0.01		11,1	0.0	87,6	2.69	F 835
46	9735.0-36.0	0.08	90.0		7 7				
50	9736.0-37.0	0.21	0.03	· ·	\ C	) (		•	Sd,f-masslts,mic
51	9737.0-38.0	7	) (		* · 7 T	0.0	84.8	_	Sd,f-ms,slts,mic
5.5	0728 0-70	7110	71.0		12,3	0,0	85.0	-	MS . S. L. C. B.
2 12	0720 0770	n •			13.0	0.0	84.1	_	
3	0+0+0+0	4.	4.4		13.1	0,0	84.0	2.62	carsity
54	9740.0-41.0	4.7	6.3		1 1	<	į	•	
55	9741.0-42.0	7.4	· ·	<b>6</b>		•	ים מ	ó	Sd,f-ca,slty,mic
56	9742.0-43.0	0.0	7 0 7		17:0	0	86.1	ò	f-carslty, mi
57	9743.0-44.0		) (		13.2	0	81.2	٠	P-cs,slts,m
α	0744 0=45	ָ פֿין	7 i		12.4	0	85.8	4	P-castons.
3	0.04-0.44.7	3	4		12.5	0.0	87.8	2.62	-carsity.mi
29	9745.0-46.0	3.4	64 63	0.17	12.1	0.0	85.4	2.62	Sdof-cassitsomic

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TTCS File #: 423

	3	ביים ביים			710-925-52
AMERICAN HUNTER EXPLORATION,LTD Well: SOUZA #1		Date: 01 Jan 1984	01 Jan	1984	TTCS F
	DEAN-STARK PLUG ANALYSIS	R PLUG A	MALYSI		

Horz Vert 4900 PSI (Z) (Z) (Ed) bensity (md) (md) (md) (Z) (Z) (Z) (Z) (Z) (Z) (Z) (Z) (Z) (Z	:	Perme	Permeability	08 Perm	Porosita	13			
1.5	I	Horz (md)	Vert (md)	g	(%)	<b>&gt;</b>	ration H20 (%)		Litholosy
1.6		<i>ir</i>	•		ı	! 			
1.8		7	ų <		Ň	0.0	83.2	•	**************************************
1.0		9 0	7.1		÷	0.0	87.2		
3.6         3.8         12.1         0.0         87.6         2.62         Sdrf-massitusming           2.5         2.3         11.8         0.0         86.3         2.62         Sdrf-massitusming           0.49         0.44         0.37         11.5         0.0         88.2         2.65         Sdrf-massitusming           0.49         0.44         0.37         11.5         0.0         88.0         2.65         Sdrf-massitusming           0.08         0.07         10.9         0.0         88.0         2.65         Sdrf-massitusming           0.12         0.06         12.2         0.0         86.3         2.65         Sdrf-massitusming           0.12         0.05         12.2         0.0         86.3         2.65         Sdrf-massitusming           0.11         0.77         0.72         12.7         0.0         81.2         2.65         Sdrf-massitusming           0.68         0.67         12.5         0.0         81.2         2.66         Sdrf-massitusming           1.1         0.93         0.06         12.5         0.0         86.8         2.65         Sdrf-massitusming           0.55         0.27         0.27         12.7         0.	_	, i	0.00		å	0.0	91.9	٠.	
3.0         2.3         11.8         0.0         86.3         2.62         SGyf-massltsninc           0.49         0.44         0.03         11.5         0.0         89.2         2.65         SGyf-massltsninc           0.49         0.44         0.03         11.6         0.0         86.3         2.65         SGyf-massltsninc           0.08         0.07         11.5         0.0         88.0         2.65         SGyf-massltsninc           0.12         0.05         10.9         0.0         86.3         2.65         SGyf-massltsninc           0.12         0.06         12.2         0.0         86.3         2.65         SGyf-massltsninc           0.12         0.05         12.5         0.0         86.3         2.65         SGyf-massltsninc           0.11         0.05         12.5         0.0         86.3         2.66         SGyf-massltsninc           0.68         0.67         12.5         0.0         86.8         2.65         SGyf-massltsninc           1.6         1.5         0.0         86.8         2.65         SGyf-massltsninc           0.50         0.27         12.7         0.0         85.8         2.65         SGyf-massltsninc		0 i			ż	0.0	87.4		71 - 53 5 1 1 3 7 5 1
2.5 2.1 11.5 0.0 89.2 2.62 Sdyf-mayslty-mic 0.49 0.37 11.6 0.0 86.3 2.65 Sdyf-mayslty-mic 0.44 0.37 11.6 0.0 86.3 2.65 Sdyf-mayslty-mic 0.08 0.07 0.00 0.00 0.00 0.00 0.00 0.00	_	3.0	2+3		7	0.0		• •	rreg.sltu.e; f.ex.sltu.e;
0.49 0.44 0.03 11.5 0.0 89.2 2.62 Sdyf-maysltymic 0.44 0.37 11.6 0.0 86.3 2.65 Sdyf-maysltymic 0.08 0.07 11.5 0.0 88.0 2.65 Sdyf-maysltymic 10.08 0.07 10.9 0.0 89.4 2.67 Sdyf-maysltymic 11.2 0.06 12.5 0.0 86.3 2.66 Sdyf-maysltymic 0.77 0.72 12.7 0.0 86.3 2.66 Sdyf-maysltymic 12.8 0.0 87.3 2.64 Sdyf-maysltymic 12.9 0.0 81.2 2.64 Sdyf-maysltymic 12.9 0.0 83.5 2.64 Sdyf-maysltymic 12.9 0.0 85.8 2.65 Sdyf-maysltymic 0.55 0.27 0.01 12.7 0.0 85.8 2.65 Sdyf-maysltymic 5.2 0.0 90.5 2.65 Sdyf-maysltymic 5.2 0.0 88.2 2.65 Sdyf-maysltymic 5.2 0.0 90.5 2.65 Sdyf-maysltymic 5.2 0.0 87.8 2.65 Sdyfaysltymic 5.2 0.0 87.8 2.65 Sdyfaysl		2,5	2.1		,				
0.44 0.37 0.03 11.6 0.0 86.3 2.65 Sdyf-masistymic 0.08 0.07 0.07 11.5 0.0 88.0 2.65 Sdyf-masistymic 0.08 0.07 0.05 10.9 0.0 89.4 2.67 Sdyf-masistymic 0.12 0.06 12.2 0.0 89.4 2.67 Sdyf-masistymic 12.1 0.09 0.00 87.3 2.66 Sdyf-fasistymic 12.1 0.09 0.00 87.2 2.66 Sdyf-fasistymic 12.2 0.0 87.3 2.64 Sdyf-masistymic 12.2 0.0 87.5 2.64 Sdyf-masistymic 12.2 0.0 87.5 2.64 Sdyf-masistymic 12.9 0.0 87.5 2.64 Sdyf-masistymic 12.9 0.0 85.8 2.65 Sdyf-masistymic 10.5 0.07 0.09 0.01 14.0 0.0 88.2 2.65 Sdyf-masistymic 10.5 0.00 99.5 2.65 Sdyf-masistymic 10.5 0.00 97.2 2.65 Sdyf-masistymic 10.5 0.00 88.2 2.65 Sdyf-masistymic 11.0 0.08 0.10 88.2 2.65 Sdyf-masistymic 11.0 0.08 0.10 Sdyf-masistymic 11.0 0.0 93.4 2.67 Sdyf-masistymic 11.0 0.0 93.4 2.67 Sdyf-sitymic 11.0 0.0 93.4 2.65 Sdyf-sitymic 11.0 0.0 93.		0.40	7 7 7		→ .	0.0	0	•	f-monstermi
0.12 0.05   11.5 0.0 88.0 2.65 Sdrf-massitysmic 0.12 0.06   12.2 0.0 86.3 2.65 Sdrf-massitysmic 12.2 0.0 86.3 2.66 Sdrf-massitysmic 12.2 0.0 85.3 2.66 Sdrf-massitysmic 12.5 0.0 83.3 2.64 Sdrf-massitysmic 12.5 0.0 83.5 2.64 Sdrf-massitysmic 12.5 0.0 83.5 2.64 Sdrf-massitysmic 12.9 0.0 83.5 2.64 Sdrf-massitysmic 12.9 0.0 85.8 2.65 Sdrf-massitysmic 12.9 0.0 85.8 2.65 Sdrf-massitysmic 12.7 0.0 85.8 2.65 Sdrf-massitysmic 12.7 0.0 85.8 2.65 Sdrf-massitysmic 12.7 0.0 85.8 2.65 Sdrf-massitysmic 10.5 0.0 90.5 2.66 Sdrf-massitysmic 10.5 0.0 94.2 2.65 Sdrf-massitysmic 11.0 0.08 0.10 14.0 0.0 88.2 2.65 Sdrfsssltysmic 11.0 0.08 0.10 88.7 2.65 Sdrfsssltysmic 11.0 0.08 0.10 85.7 2.65 Sdrfsssltysmic 11.0 0.0 93.4 2.67 Sdrfsssltysmic 11.0 0.0 93.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0			· · · ·	•	-	0.0	ð	2,65	
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0.68 0.67 0.00 12.5 0.0 81.2 2.64 Sdyf-maysltynmic 12.9 0.0 83.5 2.64 Sdyf-maysltynmic 12.9 0.0 85.8 2.63 Sdyf-maysltynmic Sdyf-maysltynmic 5.2 0.0 90.5 2.65 Sdyf-maysltynmic shy 10.5 0.07 0.09 0.01 14.0 0.0 88.2 2.65 Sdyf-maysltynmic Shale 5.2 0.0 94.2 2.65 Sdyf-maysltynmic Shale 5.2 0.0 94.2 2.65 Sdyf-maysltynmic 5.1 0.08 0.10 12.5 0.0 85.7 2.65 Sdyfsysltynmic 5.1 11.0 0.0 93.4 2.67 Sdyfsysltynmic 5.1 Shy 5.1 5.1 5.1 5.1 5.1 5.1 5.1 5.1 5.1 5.1		-	70.0		Ň,	0.0	-		0.4-34.240.34
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			• •		>	•	÷	2.67	difsisitsim

University Research Park - 360 Wakara Way - Salt Lake City, Utah 84108 - (801) 584-2480 - TWX 910-925-5284

AMERICAN HUNTER EXPLORATION, LTD Well: SOUZA #1

Date: 01 Jan 1984

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Lithology	Sd.f-cs.slts.mic	ot Recovered d,f-ms,slts,mi d,f-ms,slts,mi	0,7-m3,51tg,m1 d,f-m4,51tg,m1 d,f-m4,61,0,m1	d, fs, sltuelc d, fs, sltuelc d, fs, sltuelc d, fs, sltuelc	d,f=ms,slty,mi d,f=ms,slty, d,f=ms,slty, d,f=ms,slty,	Sd,f-mg,slty,mic Sd,f-mg,slty,mic Sd,fg,slty,mic Sd,fg,slty,mic Sd,vf-fg,slty,mic,lmy	slts,mic,v/
Grain Density (Sm/cc)	2.62		7 E E	א מז מז י	25.44 TV	2.64 2.65 2.65 2.66 2.66 8.88 8.88	2.70 5.2.69 5
ation H20 (%)	95.5	78.1	80.08 80.88	73.1 71.9 80.7	73.2 70.2 70.3 70.2 89.1	76.8 75.7 76.4 82.4 89.7	72.3
Satur Oil (%)	0.0	000	000	000	00000	00000	0.0
Porosity (%)	13.9	12.7	13.7	12.7 13.5 12.9	12.5 12.7 12.7 12.5	12.1 12.1 11.4 9.8 6.3	1.8
OB Perm 4900 PSI (md)		0.07	0 • 55		0.13	0.03	
oility Vert	2.9	0.62	8.5 8.5	0.34 0.35 0.05	0.07 0.50 1.6 0.48	0.60 0.45 0.23 0.13	0.02
Fermeability Horz Vert (md) (md)	8.8	0.73 0.58 26+	5.2	0.21 0.48 0.08	0.14 0.76 1.6 0.65	0.49 0.83 0.13 0.24	0.02
Derth (feet)	9770.0-71.0	.0-79.0 .0-80.0	9781.0-82.0 9782.0-83.0	7783.0-84.0 9785.0-85.0	9786.0-87.0 9787.0-88.0 9788.0-89.0 9789.0-90.0	9791.0-92.0 9792.0-93.0 9793.0-94.0 9794.0-95.0 9795.0-96.0	9796.0-97.0 9797.0-98.0
Sapele	81	83 84	85 86 07	88 88	90 93 94	95 96 98 99	100

⁺ Horizontal dehydration crack

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	Uni AMERICAN HUNTER Well:	iversity Rese EXPLORA: SOUZA:	University Research Park - 360 ER EXPLORATION,LTD SOUZA #1		y - Salt Lake C	Sity, Utah 8 1 Jan 1	84108 - (80 [,]	1) 584-2480 - T	Wakara Way - Salt Lake City, Utah 84108 - (801) 584-2480 - TWX 910-925-5284  Date: 01 Jan 1984  TICS File #: 423	Pase 6
   				DEAN-SIARK	PLUG	ANALYSIS				
Sample Number	Derth (feet)	Permea Horz (md)	Permeability Horz Vert (md) (md)	0B Perm 4900 PSI (md)	Porosity (2)	Satura Oil (%)	ation H20 (Z)	Grain Density	Lithology	
102	9798.0-99.0	1.0	0.62	0.12	13.5	0.0	79.5			-
103	9800.0-01.0	3,0	6		•	•	,	<b>404</b>	SOFTWANDICATION STATES	
104	9801.0-02.0	2:5	, <del>-</del>		13.1	0.0	73,7	2,63	֓֞֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	
105	9802.0-03.0	2.4	2.3		12,9	0 0	74.7	2.64	Sd,f-mg,slty,mic	
104	0007 0 00				•	?	/•08	2.63	Sd,f-ms,slts,mic	
107	9804.0-05.0	⊶ c œ c	5,3		13.4	0.0	75.5	2.64		
108	9805.0-06.0	7 7 0	1.6		13.0	0.0	76.9	2,63	フロン・一三などの1のかを到している。 かんしん アン・ディン・ディン・ディン・ディン・ディン・ディン・ディン・ディン・ディン・ディ	
109	9806.0-07.0	2 0	\ • • • •	,	13.0	0.0	74.0	2.64		
110	9807 \$ 0-08.0		40.0 4.0	0.15	; ,	•	0	2,62	1 01 6	
			7 •		12,3	0.0	84,6	2.64	1 101	
111	9808.0-09.0	3.7	ϥ		* * *	<			7 E 7 F 7 F 7 F 7 F 7 F 7 F 7 F 7 F 7 F	
112	9809,0-10,0	3.6	2.7	56.0	10 T	0.0	86.1	2.63	Sd,f-mg-slts,mic	
113	9810.0-11.0	4.3	4.1		13,7	0 0	84. 5	2,63	* print	
114	9811.0-12.0	0.53	0.46		٠ . د . د .	0.	85.9	2,62	51ts.	
115	9812,0-13,0	0,38	0.27		42.4	o .	20.6	2.64	ū	
			<u>.</u>		1604	0.0	81,5	2.64	3.51ts.mi	
116	9813.0-14.0	2.1	2.0		+ 5	<		·		
11/	9814.0-15.0	0.13	0.13	0.015	17.1	) ·	`	2,62	Sd,f-ms,slty,mic,sl/lmu	
8 :	9815.0-16.0	0.27	0.24	) • •	13,66	0.0	81,4	2.64	sh stk	
119	9816.0-17.0	90.0	0.08		10°C	٠ • •	81,7	2.64		
120	9817.0-18.0	0.02	0.02		11,2		91.4	2,67	nic, s	ks
121	9818.0-19.0	1-1 (C)	6.		)    -  -	<b>&gt;</b>	ï	/017	Sdrvfs,sltv,mic,sh lam &	2 stks

Sd.f-ma.sltv.mic.sh stks Sd.f-ma.sltv.mic

2.62

79.7

0:0

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1.2

9818.0-19.0 9819.0-20.0

121 122

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AMERICAN HUNTER EXPLORATION,LTD Well:

Date: 01 Jan 1984

423 TTCS File #:

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	Sd:f-masslts:mic	Sh.sl/sdw Sd.f-ca.sltw.mic Sd.f-ca.sltw.mic	Sd.f.ma.slts.mic Sd.f.ma.slts.mic Sd.f.ma.slts.mic.sh stks Sd.fa.slts.mic Sd.fa.slts.mic	Sd,f-ms,slts,mic Sd,f-ms,slts,mic Sd,fs,slts,mic Sd,fs,slts,mic Sd,fs,slts,mic
	Sd.f-ms	Sdrf-cars	SQ 2 C C C C C C C C C C C C C C C C C C	Sd, f-ma, sltw, m Sd, fa, sltw, mic Sd, fa, sltw, mic Sd, vf-fa, sltw,
Grain Density (sm/cc)	2.62	2.61 2.61 2.60	22.653	22222 2465 265 265 265 265
ation H20 (%)	81.2	89.58 85.3	79.8 82.7 91.0 91.9	92.4 88.0 93.0 87.7 92.9
Saturation Oil H2O (%) (%)	0.0	000	00000	00000
Porosity (%)	13.4	13.2 13.8 12.8	12.7 11.6 12.1 11.2	11.8 12.0 11.7 12.0 11.5
OB Perm 4900 PSI (md)	0.58	1. 5.	0.51	0
vility Vert	4 5.	9.7 28 6.4	3.0 0.62 0.09 10	2.6 0.90 0.08 0.12 0.06
Permeability Horz Vert (md) (md)	4.3	9.8 27 26	3.1 0.49 0.10 0.06	2.0 0.74 0.10 0.13 0.03
Depth (feet)	9820.0-21.0 9821.0 - 9823.0	9823.0-24.0 9824.0-25.0 9825.0-26.0	9826.0-27.0 9827.0-28.0 9828.0-29.0 9829.0-30.0	9831.0-32.0 9832.0-33.0 9833.0-34.0 9834.0-35.0 9835.0-36.0
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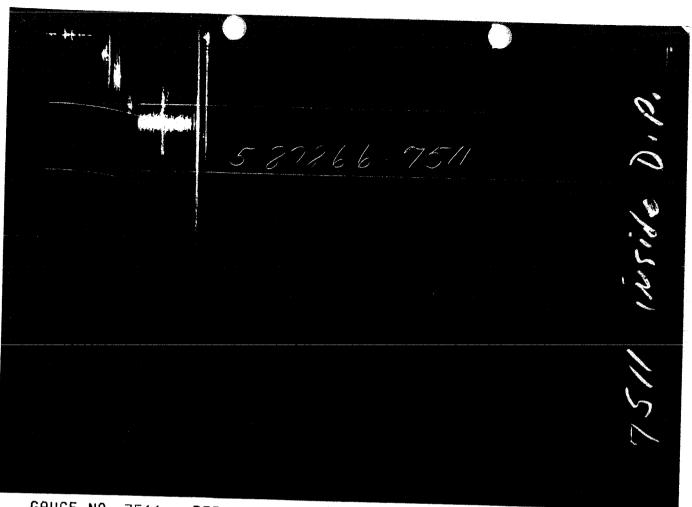
DIVISION OF OIL & GAS COAUNGA

FORMATION LESTING SERVICE REPORT

TESTED INTERVAL AMERICAN HUNTER EXPLOR

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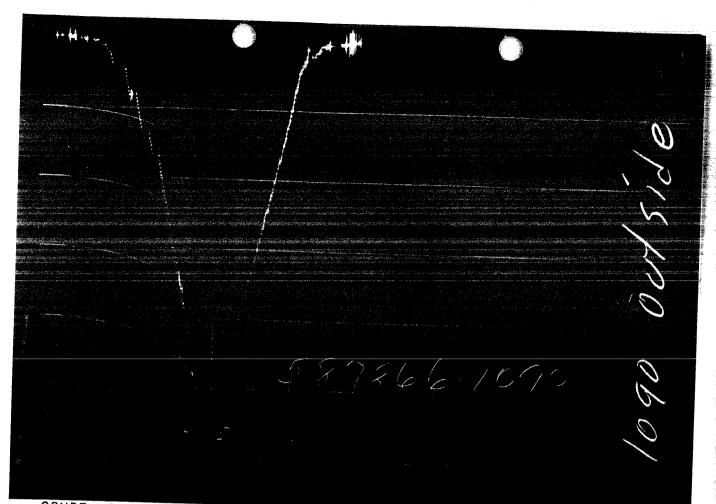


ь Г		E NO: 7511 DEPTH: 9618.0	BLANKED OFF:_	NO HOUR OF CLOCK	: 24
L	ID	DESCRIPTION	PRESSURE	TIME	<del></del>
	A	INITIAL HYDROSTATIC	REPORTED CALCULATED	REPORTED CALCULATED	TYPE
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GAUG	E NO: 641 DEPTH: 9634.0	BLANK	KED OFF:_	NO HOUR OF	0.00
ID	DESCRIPTION	PRE:	SSURE	TIME	CLOCK: 24
А	INITIAL HYDROSTATIC	REPORTED   5469	CALCULATED 5419.4		LCULATED TYPE
В	FINAL HYDROSTATIC	_	5419.4		

24 E



	JGE NO: 1090 DEPTH: 9770.0	BLAN	KED OFF:Y	ES HOUR OF CLOCK:_	
I	DESCRIPTION	PRE	SSURE	TIME	
F	INITIAL HYDROSTATIC	REPORTED 5455	CALCULATED 5484.4	REPORTED CALCULATED TY	PE
E	FINAL HYDROSTATIC	5308	5484.4		_

GAUG	SE NO: 7512 DEPTH: 9774.0				
ID	DESCRIPTION		KED OFF:Y	ES HOUR O	F CLOCK: 24
A	INITIAL HYDROSTATIC	KEPORTED	SSURE CALCULATED	IME	
В	FINAL HYDROSTATIC	5498	5485.0	- SWIED E	ALCULATED TYPE
	THIE	5350	5485.0		

EQUIPMENT & HOLE DATA	AND THE RESIDENCE OF THE SECOND SECON
* ************************************	- ' ''O'' O'' LI''
NET PAY (ft): GROSS TESTED FOOTBGE.	DATE: 12-6-92 750-
GROSS TESTED FOOTAGE:	DATE: 12-6-83 TEST NO: 8
ALL DEPTHS MEASURED FROM: KELLY BUSHING CASING PERFS. (ft): HOLE OR CASING SIZE (t.)	TYPE DST: OPEN HOLE
ELEVATION (ft): 8.750  TOTAL DEPTH (ft): 0	HALLIBURTON CAMP: BAKERSFIELD
FINAL SURFACE CHOKE ( )	I ESTER: TONS
MUD WEIGHT (1b/gal): 0.750  MUD VISCOSITY (sec): 10.40	WITNESS: WALT ZURBA
ACTUAL HOLE TEMP. (°F): 120 @ 9777 0 64	
FLUID PROPERTIES FOR RECOVERED MUD & WATER SOURCE RESISTIVITY CHLORIDES	SAMPLER DATA Pstg AT SURFACE: cu.ft. OF GAS: cc OF OIL: cc OF WATER:
REMARKS:	MEASURED I
LOST PACKER SEAT	•

TYPE & SIZE MEASURING DEVICE: _ TICKET NO: 58786600 SURFACE PRESSURE PSI GAS RATE MCF CHOKE SIZE LIQUID RATE BPD TIME REMARKS 12-6-83 0423 OPENED HYDROSPRING 0424 NO PACKER SEAT, PULLED LOOSE

				TICKET NO. 587866		
		0.0.	I.D.	LENGTH	DEPTH	
ı E	DRILL PIPE					
50		5.000	4.276	9338.0		
3	IMPACT REVERSING SUB	6.000	3.000	1.0	9339.0	
5	DRILL COLLARS	6.000	3.000	273.0	_	
11	CROSSOVER	6.000	3.000	0.9		
80	AP RUNNING CASE	5.750	2.250	4.6		
13	183	5.000	3.000	4.2	9618.0	
60	DUAL CIP SAMPLER	5,000	0.750	7.0		
во	HYDROSPRING TESTER	5.000	0.750	5.0	9629.0	
15	AP RUNNING CASE	5.000	3.000	4.2	9634.0	
16	JAR	5.000	1.750	5.0		
	VR SAFETY JOINT	5.000	1.000	2.8	:	
70	OPEN HOLE PACKER	7.750	1.530	5.8	9646.0	
70	OPEN HOLE PACKER	7.750	1.530	5.8	9052.0	
20	FLUSH JOINT ANCHOR	5.000		4.∠		
81	BLANKED-OFF RUNNING COSE		2.370			
81 6	BLANKED-OFF RUNNING COOF	.000		4.6	9770.0	
82	TEMPERATURE RUNNING CO.	.000		3.9	9774.0	
<u>IIII</u>	5	.000	2.440	4.1	9777.0	
Т	OTAL DEPTH				.	
					9778.0	
					1	

## 587866- TE 68

Temp

75.68

## - AIVALYSIS

Indicated Flow Capacity

$$kh = \frac{1637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

S = 1.151 
$$\left[ \frac{m(P^*) - m(P_f)}{m} - LOG \frac{kt}{\phi \mu c_f r_w^2} + 3.23 \right]$$
 —

Damage Ratio

$$DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 \text{ mS}}$$

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g \ m(P^*)}{m(P^*) - m(P_f)}$$

MCFD

Indicated Flow Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$$

MCFD

Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{kt}{-\phi\mu c_t}}$$

ft



TICKET NO. 58786500 15-DEC-83 BAKERSFIELD

RECEIVED

APR 2 3 1984

FORMATION TESTING SERVICE REPORT

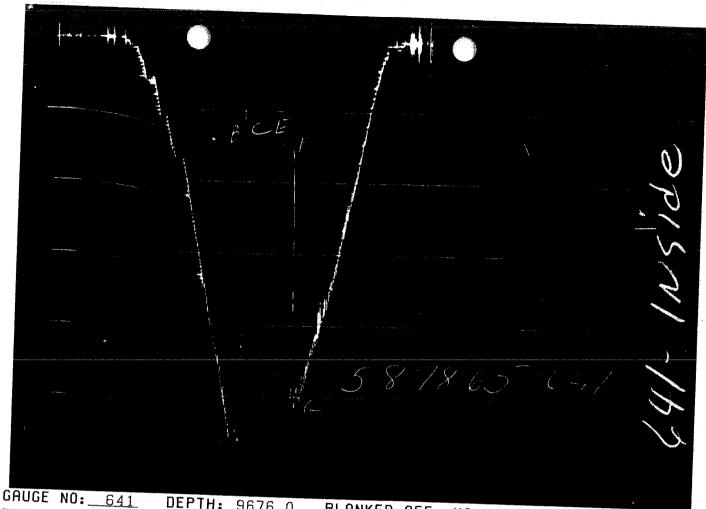
D19-21924 NO. TEST NO. CHANNEY RANCH TESTED INTERVAL 9778 HUNTER EXPLORATION LIMITED CALIFORNIA

LEASE NAME

587865 7511

pic

GAUGE NO: 7511 DEPTH: 9660.0 BLANKED OFF: NO HOUR OF CLOCK: 24 ΙD DESCRIPTION PRESSURE TIME
REPORTED | CALCULATED REPORTED CALCULATED TYPE A INITIAL HYDROSTATIC INITIAL FIRST FLOW В 1323 1294.2 FINAL FIRST FLOW С 10.0 10.6 F 2021 1294.2 INITIAL FIRST CLOSED-IN  $\mathbb{C}$ 2021 1294.2 FINAL FIRST CLOSED-IN D 60.0 59.4 С 1339.1 Ε INITIAL SECOND FLOW 1339.1 FINAL SECOND FLOW F 45.0 39.1 F 1508.7 FINAL HYDROSTATIC G



	GE NO: 641 DEPTH: 9676.0	BLAN	KED OFF:_	NO HOUR	OF CLOCK	
ID	DESCRIPTION	PRE	SSURE	7	ME CLUCK	
A	INITIAL HYDROSTATIC	REPORTED	CALCULATED	REPORTED	CALCULATED	TYPE
В	INITIAL FIRST FLOW	5543	5463.4			
		1345	1387.6			
-	FINAL FIRST FLOW	1345	1381.7	10.0	10.6	F
С	INITIAL FIRST CLOSED-IN	1345	1381.7	-		
D	FINAL FIRST CLOSED-IN	5561		60.0	59.4	С
Ε	INITIAL SECOND FLOW		5575.9			
F	1	1364	1399.4	45		
	FINAL SECOND FLOW	1530	1580.2	45.0	39.1	F
G	FINAL HYDROSTATIC	5177	5132.4			
		The same of the sa	0.00.4			

GAUGE NO: 1090 DEPTH: 9770.0 BLANKED OFF: YES HOUR OF CLOCK:

ID DESCRIPTION PRESCUPE HOUR OF CLOCK:									
DESCRIPTION	PRE				T				
INITIAL HYDROSTATIC			REPORTED	CALCULATED	TYPE				
		5463.4							
	1371	1469.4							
FINAL FIRST FLOW	1371	1415.2	10.0	10.6	F				
INITIAL FIRST CLOSED-IN	1371								
	_		60.0	50 /					
	5566	5586.4		55.4	С				
INTITHE SECOND FLOW	1389	1434.7							
FINAL SECOND FLOW	1575	1625 B	45.0	39.1	F				
FINAL HYDROSTATIC									
	5235	5136.2							
	INITIAL HYDROSTATIC  INITIAL FIRST FLOW  FINAL FIRST FLOW  INITIAL FIRST CLOSED-IN  FINAL FIRST CLOSED-IN  INITIAL SECOND FLOW	DESCRIPTION REPORTED  INITIAL HYDROSTATIC 5455  INITIAL FIRST FLOW 1371  FINAL FIRST CLOSED-IN 1371  FINAL FIRST CLOSED-IN 5566  INITIAL SECOND FLOW 1389  FINAL SECOND FLOW 1575	DESCRIPTION PRESSURE REPORTED   CALCULATED  INITIAL HYDROSTATIC 5455 5463.4  INITIAL FIRST FLOW 1371 1469.4  FINAL FIRST CLOSED-IN 1371 1415.2  INITIAL FIRST CLOSED-IN 5566 5586.4  INITIAL SECOND FLOW 1389 1434.7  FINAL SECOND FLOW 1575 1625.8	DESCRIPTION  REPORTED CALCULATED REPORTED  INITIAL HYDROSTATIC  INITIAL FIRST FLOW  FINAL FIRST FLOW  INITIAL FIRST CLOSED-IN  FINAL FIRST CLOSED-IN  INITIAL FIRST CLOSED-IN  FINAL FIRST CLOSED-IN  INITIAL SECOND FLOW  FINAL SECOND FLOW  TIME HYDROSTATIC  TIME HYDROSTATIC  TO ALCULATED REPORTED  REPORTED CALCULATED  REPORTED CALCULATED  REPORTED  FINAL SECOND FLOW  1371 1415.2  60.0  45.0  FINAL SECOND FLOW  1575 1625.8	DESCRIPTION         PRESSURE REPORTED   CALCULATED REPORTED   CALCULATED   CA				

	E NO: 7512 DEPIH: 9//4.0	_ BLAN	KED OFF:Y	ES HOUR	OF CLOCK	: 24
ID	DESCRIPTION	PRE	SSURE		ME	
	Thirty	REPORTED	CALCULATED	REPORTED	CALCULATED	TYPE
A	INITIAL HYDROSTATIC	5461	5463.5			
В	INITIAL FIRST FLOW	1380	1476.2			
C	FINAL FIRST FLOW	1380	1422.1	10.0	10.6	F
С	INITIAL FIRST CLOSED-IN	1380	1422.1			
D	FINAL FIRST CLOSED-IN	5590	5585.9	60.0	59.4	С
Ε	INITIAL SECOND FLOW	1398	1443.8	1		
F	FINAL SECOND FLOW	1586	1633.7	45.0	39.1	F
G	FINAL HYDROSTATIC	5238	5144.6			
			<u>-</u>			

	EQUIPMENT & HOLE DATA	
	FURMHIION TESTED:	TICKET NUMBER: 58786500
	NET PAY (ft):	DATE: 12-5-83 TEST NO: 7
	MLL DEPIHS MEASURED FROM. KELLY BUCLING	TYPE DST. OPEN HOLE
	CHOING PERFS. [ft]:	OFEN HULE
	HOLE ON CHOING DIZE [in]: Q 7EA	HALLIBURTON CAMP:
I	CLEVHIIUN (ft):	BAKERSFIELD
	101AC DEFIN (11): 0770 A	
Ì	1 11CNCN DECIDIO1   1 1 1 1 0 0600 0604	I IFSTER
	I INDE SUKTHEE CHIKE (45).	
	DOTTON HOLL CHUKE (In):	
	10 40 10 10 40	"A INCOO.
- 1	non Alornolla (sec):	
i	rairuuien unte lemb" lobl"	IDRILLING CONTRACTOR.
H	ncture nule temp. (°F): 227 @ 9778.0 ft	MONTGOMERY
ı	LUID PROPERTIES FOR	
	RECUVERED MOD & WATER	SAMPLER DATA
	SOURCE RESISTIVITY CHLORIDES	Pstg AT SURFACE:
-	6 of DOM	cu.ft. OF GAS:
	0 °F	cc OF OIL:
	8 ppm	CO OF WOTER
		cc OF WATER:
1-		cc OF MUD:
<b> </b>		TOTAL LIQUID cc:
	HYDROCARBON PROPERTIES	CUSHION DATA
0	IL GRAVITY (OAPI).	TYPE AMOUNT WEIGHT
_	AS/OIL RATIO (cu.ft. per bbl):AS GRAVITY:	WATER (FEET) 3000.0 8.33
	ECOVERED:	
	3000 FEET OF WATER CUSHION	ROM VE
	1500 FEET OF MUD	C
		- R R
		MERSUREI
B	EMORKO	
	EMARKS:	
١٠٠	OST PACKER SEAT DURING SECOND FLOW PERIOD.	[ ]
		11

TIME	CHOKE SIZE	SURFACE PRESSURE	GAS RATE	Llouid	TICKET NO: 58786500
12-5-83		PS1	MCF	RATE BPD	REMARKS
0225	Bu				
0227	ВН				OPENED HYDROSPRING
0230					FAINT BLOW
0235					LIGHT BLOW
0335					CLOSED IN
					OPENED
0340					
0350					FAINT BUBBLE
0400					FAINT BLOW
0420					FAINT BLOW
					PACKER SEAT GAVE WAY
425					CLOSED DCIP SAMPLER
					PULLED LOOSE
			_		
			•	•	
		:	:	:	
	*		4 .	ė	en e
	:				
	<u> </u>	İ	Ť	‡	7
· · · · · · · · · · · · · · · · · · ·	i		į	·	
				·	

CLOCK NO: 28224 HOUR: 24



GAUGE NO: 7511

	-			-		_	
R	EF	MINUTES	PRESSURE	ΔΡ	<u>1×Δ1</u> 1+Δ1	$\log \frac{t + \Delta t}{\Delta t}$	]
,			FIRST	FLOW			
B C	1	0.0	1294.2 1294.2	0.0			
		F.	IRST CL	OSED-IN	I		
D	1	0.0 59.4	1294.2 1339.1	45.0	9.0	0.071	
			SECOND	FLOW			
E	·** 23456789	30.0	1339.1 1361.2 1368.2 1398.1 1422.3 1438.0 1461.0 1480.8 1508.7	22.1 7.0 29.8 24.2 15.7 23.1 19.8 27.9			

11CKET NO: 58786500

CLOCK NO: 26221 HOUR: 24



GAUGE NO: 641

DEPTH: 9676.0

سو سو	-				7		<u> </u>	RVICES		PIH: 96	70.U		
	RE	F	MINUTES	PRESSURE	ΔΡ	<u>t×∆t</u> t+∆t	$\log \frac{t + \Delta t}{\Delta t}$	REF	MINUTES	PRESSURE	ΔP	<u>t×Δt</u> t + Δt	$\log \frac{t + \Delta}{\Delta t}$
				FIRST	FLOW						The second second	( / Δ(	1 - At
	В	1	0.0	1387.6									
		2	2.0	1387.2	-0.4								
		3	4.0	1384.3	-3.0			] ]					
		4	6.0	1382.8	-1.5			11					
		5	8.0	1382.8	0.0								
		6	10.0	1382.8	0.0								
	_	7	10.6	1381.7	-1.1								
			F	IRST CL	OSED-IN								
				THE CE	0250-114								
	•	1	0.0	1381.7						-			
		2	5.0	4049.5	2667.8	3.4		į					
		3	10.0	4555.2	3173.5	5.4	0.492	1					
		4	15.0	4865.1	3483.4	6.2	0.313	1					
		5	20.0	5064.0	3682.3	6.9	0.231						
		6	25.0	5196.9	3815.2	7.4	0.184 0.153	1					
		7	30.0	5295.6	3913.9	7.8	0.133						
		8	35.0	5368.4	3986.7	8.1	0.131	i					
		9	40.0	5424.3	4042.6	8.4	0.114						
		10	45.0	5473.1	4091.4	8.6	0.091						i de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de l
		[ ]	50.0	5514.8	4133.1	8.7	0.083						Į
0		12	55.0	5550.3	4168.6	8.9	0.003						
D	1	13	59.4	5575.9	4194.2	9.0	0.071						
			;	SECOND	FLOW								
Ε		i	0.0	1399.4									ĺ
_		2		1403.1	2 7		1						
		3	10.0	1413.5	3.7		1						
		4	15.0	1459.1	10.4		11						- 1
		- 5	20.0	1482.1	45.7								
		6	25.0	1507.4	22,9		11						1
		7		1522.4	25.3								
		<del>3</del>	35.0	1542.9	15.0 20.5								
<del></del>			ati 1	104519	20.5		: :						: :

REMARKS:

CLOCK NO: 26228 HOUR: 24



GAUGE NO: 1090

DEPTH: 9770.0

REI	F	MINUTES	PRESSURE	ΔP	1×Δt t+Δt	$log \frac{t + \Delta t}{\Delta t}$	REF	MINUTES	PRESSURE	ΔΡ	1×Δ1 1+Δ1	1 1
			FIRST	FLOW	Acceptance of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon		The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa			der were der felt blessen Abelder von der Abelder von	1 + 41	logt
_			i inoj.	1 LUW								
3	1	0.0	1469.4									
	2	2.0	1438.6	-30.8								
	3	4.0	1421.7	-16.9		j	1					
	4	6.0	1418.4	-3.3			İ					
	5	8.0	1418.0	-0.4		1	l					
	6	10.0	1415.4	-2.6		i	1					
C	7	10.6	1415.2	-0.2		İ						
		F	IRST CL	OSED-IN	J							
_	1	0.0	1415.2		•							
	2	5.0	4198.0	2782.8	<i>2</i> .							
	3	10.0	4642.9		3.4	0.496						
	4	15.0	4912.2	3227.7	5.1	0.313	1					
	5	20.0		3496.9	6.2	0.232	1					
	6	25.0	5089.2	3673.9	6.9	0.184	1					
			5215.6	3800.4	7.4	0.153						
	7	30.0	5312.1	3896.9	7.8	0.131						
	8	35.0	5382.2	3967.0	8.1	0.114						
	9	40.0	5441.0	4025.8	8.4	0.102	1					
	10	45.0	5489.2	4073.9	8.5	0.092						
	11	50.0	5529.0	4113.8	8.7	0.032	1					
	12	55.0	5563.4	4148.2	8.9	0.083						
1	3	59.4	5586.4	4171.2	9.0	0.076						
			SECOND		3.0	0.071						
				T L, U W								
	1	0.0	1434.7			- 11						
i	2	5.0	1435.1	0.4		11						
;	3	10.0	1443.2	8.2		11						
1	4	15.0	1495.4	52.1		11						
ç	5	20.0	1511.1	15.8		11						
	6	25.0	1548.1			- 11						
	7	30.0	1560.5	36.9								
ε		35.0	1579.6	12.4		11						
9		39.1	1625.8	19.1 46.2								
		55.1	1052.0	40.2								
						- 11						
						11						
												i
						11						
						L_						1



REF	MINUTES	7	HOUR: 24		HALLIE	AICES		AUGE NO: EPTH: 97		L.	
		PRESSURE	ΔΡ	<u>t×∆t</u> t+∆t	$log \frac{t + \Delta t}{\Delta t}$	REF	MINUTES	PRESSURE	ΔP	<u>1×Δ1</u> 1+Δ1	log
_		FIRST	FLOW			ĺ				Ι +Δτ	1.09
B 1	0.0	1476.2			1	1					
3	2.0 4.0	1448.3 1430.5									
4	6.0	1425.1	-17.8 -5.4								
5 _ 6	8.0	1424.9	-0.2		l		*				
C 7	10.0 10.6	1421.5 1422.1	-3.4								
		1462.1	0.6								
	F]	RST CL	OSED-IN								
C 1	0.0	1422.1			- 11						
2 3	5.0	4047.3	2625.2	3.4	0.496						
4	10.0 15.0	4552.1 4869.2	3130.0	5.1	0.313						
5	20.0	5066.7	3447.1 3644.6	6.2	0.232						
6 7	25.0	5200.9	3778.8	6.9 7.4	0.184 0.153						
8	30.0 35.0	5298.0 5375.0	3875.9	7.8	0.133						
9	40.0	5436.1	3952.9 4014.0	8.1	0.114						
10 11	45.0	5485.2	4063.1	8.4 8.6	0.102 0.091						
12	50.0 55.0	5525.9 5562.2	4103.8	8.7	0.083					*	
) 13		5585.9	4140.1 4163.8	8.9 9.0	0.076 0.071						•
	S	ECOND I	FLOW								
i		1443.8									
2	_	455	~3.9		- 11						
3 4	10.0	451.7	11.8		- 11						
5		502.4 523.4	50.7		- 11						
6	25.0 1	555.1	21.0 31.6								
7 8	30.0 1	574.0	18.9		11						
9	35.0 19 39.1 18	583.0	9.0								- 1
	00.1 16	533.7	50.7		- 11						- 1
											- 1
											l
					11						- 1

REMARKS:

¢ L		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Company of the Compan	TICKET NO. 58786500			
		0.D.	I.D.	LENGTH	DEPTH		
	DRILL PIPE						
	<del>M</del>	5.000	4.276	9393.0			
50	IMPACT REVERSING SUB	6.000	3.000	1.0	9382.0		
· A	DRILL COLLARS	6.000	3.000	273.Ó			
1	CROSSOVER	6.000	3.000	0.9			
, A	HANDLING SUB & CHOKE ASSEMBLY	5.750	2.250	4.6			
	AP RUNNING CASE	5.000	3.000	4.2	9660.0		
╂┈╢	DUAL CIP SAMPLER	5.000	0.750	7.0			
0	HYDROSPRING TESTER	5.000	0.750	5.0	9671.0		
$H\!-\!H$	AP RUNNING CASE	5.000	3.000	4.2	9676.0		
	JAR	5.000	1.750	5.0	10.0.0		
٧	VR SAFETY JOINT	5.000	1.000	2.8			
	OPEN HOLE PACKER	7.750	,1.530	5.8	9688.0		
	OPEN HOLE PACKER	7.750	1.530	5.8	9694.0		
	ANCHOR PIPE SAFETY JOINT	5.000	1.250	4.2			
	FLUSH JOINT ANCHOR	5.000	2.370				
0	BLANKED-OFF RUNNING CASE	5.000	21070	65.0			
D	BI ANKED-DEE BUNNING COOP			4.6	9770.0		
	TEMPERATURE RUNNING COSE	5.000		3.9	9774.0		
Щ	San Marino Challer	5.000		4.1	9778.0		
T	OTAL DEPTH						
					9778.0		

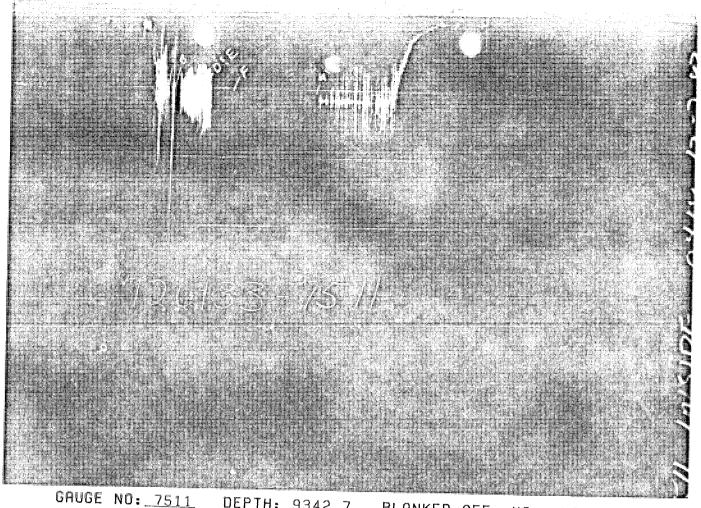


TICKET NO. 72613300
13-DEC-83
BAKERSFIELD
019-21924

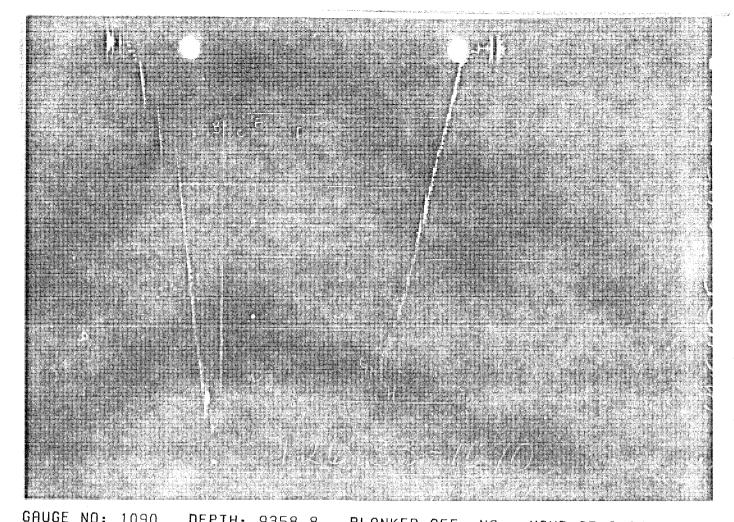


DIVESION OF OIL & GAS COALINGA

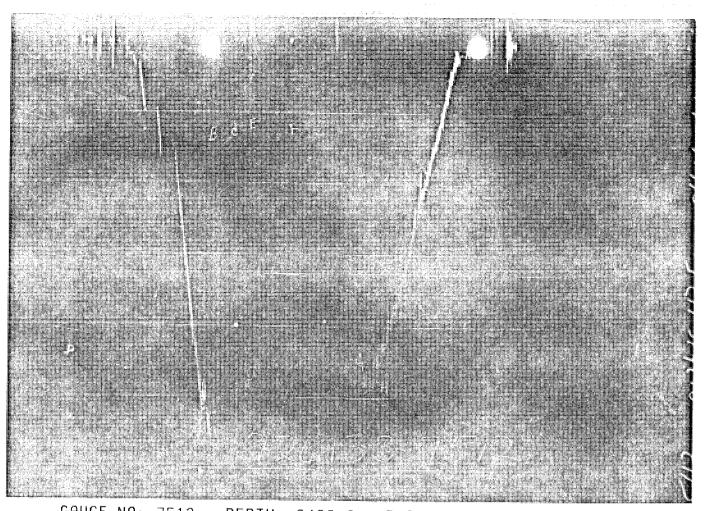
FORMATION TESTING SERVICE REPORT



DEPTH: 9342.7 BLANKED OFF: NO HOUR OF CLOCK: 2 ΙD PRESSURE DESCRIPTION TIME REPORTED CALCULATED TYP REPORTED | CALCULATED INITIAL HYDROSTATIC A INITIAL FIRST FLOW В 1088.8 FINAL FIRST FLOW 11.0 11.1 1-1096.7 С INITIAL FIRST CLOSED-IN 1096.7 D FINAL FIRST CLOSED-IN 60.0 59.8 С 1103.9 Ε INITIAL SECOND FLOW 1103.9 FINAL SECOND FLOW 72.0 73.0 1122.5 INITIAL SECOND CLOSED-IN 1122.5 FINAL SECOND CLOSED-IN G 180.0 179.0 С 1139.3 FINAL HYDROSTATIC



DEFIN: 9358.8	- REHVI	KED OFF:_	<u>NO</u> HOUR	OF CLOCK	: 24
DESCRIPTION					TYPE
INITIAL HYDROSTATIC	5548	5344.7	KLIOKIED	CHLCOLHIED	
INITIAL FIRST FLOW	1260	1232.5			
FINAL FIRST FLOW	1260	1232.5	11.0	11.1	F
INITIAL FIRST CLOSED-IN	1260	1232.5	7.1		
FINAL FIRST CLOSED-IN	4499	4457.1	60.0	59.8	С
INITIAL SECOND FLOW	1278	1254.4			
FINAL SECOND FLOW	1278	1243.0	72.0	73.0	F
INITIAL SECOND CLOSED-IN	1278	1243.0		-	
FINAL SECOND CLOSED-IN	4683	4661.7	180.0	179.0	С
FINAL HYDROSTATIC	5419	5086.0			
	DESCRIPTION  INITIAL HYDROSTATIC  INITIAL FIRST FLOW  FINAL FIRST FLOW  INITIAL FIRST CLOSED-IN  FINAL FIRST CLOSED-IN  INITIAL SECOND FLOW  INITIAL SECOND CLOSED-IN  FINAL SECOND CLOSED-IN	DESCRIPTION PRE REPORTED   INITIAL HYDROSTATIC 5548  INITIAL FIRST FLOW 1260 FINAL FIRST FLOW 1260 INITIAL FIRST CLOSED-IN 1260 FINAL FIRST CLOSED-IN 4499 INITIAL SECOND FLOW 1278 FINAL SECOND FLOW 1278 INITIAL SECOND CLOSED-IN 1278 FINAL SECOND CLOSED-IN 4683	DESCRIPTION PRESSURE REPORTED   CALCULATED  INITIAL HYDROSTATIC  5548 5344.7  INITIAL FIRST FLOW 1260 1232.5  FINAL FIRST CLOSED-IN 1260 1232.5  FINAL FIRST CLOSED-IN 1260 1232.5  FINAL FIRST CLOSED-IN 1260 1232.5  FINAL FIRST CLOSED-IN 1278 1254.4  FINAL SECOND FLOW 1278 1278 1243.0  FINAL SECOND CLOSED-IN 1278 1243.0  FINAL SECOND CLOSED-IN 4683 4661.7	DESCRIPTION	DESCRIPTION



GAUGE NO: _7512 DEPTH: 9422.0 BLANKED OFF: YES HOUR OF CLOCK: 24 PRESSURE ΙD DESCRIPTION TIME TYPE REPORTED | CALCULATED REPORTED | CALCULATED A INITIAL HYDROSTATIC 5535 5390.6 INITIAL FIRST FLOW В 1287 1297.6 11.0 11.1 F С FINAL FIRST FLOW 1287 1271.2 С INITIAL FIRST CLOSED-IN 1287 1271.2 60.0 59.8 С FINAL FIRST CLOSED-IN D 4460 4473.7 Ε INITIAL SECOND FLOW 1287 1304.9 72.0 73.0 F F FINAL SECOND FLOW 1287 1274.5 F INITIAL SECOND CLOSED-IN 1287 1274.5 180.0 179.0 C G FINAL SECOND CLOSED-IN 4664 4683.9 FINAL HYDROSTATIC 5424 5127.2

GAUGE NO: 641 DEPTH: 9425.9 BLANKED OFF: YES HOUR OF CLOCK: 24

ID DESCRIPTION PRESSURE TIME TYPE
REPORTED CALCULATED REPORTED CALCULATED

- 1	10	DESCRIPTION		JUUIL	i 1 1	116	I TYPE I
I		DESCRIT (10W	REPORTED	CALCULATED	REPORTED	CALCULATED	
	А	INITIAL HYDROSTATIC	5543	5405.9			
	В	INITIAL FIRST FLOW	1290	1289.1	11 0	1 1 1	
	С	FINAL FIRST FLOW	1290	1272.5	11.0	11.1	F
	С	INITIAL FIRST CLOSED-IN	1290	1272.5	CO O	FO 9	
	D	FINAL FIRST CLOSED-IN	4481	4496.0	60.0	59.8	С
	E	INITIAL SECOND FLOW	1272	1300.2	72.0	73.0	F
	F	FINAL SECOND FLOW	1272	1275.8	72.0	73.0	
	F	INITIAL SECOND CLOSED-IN	1272	1275.8	180.0	179.0	С
	G	FINAL SECOND CLOSED-IN	4540	4701.7	100.0	179.0	
	Н	FINAL HYDROSTATIC	5433	5141.0			

grant and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same and the same	
EQUIPMENT & HOLE DATA	TICKET NUMBER: 72613300
FORMATION TESTED:	DOTE: 12 2 92 TEST NO. C
NET PAY (ft):	DATE: 12-2-83 TEST NO: 6
GROSS TESTED FOOTAGE:53.4  ALL DEPTHS MEASURED FROM:KB	TYPE DST: OPEN HOLE
CASING PERFS. (ft):	
HOLE OR CASING SIZE (in): 8.750	INICETORION CULL
ELEVATION (ft):	BAKERSFIFLD
TOTAL DEPTH (ft): 9433.0	DIINI AP
PACKER DEPTH(S) (ft): <u>9374, 9380</u>	TESTER: DUNLAP KOUTROULIS
FINAL SURFACE CHOKE (in):	
BOTTOM HOLE CHOKE (in): 0.750	WITNESS ZURBA
MUD WEIGHT (lb/gal):10.50	WIINESS:
MUD VISCOSITY (sec):46	
ESTIMATED HOLE TEMP. (°F):20	DRILLING CONTRACTOR: '
ACTUAL HOLE TEMP. (°F): Ø ft	MONTGOMERY
FLUID PROPERTIES FOR RECOVERED MUD & WATER	SAMPLER DATA
	Pstg AT SURFACE:
SOURCE RESISTIVITY CHLORIDES	cu.ft. OF GAS:
6 °F ppm	
6 °F ppm	cc OF OIL:
	cc OF WATER:
8 ppm	cc OF MUD:
	TOTAL LIQUID cc:
HYDROCARBON PROPERTIES	CUSHION DATA
OIL GRAVITY (°API): @°F	TYPE AMOUNT WEIGHT
GAS/OIL RATIO (cu.ft. per bbl): GAS GRAVITY:	<u>WATER (FT.)</u> 2700.0 8.33
RECOVERED:	
2700' OF CUSHION	F RO VEM
150' OF DRILLING MUD ABOVE CH	USHION
	NSHION DE

## **REMARKS:**

CLOCK ON TE-68 SLIPPED AND WOULD NOT RECORD. CHART NOT SENT IN FOR PROCESSING.

TYPE & SIZE MEASURING DEVICE: TICKET NO: 72613300 SURFACE GAS LIQUID CHOKE REMARKS PRESSURE PSI TIME RATE RATE SIZE BPD MCF 12-2-83 0530 MADE UP TOOLS 0700 RAN IN HOLE 1045 1/4"BH OPENED TOOL WITH A FAINT BLOW FOR 2 MINUTES, THEN DIED. 1056 CLOSED TOOL 1156 1/4"BH OPENED TOOL WITH NO BLOW 1308 CLOSED TOOL 1608 CLOSED BY-PASS AND PULLED OUT OF HOLE. `a.___

CLOCK NO: 9661 HOUR: 24



GAUGE NO: 1090

DEPTH: 9358.8

R	EF	MINUTES	PRESSURE	ΔΡ	<u>t × Δt</u> t + Δt	$\log \frac{t + \Delta t}{\Delta t}$	
			FIRST	FLOW		S S S S S S S S S S S S S S S S S S S	-
В	1	0.0	1232,5				Section 1
	2	2.0	1234.0	1.5			
	3	4.0	1239.0	5.0			
	4 5	6.0 8.0	1239.0	0.0			
	6	10.0	1239.0 1234.1	0.0 -4.8			ļ
С	7	11.1	1232.5	-1.7			
		F	IRST CL	OSED-IN	I		
С	1	0.0	1232.5				
_	2	4.0	1601.1	368.6	2.9	0.580	
	3	8.0	1939.7	707.2	4.7	0.378	
	4	12.0	2285.4	1052.9	5.8	0.286	П
	5	16.0	2635.4	1402.9	6.6	0.229	
	6 7	20.0 24.0	2930.4 3217.6	1697.9	7.1	0.192	
	8	28.0	3440.2	1985.1 2207.7	7.6 8.0	0.165 0.145	
	9	32.0	3644.1	2411.6	8.3	0.145	
	10	36.0	3812.0	2579.6	8.5	0.117	
	11	40.0	3951.3	2718.8	8.7	0.107	П
	12	44.0	4084.7	2852.2	8.9	0.098	
	13 14	48.0	4190.8	2958.3	9.0	0.091	
	15	52.0 56.0	4291.5 4380.3	3059.1 3147.8	9.2 9.3	0.084	
D	16	59.8	4457.1	3224.6	9.4	0.079	
			SECOND	FI NW			
_				I LOW			
Ε	1	0.0	1254.4				
	2 3	10.0	1255.8	1.5		ľ	-
	4	20.0 30.0	1251.4 1242.5	-4.5 -8.0			1
	5	40.0	1240.8	-8.9 -1.7		ļ	
	6	50.0	1243.8	3.0		ļ	İ
	7	60.0	1243.8	0.0			
F	8	70.0	1243.8	0.0			
,	9	73.0	1243.0	-0.7			
		SE	COND CL	OSED-IN			
F	1	0.0	1243.0				
	2	10.0	1593.9	350.8	9.0	0.973	
	3	20.0	1947.1	704.1	16.1	0.717	
	4 5	30.0 40.0	2313.3 2664.4	1070.3	22.1	0.580	ĺ
	6	50.0	2992.6	1421.4 1749.5	27.1 31.3	0.492	
	7	60.0	3278.0	2034.9	35.0	0.429	
	8	70.0	3535.0	2292.0	38.2	0.343	
						i	1

RE	F	MINUTES	PRESSURE	ΔΡ	<u>t×Δt</u> t+Δt	log t+ At
	SE	COND CLOSED	-IN - CONTI	NUED	Mit in 12 - all children i in 19 Maria i madernida dan sessa i maderiari mind	Contraction of the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second seco
	9	80.0	3738.1	2495.1	41.0	0.312
	10	90.0	3911.7	2668.6	43.5	0.287
	1 i	100.0	4058.0	2815.0	45.7	0.265
	12	110.0	4175.1	2932.1	47.7	0.247
	13	120.0	4278.8	3035.8	49.5	0.231
	14	130.0	4365.0	3122.0	51.1	0.217
	15	140.0	4440.1	3197.1	52.5	0.204
	16	150.0	4505.7	3262.7	53.9	0.193
	17	160.0	4563.0	3319.9	55,1	0.184
_	18	170.0	4617.9	3374.8	56.3	0.175
G	19	179.0	4661.7	3418.7	57.2	0.167

CLOCK NO: 26221 HOUR: 24



rqc

GAUGE NO: 7512

DEPTH: 9422.0

		******				HAS
RI	EF	MINUTES	PRESSURE	ΔP	<u>t×Δt</u> t+Δt	$\log \frac{t + \Delta t}{\Delta t}$
			FIRST	FLOW		
В	1 2	0.0	1297.6 1289.0	-8.6		
	3 4	4.0 6.0	1291.0	2.1 -2.2		
С	5 6	10.0	1283.0 1273.8	-5.8 -9.2		
	7	11.1	1271.2	-2.6		
		F	IRST CL	OSED-IN	١	
С	1 2 3 4	0.0 4.0 8.0 12.0	1271.2 1636.0 1981.6 2337.3	364.8 710.5 1066.1	3.0 4.6 5.8	0.575 0.379 0.286
	5 6 7	16.0 20.0 24.0	2694.2 3005.6 3261.6	1423.0 1734.4 1990.5	6.6 7.1 7.6	0.229 0.192 0.165
	9	28.0 32.0	3481.4 3664.8	2210.2 2393.6	8.0 8.3	0.145 0.129
	10	36.0 40.0	3832.2 3976.0	2561.1 2704.8	8.5 8.7	0.117
	12 13 14	44.0 48.0 52.0	4099.4 4206.3 4307.2	2828.3 2935.1 3036.1	8.9 9.0 9.2	0.098 0.091 0.084
D	15 16	56.0 59.8	4397.0	3125.9 3202.5	9.3	B
			SECOND	FLOW		
·E,	1,	0.0	1304.9			
	3	10.0 20.0	1287.6 1282.2	-17.2 -5.4		
•	4	30.0	1272.1	-10.1		
	. 5 6	40.0 50.0	1270.4 1273.0	-1.7 2.6		
	7	60.0	1273.0	0.0		
F	8 9	70.0 73.0	1273.0 1274.5	0.0 1.5		
		SE	COND CL	OSED-II	N	
F	1	0.0	1274.5			3
	2 3	10.0 20.0	1595.3 1947.6	320.8 673.0	8.9 16.2	0.973 0.716
	4	30.0	2315.9	1041.4	22.1	0.580
	5	40.0	2686.5	1412.0	27.1	0.492
	6 7	50.0 60.0	3021.6 3316.2	1747.1 2041.7	31.3 35.0	0.429 0.380
	8	70.0	3565.0	2290.5	38.2	0.343

RE	F	MINUTES	PRESSURE	ΔP	<u>t×∆t</u> t+∆t	$\log \frac{t + \Delta t}{\Delta t}$
	SE	COND CLOSED	-IN - CONTI	NUED	ESTS ANNUAL COCKET PROTECTION OF CHARGE CONTRACTOR	TOWNS MANY MANY TO A WOOD AND THE
	9	80.0	3762.4	2487.9	41.0	0.312
	10	90.0	3933.1	<b>26</b> 58.6	43.5	0.287
	11	100.0	4072.7	2798.2	45.7	0.265
	12	110.0	4188.5	2914.0	47.7	0.247
	13	120.0	4293.5	3019.0	49.5	0.231
	14	130.0	4384.8	3110.3	51.1	0.217
	15	140.0	4462.9	3188.4	52.6	0.204
	16	150.0	4531.4	3256.8	53.9	0.193
	17	160.0	4589.6	3315.1	55.1	0.183
	18	170.0	4643.2	3368.7	56.3	0.175
G	19	179.0	4683.9	3409.3	57.2	<b>0.</b> 167

REMARKS:

CLOCK NO: 18754 HOUR: 24



GAUGE NO: 641

DEPTH: 9425.9

L						1 I € manuscreptures
RI	EF	MINUTES	PRESSURE	ΔΡ	1×Δ1 1+Δ1	$\log \frac{t + \Delta t}{\Delta t}$
			FIRST	FLOW		
В	i	0.0	1289.1			
l	2	2.0	1285.8	-3.3		
	3	4.0	1287.1	1.3		
	4	6.0	1285.4	-1.7		
	5	8.0	1281.0	-4.4		
С	6	10.0	1274.3	~6.7		
	7	11.1	1272.5	-1.8		
		F	IRST CL	OSED-IN	4	
С	1	0.0	1272.5			
	2	4.0	1618.1	345.7	2.9	0.579
	3	8.0	1973.0	700.6	4.7	0.378
	4	12.0	2317.8	1045.3	5.8	0.284
	5	16.0	2656.5	1384 <b>.0</b>	6.6	0.229
	6	20.0	2957.0	1684.6	7.1	0.192
	7	24.0	3245.2	1972.8	7.6	0.165
	8	28.0	3473.0	2200.5	8.0	0.145
	9 10	32.0 36.0	3666.2	2393.7	8.3	0.130
	11	40.0	38 <b>45.4</b> 3996.9	2572.9	8.5	0.117
	12	44.0	4127.2	2724.4 2854.7	8.7 8.9	0.106
	13	48.0	4240.7	2968.3	9.0	0.098
	14	52.0	4337.8	3065.3	9,2	0.090
	15	56.0	4427.2	3154.7	9.3	0.079
D	16	59.8	4496.0	3223.5	9.4	0.074
			SECOND	FLOW		
Е	1	0.0	1300.2			1
_	5	10.0	1290.2	-10.0		i
	3	20.0	1287.4	-2.8		
	4	30.0	1276.7	-10.7		
	5	40.0	1276.7	0.0		
	6	50.0	1275.4	-1.3		
	7	60.0	1275.4	0.0		- 1
F	8	70.0	1275.4	0.0		l
•	9	73.0	1275.8	0.4		
		SE	COND CL	OSED-IN	1	
F	i	0.0	1275.8			1
	2	10.0	1606.3	330.5	8.9	0.973
	3	20.0	1973.4	697.6	16.2	0.716
	4	30.0	2351.3	1075.5	22.1	0.580
	5	40.0	2711.1	1435.3	27.1	0.492
	6	50.0	3033,1	1757.3	31.3	0.429
	7 8	60.0	3321.9	2046.1	35.0	0.381
	O	70.0	3567.5	2291.7	38.2	0.343

	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				
REF	MINUTES	PRESSURE	ΔP	<u>1 × Δ1</u> 1 + Δ1	1091+AI
SE	COND CLOSED	-IN - CONTI	NUED	BOCCOSTE (FOR COMMAN) IN A WISSO SpREEL with agreement of	And the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s
9	80.0	3780.7	2504.9	41.0	0.312
10	90.0	3954.8	2679.0	43.5	0.287
11	100.0	4095.0	2819.3	45.7	0.285
12	110.0	4215.2	2939.4	47.7	0.247
13	120.0	4316.3	3040.5	49.5	0.231
14	130.0	4403.5	3127.7	51.1	0.217
15	140.0	4477.1	3201.3	52.6	0.204
16	150.0	4548.4	3272.7	53.9	0.193
17	160.0	4604.4	3328.6	55.1	0.184
18	170.0	4658.2	3382.4	56.3	0.175
G 19	179.0	4701.7	3425.9	57 <b>.2</b>	0.167
					- Towards

			0.0.	I.D.	LENGTH	DEPTH
		DRILL PIPE	5.000	4.276	9052.1	
5	0	IMPACT REVERSING SUB	6.000	3.000	1.0	9052.0
3		DRILL COLLARS	6.000	2.750	283.0	e e e
5		CROSSOVER	6.000	3.000	0.9	
		HANDLING SUB & CHOKE ASSEMBLY	5.750	2.250	4.6	
80	)	AP RUNNING CASE	5.000	3.000	4.2	9342.7
13	3 0	DUAL CIP SAMPLER	5.000	0.750	7.0	
60	c l	HYDROSPRING TESTER	5.000	0.750	5.0	9356.6
80		AP RUNNING CASE	5.000	3.000	4.2	9358.8
15		JAR	5.000	1.750	5.0	
16	v	VR SAFETY JOINT	5.000	1.000	2.8	
. 70		OPEN HOLE PACKER	7 <b>.7</b> 50	1.530	5.8	<b>9</b> 373 <b>.</b> 8
70		OPEN HOLE PACKER	7.750	1.530	5.8	9379.6
19		ANCHOR PIPE SAFETY JOINT	5.000	1.250	4.2	
20		FLUSH JOINT ANCHOR	5.000	2.370	35.0	
81	0	BLANKED-OFF RUNNING CASE	5.000		4.6	9422.0
81		BLANKEO-OFF RUNNING CASE	5.000		3.9	9425.9
82		TEMPERATURE RUNNING CASE	5.000		4.1	9432.0
	Ţ	OTAL DEPTH				9433.0

28: -26: -24: -23: -20: -20: -193: -175: -16:



15-DEC-83
BAKERSFIELD
019-21924



VELL NO

TEST NO.

TESTED INTERVAL

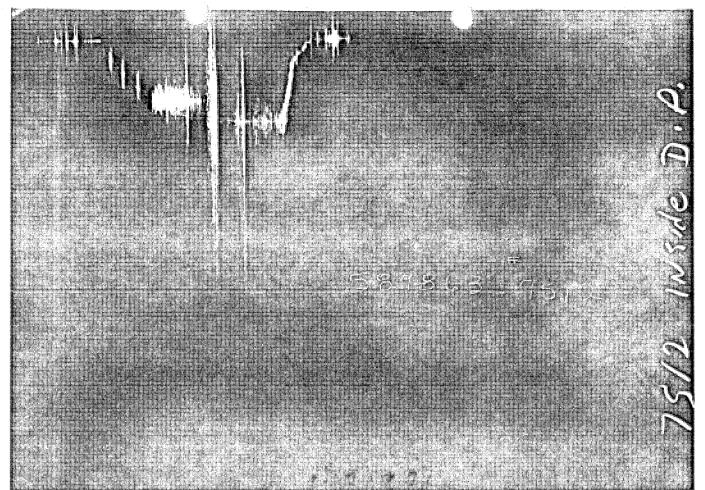
AMERICAN HUNTER EXPLORATION, LIMITED

STATE CALIFORNIA

FIELD

DRESION OF OIL & GAS COALINGA

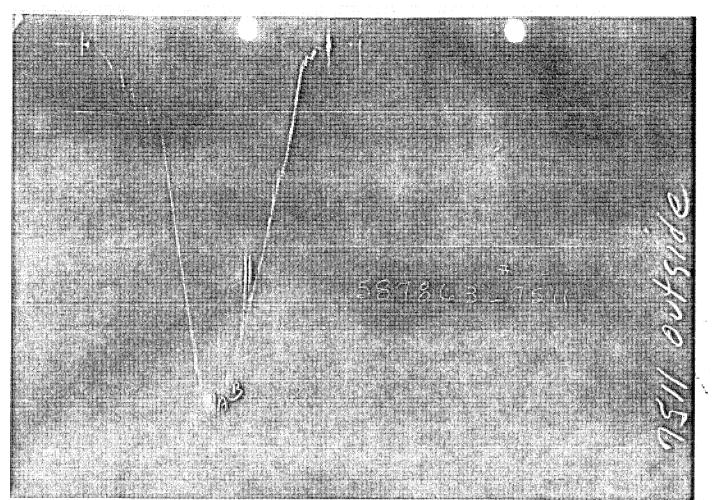
FORMATION TESTING SERVICE REPORT



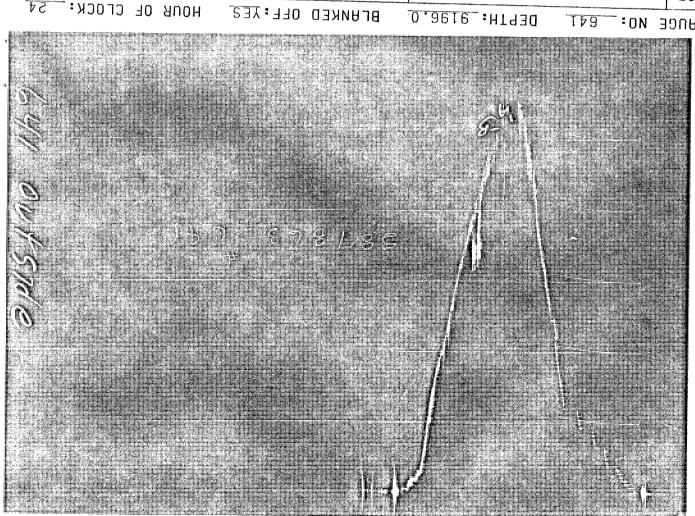
	GAUG	E NO: 7512 DEPTH: 9126.0	BLANKED OFF:	NO HOUR OF CLOCK:	24
	ID	DESCRIPTION	PRESSURE REPORTED CALCULATED	TIME	YPE
	A	INITIAL HYDROSTATIC	KELDKIED   CHECDEHIEL	D REPORTED CALCULATED	
	В	FINAL HYDROSTATIC			

 $\Gamma^{+}(Q,\zeta)$ 

UEPIH: 9142.0	. Blani	<pre><ed off:_<="" pre=""></ed></pre>	NO HOUR OF CLOCK	. 24
ID DESCRIPTION	PRE	SSURE	TIME	TYPE
A INITIAL HYDROSTATIC		5130.7	REPORTED CALCULATED	TYPE
B FINAL HYDROSTATIC	5198	5086.6		



GAUGE NO: 7511 DEPTH: 9192.0 BLANKED OFF: YES HOUR OF CLOCK: 24 PRESSURE REPORTED | CALCULATED TIME ΙD DESCRIPTION **TYPE** REPORTED CALCULATED A INITIAL HYDROSTATIC 5260 5166.5 В FINAL HYDROSTATIC 5182 5132.1



	₱"6SIS	2513	FINAL HYDROSTATIC	В
REPORTED   CALCULATED   11 L	7.9712	2887	INITIAL HYDROSTATIC	Ą
TIME	PRESSURE CALCULATED		DESCRIPTION	
S HOUR OF CLOCK: 24	VED OFF:∑E	ВГВИ	C NO: 641 DEPTH: 9196.0	 

EQUIPMENT & HOLE DATA	TICKET NUMBER: 58786300		
FORMATION TESTED:	DATE: 11-30-83 TEST NO: 5		
GROSS TESTED FOOTAGE: 40.0	51112 II V 00 103 1 100 1		
ALL DEPTHS MEASURED FROM: KELLY BUSHING	TYPE DST: OPEN HOLE		
CASING PERFS. (ft):	HALLIBURTON CAMP:		
HOLE OR CASING SIZE (tn): 8.750	BAKERSFIELD		
ELEVATION (ft):			
TOTAL DEPTH (ft): 9200.0	TESTER: R.D. LYONS		
PACKER DEPTH(S) (ft): 9154, 9160			
FINAL SURFACE CHOKE (in):0.750	WOLT ZUDDO		
MUD WEIGHT (lb/gal): 10.50	WITNESS: WALT ZURBA		
MUD VISCOSITY (sec): 46			
ESTIMATED HOLE TEMP. (°F);	DRILLING CONTRACTOR:		
ACTUAL HOLE TEMP. (°F): 121 @ 9200.0 ft	MONTGOMERY DRILLING COMPANY		
FLUID PROPERTIES FOR RECOVERED MUD & WATER SOURCE RESISTIVITY CHLORIDES	SAMPLER DATA Pstg AT SURFACE: cu.ft. OF GAS:		
	cc OF OIL:		
	cc OF WATER:		
	cc OF MUD:		
	TOTAL LIQUID cc:		
HYDROCARBON PROPERTIES  OIL GRAVITY (°API): @°F  GAS/OIL RATIO (cu.ft. per bbl):  GAS GRAVITY:	CUSHION DATA TYPE AMOUNT WEIGHT WATER (FI) 2000.0 8.33		
RECOVERED:			
PULLED TO FLUID RECOVERED CUSHION AND 523 FEET OF DRILL	8 (1 %		
REMARKS:			
LOST PACKER SEAT	Transaction of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Co		
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РАСКЕВ ЗЕВТ... CAME OUT OF THE HOLE., NO **DROPPED - PULLEO LOOSE AND** OPENED HYDROSPRING - FLUID 0230 DROPPED - PULLED LOGSE. OPENED HYDROSPRING - FLUIO 0253 E8-0E-11 110011 RATE BPD GRS RATE ACF PRESSURE PRESSURE PSI **K**EWBKK2 21SE CHOKE LIWE 11CKE1 NO: 28786300 TYPE & SIZE MEASURING DEVICE:

			0.0.	I.D.	LENGTH	DEPTH
9			****			
		DRILL PIPE	5.000	4.276	8854.0	
50	0	IMPACT REVERSING SUB	6.000	3.000	1.0	8838.0
3		DRILL COLLARS	6.000	2.750	283.0	
5		CROSSOVER	6.000	3.000	0.9	
11		HANDLING SUB & CHOKE ASSEMBLY	5.750	2,250	4.6	
80		AP RUNNING CASE	5.000	3.000	4.2	9126.0
13	0	DUAL CIP SAMPLER	5.000	0.750	7.0	
60	2	HYDROSPRING TESTER	5.000	0.750	5.0	, ,
80		AP RUNNING CASE	5.000	3.000	4.2	9142.0
15		JAR	5.000	1.750	5.0	The second
16	v	VR SAFETY JOINT	5.000	1.000	2.8	
70		OPEN HOLE PACKER	7.750	1.530	5.8	9154.0
70		OPEN HOLE PACKER,	7.750	1.530	5.8	9160.0
19		ANCHOR PIPE SAFETY JOINT	5.000	1.250	4.2	
20		FLUSH JOINT ANCHOR	5.000	2.370	21.0	
81	0	BLANKED-OFF RUNNING CASE	5.000		4.6	9192.0
81	0	BLANKED-OFF RUNNING CASE	5.000		3.9	9196.0
82		TEMPERATURE RUNNING CASE	5.000		4.1	9200.0
	т	OTAL DEPTH				
	1	OTHE BELLII				9200.0

## 89 国上一只约868年



Investigation

Approx. Radius of

Rate (Minimum)

Indicated Flow

Indicated Flow Capacity

Capacity

Average Effective

Permeability

Average Effective

San 1.151

$$\frac{kh}{h} = \frac{1637 Q_9 T}{h}$$

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11CKET NO. 58786200 15-DEC-83 BAKERSFIELD 019-21924



DIMISION OF OIL & GAS COALINGA

FORMATION TESTING SERVICE REPORT

EGAL LOCATION

LEASE NAME

WELL NO.

TEST NO.

TESTED INTERVAL

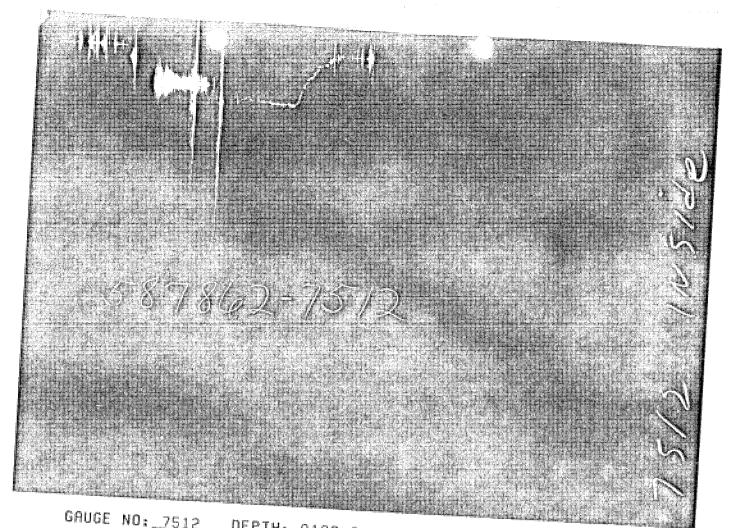
CHANNEY RANCH

FIELD AREA

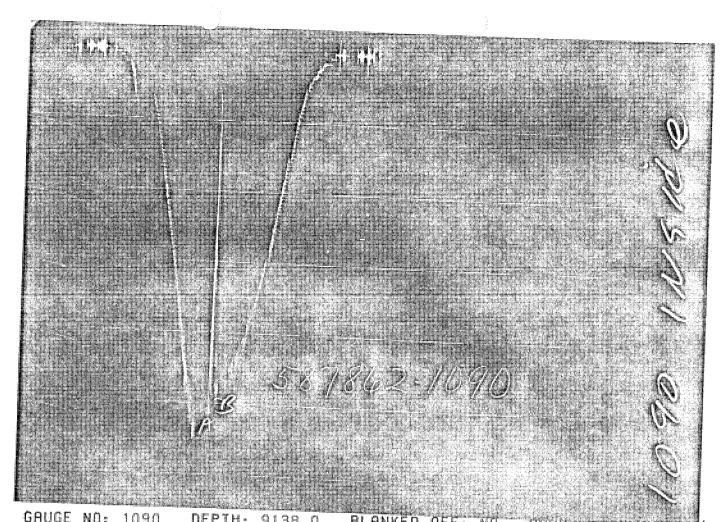
FRESNO

CALIFORNIA

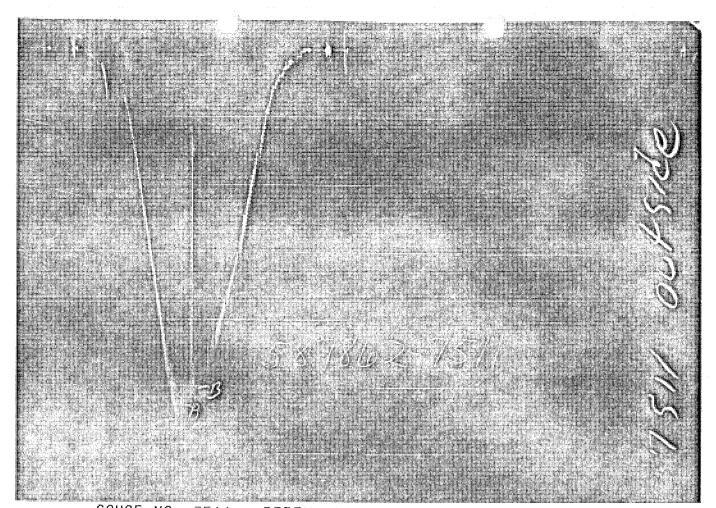
_EASE OWNER/COMPRNY NAM



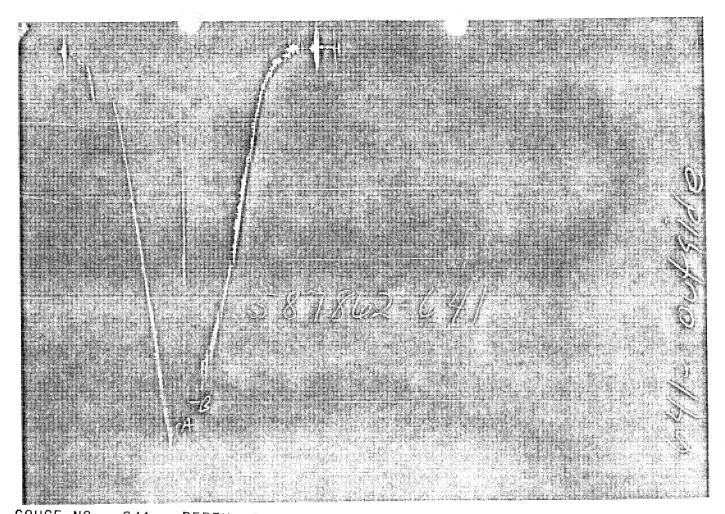
GAUG	E NO: 7512 DEPTH: 9122.0		
ID	DESCRIPTION	D BLANKED OFF: NO HOUR OF PRESSURE	CLOCK: 22
A	INITIAL HYDROSTATIC	REPORTED CALCULATED DECEMBER	CULATED TYPE
В	FINAL HYDROSTATIC		



*		<u> </u>	_ OLHN	NEU Urri	NU HUUK	OF CESSEN	4
	ID	DESCRIPTION		SSURE	TIME		TYPE
ŀ			REPORTED	CALCULATED	REPORTED	CALCULATED	
	A	INITIAL HYDROSTATIC		5207.9			
	В	FINAL HYDROSTATIC		4877.3			



	UHUU	E NO: 7511 DEPTH: 9192.0	. BLANK	(ED OFF: Y	<u>ES</u> HOUR	OF CLOCK	(: <u>_</u> _
	ID	DESCRIPTION	PRE:	SSURE	ΤI	TVE	
			REPORTED	CALCULATED	REPORTED	CALCULATED	- ' ' ' '
-	А	INITIAL HYDROSTATIC	5299	5268.1			
	В	FINAL HYDROSTATIC	4947	4939.3	***************************************		



GAUGE NO: _ 641 DEPTH: 9196.0 BLANKED OFF: YES HOUR OF CLOCK: 24 PRESSURE REPORTED CALCULATED ΙD DESCRIPTION TIME TYPE REPORTED CALCULATED A INITIAL HYDROSTATIC 5287 5280.4 В FINAL HYDROSTATIC 4994 4956.3

EQUIPMENT & HOLE UNA	
	TICKET NUMBER: 58786200
CD000 -	
GROSS TESTED FOOTAGE:  ALL DEPTHS MEASURED FROM:  CASING PERES. (2)	DATE: 11-29-83 TEST NO: 4
HOUT OR . (ft):	_   TYPE DST:OPEN HOLF
ELEVATION (ft):	HALLIBURTON CAMP: BAKERSFIELD
PACKER DEPTH(S) (ft): 9150, 9156  FINAL SURFACE CHOKE (tn):  BOTTOM HOLE CHOKE (tn):	TESTER: LYONS
MUD WEIGHT (lb/gal): 0. /// MUD VISCOSITY (sec): 10.///	WITNESS: ZURBA
ACTUAL HOLE TEMP. (°F): 212 @ 9200	DRILLING CONTRACTOR:  MONTGOMERY DRILLING COMPANY
SOURCE RESISTIVITY	SAMPLER DATA
eoF	Psig AT SURFACE:
— 6 — ob — bbw — 6 — ob — bbw	cu.ft. OF GAS:
9 oF bbw	cc nt OIL:
0 of bbw	CC OF WHIER:
8 oF - bbw	cc OF MUD:
HYDROCARRON BRODES - PPM	TOTAL LIQUID cc:
HYDROCARBON PROPERTII.	0110111
OIL GRAVITY (°API): @ "I GAS/OIL RATIO (cu.ft. per bbl):	CUSHION DATA
	WHIFR (CT)
RECOVERED:	1188.0 8.33
523' OF HOLE FLUID AND	
A LOID HALL MUD	MEHSURED FROM TESTER VALVE
	VAI
	SURE
REMARKS:	1ERS
LOST PACKER SEAT.	
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	Their President

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TYPE & SI	ZE MEASUR	ING DEVICE:	T		TICKET NO: 5878620
TIME	CHOKE SIZE	SURFACE PRESSURE PSI	GAS RATE MCF	LIQUID RATE BPD	REMARKS
11-29-83			ACCOUNT OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF THE PROPERTY OF 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0217					OPENED HYDROSPRING WITH A LIGHT
					BLOW
0219					PACKER SEAT GAVE AWAY
0220					PULLED LOOSE.
					1000
			17.17		
			ATT - 11 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		
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	TRANSPORT AND AND AND AND AND AND AND AND AND AND		The second section of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second sections of the second section sections of the second section sections of the second section sections of the second section sections of the section section sections of the section section section sections of the section section section section sections of the section section section section sections of the section section section section sections of the section section section section sections of the section section section section sections of the section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section section s		

·						
				I.D.	LENGTH	DEPTH
	<b>V</b>		_			
1		DRILL PIPE	5.000	4.276	8854.0	
50	a	IMPACT REVERSING SUB	6.000	3.000	1.0	8834.0
3		DRILL COLLARS	6.000	2.750	283.0	
5		CROSSOVER	6.000	3.000	0.9	
11		HANDLING SUB & CHOKE ASSEMBLY	5:750	2.250	4.6	
80		AP RUNNING CASE	5.000	3.000	4.2	9122.0
13	٥	DUAL CIP SAMPLER	5.000	0.750	7.0	
60	D	HYDROSPRING TESTER	5.000	0.750	5.0	· ·
80		AP RUNNING CASE	5.000	3.000	4.2	- <b>Q</b> 138.0
15		JAR	5.000	1.750	5.0	**************************************
16	v	VR SAFETY JOINT	5.000	1.000	2.8	
70		OPEN HOLE PACKER	7.750	1.530	5.8	9150.0
70		OPEN HOLE PACKER	7.750	1.530	5.8	9156.0
19		ANCHOR PIPE SAFETY JOINT	5.000	1.250	4.2	
20		FLUSH JOINT ANCHOR	5.000	2.370	25.0	
81	0	BLANKED-OFF RUNNING CASE	5.000		4.6	9192.0
81	D	8LANKED-OFF RUNNING CASE	5.000		3.9	9196.0
82		TEMPERATURE RUNNING CASE	5.000		4.1	9200.0
	_					
		TOTAL DEPTH				9200.0



Indicated Flow Capacity

$$kh = \frac{1637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[ \frac{m(P^*) - m(P_f)}{m} - LOG \frac{kt}{\phi \mu c_f r_w^2} + 3.23 \right] - -$$

Damage Ratio

$$DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 \text{ mS}}$$

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g \ m(P^*)}{m(P^*) - m(P_f)}$$

MCFD

Indicated Flow Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$$

MCFD

Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{kt}{\phi \mu c_t}}$$

ft

## RECEIVED

APR 2 3 1984

DIVISION OF OIL & GAS



TICKET NO. 58786100 28-NOV-83 BAKERSFIELD

SEC. - TWP. - RNG.

LEASE NAME

WELL NO.

**1831** 

NO.

6463, 1 -

6512.

AMERICAN HUNTER EXPLORATION LIMITED LEASE OWNER/COMPANY NAME

TESTED INTERVAL

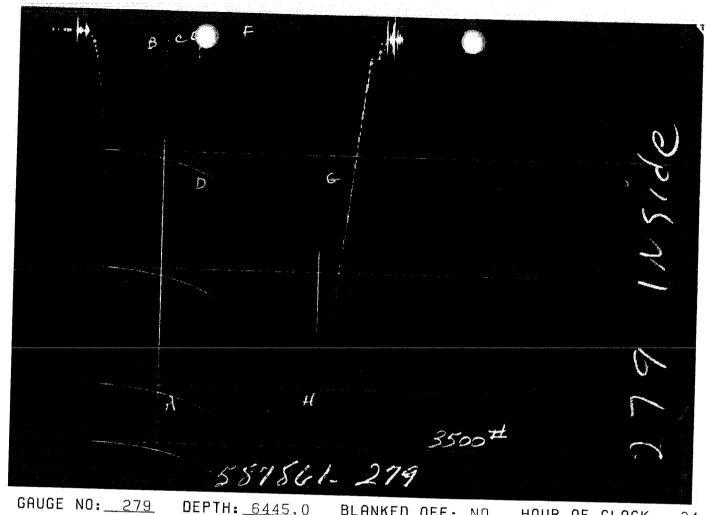
F I ELD AREA STATE CALIFORNIA

FORMATION TESTING SERVICE REPORT

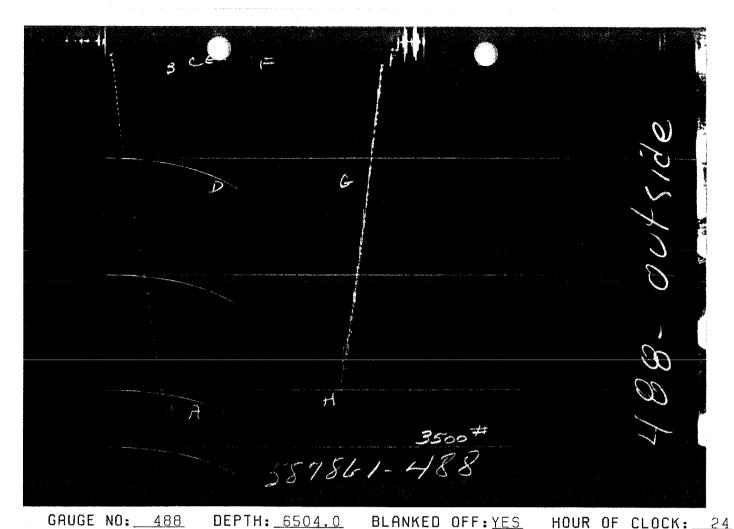
500 # 587861-6179

GAUGE NO: 6179 DEPTH: 6429.0 BLANKED OFF: NO HOUR OF CLOCK: 24

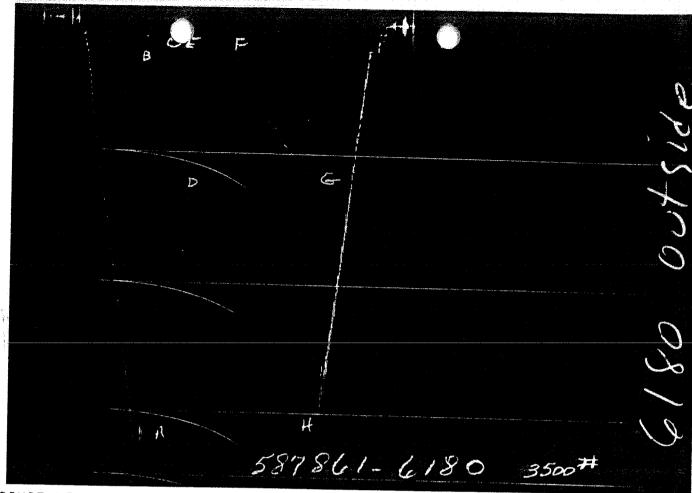
ΙD	DESCRIPTION	PRESSURE		II	ME	7115
A	INITIAL HYDROSTATIC	REPORTED	CALCULATED	REPORTED	CALCULATED	TYPE
В	INITIAL FIRST FLOW	31	73.6			
С	FINAL FIRST FLOW	31	21.7	10.0	9.7	F
С	INITIAL FIRST CLOSED-IN	31	21.7			
D	FINAL FIRST CLOSED-IN		32.5	61.0	60.2	С
E	INITIAL SECOND FLOW		21.4			
F	FINAL SECOND FLOW		3.6	91.0	92.9	F
F	INITIAL SECOND CLOSED-IN		3.6			
G	FINAL SECOND CLOSED-IN		3.8	187.0	186.2	С
Н	FINAL HYDROSTATIC					
					1	i



BLANKED OFF: NO HOUR OF CLOCK: 24 ΙD PRESSURE DESCRIPTION TIME REPORTED CALCULATED REPORTED TYPE CALCULATED Α INITIAL HYDROSTATIC 3183 3142.4 В INITIAL FIRST FLOW 66 67.1 10.0 9.7 F  $\mathbb{C}$ FINAL FIRST FLOW 55 36.7 INITIAL FIRST CLOSED-IN  $\mathbb{C}$ 55 36.7 FINAL FIRST CLOSED-IN 61.0 60.2 С D 1195 1185.1 Ε INITIAL SECOND FLOW 22 39.1 91.0 F 92.9 F FINAL SECOND FLOW 22 10.3 INITIAL SECOND CLOSED-IN F 22 10.3 187.0 FINAL SECOND CLOSED-IN 186.2  $\mathbb{C}$ G 1195 1205.9 FINAL HYDROSTATIC Η 3183 3042.0



	E NO. 300 BEI III. 0004.0		(LD 011 . 1	LJ HOOK	Of CLUCK	· <u> </u>
ID	DESCRIPTION	PRES	SSURE CALCULATED	TIM REPORTED	1E CALCULATED	TYPE
А	INITIAL HYDROSTATIC	3167	3177.4			
В	INITIAL FIRST FLOW	207	264.4	10.0	0 7	
С	FINAL FIRST FLOW	207	229.9	10.0	9.7	F
С	INITIAL FIRST CLOSED-IN	207	229.9	C1 0	60.2	С
D	FINAL FIRST CLOSED-IN	1195	1194.6	61.0		
E	INITIAL SECOND FLOW	218	242.2	0.1 0		_
F	FINAL SECOND FLOW	286	271.3	91.0	92.9	F
F	INITIAL SECOND CLOSED-IN	286	271.3	107.0	4.00	
G	FINAL SECOND CLOSED-IN	1195	1212.4	187.0	186.2	С
Н	FINAL HYDROSTATIC	3167	3056.4			



GAUG	E NO: 6180 DEPTH: 6508.0	_ BLANI	KED OFF:Y	ES HOUR	OF CLOCK	: 24
ID	DESCRIPTION	PRE REPORTED	SSURE CALCULATED	T I REPORTED	ME	TYPE
A	INITIAL HYDROSTATIC	3193	3179.3	KEFURTEU	CALCULATED	
В	INITIAL FIRST FLOW	250	276.6			
С	FİNAL FIRST FLOW	229	236.6	10.0	9.7	F
C	INITIAL FIRST CLOSED-IN	229	236.6	· · · · · · · · · · · · · · · · · · ·		
D	FINAL FIRST CLOSED-IN	1169	1183.0	61.0	60.2	С
E	INITIAL SECOND FLOW	229	254.5			
F	FINAL SECOND FLOW	271	283.8	91.0	92.9	F
F	INITIAL SECOND CLOSED-IN	271	283.8			
G	FINAL SECOND CLOSED-IN	1190	1205.6	187.0	186.2	C
Н	FINAL HYDROSTATIC	3193	3050.5			

CLOCK NO: 28187 HOUR: 24



**GAUGE NO:** 6179

log t+At

						& E P	AAICES				
RE	F	MINUTES	PRESSURE	ΔP	<u>t×∆t</u> t+∆t	log <u>t+Δt</u>	REF	MINUTES	PRESSURE	ΔP	1×,
			FIRST	FLOW						Marie Valencia de la comunicación de la Consideración se separa de la consideración se separa de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración del la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consideración de la consi	e Principal de la companya de la companya de la companya de la companya de la companya de la companya de la co
В											
D	1	0.0	73.6								
	2	2.0	52.3	-21.3							
	3	4.0 6.0	41.6	-10.7							
	4 5	8.0	37.2 32.9	-4.4 -4.3							
С	ວ 6	9.7	21.7	-4.3			[				
L	0	5.7	21.7	-11.5							
		F	IRST CL	OSED-II	N						
ſ	i	0.0	21.7								
C D	5	60.2	32.5	10.9	8.4	0.065					
			SECONE	FLOW							
			JECONE	) I LOW							
Ε	1	0.0	21.4								
	2	10.0	5.0	-16.4							
	3	20.0	4.4	-0.6							
	4	30.0	4.0	-0.4							
	5	40.0	4.0	0.0							
	6	50.0	4.0	0.0							
	7	60.0	4.0	0.0							
	8	70.0	4.0	0.0							
	9	80.0	4.1	0.1							
F	10	92.9	3.6	-0.5							
		SE	ECOND CI	LOSED-I	N						
F	1	0.0	3.6								
Ġ	2	186.2	3.8	0.2	66.1	0.191					
			_	<del>_</del>							

REMARKS: THIS GAUGE WAS RUN ABOVE THE TOOL.



CLI	DC M	NO: 2	8235 H	IOUR: 2	4		VIC
RE	F	MINUTES	PRESSURE	ΔΡ	1×Δ1 1+Δ1	$\log \frac{t + \Delta t}{\Delta t}$	
			FIRST	FLOW			
В	1 2 3	0.0 2.0 4.0	67.1 67.6 54.0	0.6 -13.6			
С	4 5 6	6.0 8.0 9.7	46.9 42.0 36.7	-7.1 -4.9 -5.3			
U	Ü			.0SED-I	N		
_				-0350-1	IN		
	1 2 3 4 4 5 6 7 8 9 10 11 12 13	0.0 5.0 10.0 15.0 20.0 25.0 30.0 35.0 40.0 45.0 50.0 55.0		430.7 602.5 715.4 797.3 860.7 917.4 964.5 1006.5 1047.3 1083.5 1115.7 1148.4	3.3 4.9 5.9 6.5 7.0 7.3 7.6 7.8 8.0 8.1 8.3	0.294 0.216 0.172 0.143 0.122 0.106 0.094 0.085 0.077	manage dessity for the profile states that the states with the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of the states of
E	1 2 3 4 5 6 7 8 9	0.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 92.9	39.1 11.6 11.1 9.9 9.9 9.5 9.5 10.0	-27.5 -0.6 -1.2 0.0 0.0 -0.3 0.0 0.4			
		, Si	ECOND C	LOSED-	IN		
F	1 2 3 4 5 6 7 8 9 10	0.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	10.3 210.5 333.8 433.8 517.7 590.1 658.2 718.2 774.3 827.2 876.8	200.2 323.5 423.5 507.3 579.8 647.9 707.9 764.0 816.8 866.5	9.1 16.7 23.2 28.8 33.6 37.9 41.6 44.9 47.9	1.050 0.787 0.645 0.552 0.485 0.433 0.392 0.358 0.330	

E E	CATALOGUE (A)		III. UT	70.0		
RE	F	MINUTES	PRESSURE	ΔΡ	<u>1 ×Δt</u> 1 + Δt	log <u>t+Δt</u>
	SEC	OND CLOSED-	IN - CONTIN	UED		
	12	110.0	922.7	912.4	53.1	0.286
	13	120.0	966.9	956.6	55.3	0.268
	14	130.0	1007.7	997.4	5 <b>7.</b> 3	0.253
	15	140.0	1046.4	1036.1	59.2	0.239
	16	150.0	1084.0	1073.7	60.9	0.226
	17	160.0	1121.4	1111.1	62.5	0.215
	18	170.0	1154.6	1144.2	64.0	0.205
	19	180.0	1187.7	1177.4	65.4	0.196
G	20	186.2	1205.9	1195.6	66.1	0.191

CLOCK NO: 26292 HOUR: 24



GAUGE NO: 488

DEPTH: 6504.0

RE	F	MINUTES	PRESSURE	ΔP	1×Δt 1+Δt	$log \frac{t + \Delta t}{\Delta t}$
			FIRST	FLOW		
В	1 2 3 4	0.0 2.0 4.0 6.0	264.4 251.5 236.6 231.2	-12.9 -15.0 -5.3		
С	5 6	8.0 9.7	228.5 229.9	-2.7 1.4		
		F	IRST CL	.OSED-I	N	·
С	1	0.0	229.9			
J	2 3 4 5 6 7	5.0 10.0 15.0 20.0 25.0 30.0	501.5 652.8 755.3 835.5 895.1 953.6	271.6 422.9 525.4 605.6 665.2 723.7	3.3 4.9 5.9 6.5 7.0 7.3	0.467 0.295 0.216 0.172 0.142 0.122
ם	8 9 10 11 12 13	35.0 40.0 45.0 50.0 55.0 60.2	998.7 1049.7 1092.7 1129.7 1162.9 1194.6	768.8 819.8 862.8 899.8 933.0 964.7	7.6 7.8 8.0 8.1 8.3	
			SECONE	) FLOW		
Ε.	1 2 3 4 5 6 7	0.0 10.0 20.0 30.0 40.0 50.0	242.2 242.2 251.7 258.2 259.1 266.5 268.2	0.0 9.5 6.4 0.9 7.4 1.7		
F	8 9 10	70.0 80.0 92.9	269.9 274.0 271.3	1.6 4.1 -2.7		
	10			LOSED-1	· N	
_				-03-D-1	. 14	
F	1 2 3 4 5 6 7 8 9 10	0.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	271.3 284.0 328.3 415.0 497.9 569.3 640.9 706.5 767.6 825.1 877.2	12.7 57.0 143.7 226.6 298.0 369.6 435.2 496.4 553.8 605.9	9.1 16.7 23.2 28.8 33.6 37.8 41.6 45.0 47.9 50.6	1.052 0.787 0.645 0.552 0.485 0.433 0.392 0.358 0.330 0.307

REF	MINUTES	MINUTES PRESSURE ΔP		<u>t×Δt</u> t+Δt	109174
SE	COND CLOSED-	IN - CONTIN	IUED		
12	110.0	921.6	650.4	53.1	0.286
13	120.0	965.9	694.6	55.3	0.268
14	130.0	1008.2	737.0	57.3	0.253
15	140.0	1046.3	775.0	59.2	0.239
16	150.0	1085.5	814.2	60.9	0.886
17	160.0	1121.7	850.4	62.5	0.215
18	170.0	1156.3	885.0	64.0	0.205
19	180.0	1192.1	920.8	65.3	0.196
G 20	186.2	1212.4	941.1	66.1	0.191

CLOCK NO: 13680 HOUR: 24



			<del></del>			The same same and	
REF	-	MINUTES	PRESSURE	ΔΡ	<u>t ×∆t</u> t + ∆t	$\log \frac{t + \Delta t}{\Delta t}$	the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa
			FIRST	FLOW			
В	1 2 3	0.0 2.0 4.0 6.0	276.6 259.3 246.2 240.2	-17.3 -13.0 -6.1			
С	4 5 6	8.0 9.7	235.9 236.6	-4.3 0.7			
		F	IRST CL	.OSED-I	N		
С	1 2 3 4 5 6 7 8 9 10 11 12 13	0.0 5.0 10.0 15.0 20.0 25.0 30.0 35.0 40.0 45.0 50.0 60.2	236.6 512.1 652.2 750.1 823.5 887.2 940.3 988.4 1037.0 1078.8 1116.7 1150.1 1183.0	275.5 415.6 513.5 586.8 650.5 703.7 751.8 800.3 842.2 880.1 913.5 946.3	3.3 4.9 5.9 6.5 7.0 7.3 7.6 7.8 8.0 8.1 8.3	0.468 0.296 0.217 0.172 0.143 0.122 0.106 0.094 0.085 0.077 0.071	
			SECONE	FLOW			
E	1 2 3 4 5 6 7 8 9	0.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 92.9	254.5 253.4 261.9 267.7 269.8 277.5 278.2 281.6 285.4 283.8	-1.0 8.5 5.8 2.1 7.6 0.7 3.4 3.8 -1.6			
		SI	ECOND C	LOSED-1	IN		
F	1 2 3 4 5 6 7 8 9 10	0.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	283.8 296.9 338.8 425.4 507.7 583.8 652.1 713.8 772.7 826.0 877.1	13.0 55.0 141.5 223.9 300.0 368.3 430.0 488.8 542.2 593.3	9.1 16.7 23.2 28.8 33.6 37.9 41.6 44.9 47.9 50.6	1.051 0.788 0.646 0.552 0.484 0.433 0.392 0.358 0.330 0.307	

DEPTH: 6508.0											
REF	MINUTE	S PRES	SURE	ΔΡ	<u>t×Δt</u> t+Δt	log <u>t + Δt</u>					
SEC 12 13 14 15 16 17 18 19 <b>G</b> 20	COND CLOS 110 120 130 140 150 160 170 180	.0 9 .0 10 .0 10 .0 10 .0 11 .0 11	CONTINUED 24.4 67.5 10.1 48.0 85.1 20.4 54.9 87.1 05.6	640.6 683.7 726.3 764.2 801.3 836.5 871.1 903.2 921.8	53.1 55.3 57.3 59.2 60.9 62.5 64.0 65.3 66.1	0.286 0.268 0.253 0.239 0.226 0.215 0.205 0.196 0.191					
					·						

ı		0.D.	I.D.	LENGTH	DEPTH
z.	<u>-</u>				
	DRILL PIPE	5.000	4.270	6250.0	
50	IMPACT REVERSING SUB	6.000	3.000	1.0	6238.0
3	DRILL COLLARS	6.000	3.000	180.0	
5	CROSSOVER	6.000	3.000	0.9	
11	HANDLING SUB & CHOKE ASSEMBLY	5.750	2.250	4.6	
97	RECORDER ABOVE DCIP VALVE	5.000	3.000	4.2	6429.0
13	DUAL CIP SAMPLER	5.000	0.750	7.0	
60	HYDROSPRING TESTER	5.000	0.750	5.0	
80	AP RUNNING CASE	5.000	3.000	4.2	6445.0
15	JAR	5.000	1.750	5.0	
16 v	VR SAFETY JOINT	5.000	1.000	2.8	
70	OPEN HOLE PACKER	7.750	1.530	5.8	6457.0
70	OPEN HOLE PACKER	7.750	1.530	5.8	6463.0
19	ANCHOR PIPE SAFETY JOINT	5.000	1.250	4.2	
20	FLUSH JOINT ANCHOR	5.000	2.370	30.0	
82	TEMPERATURE RUNNING CASE	5.000	2.440	4.6	6500.0
81	BLANKEO-OFF RUNNING CASE	5.000		3.9	6504.0
81 0	BLANKED-OFF RUNNING CASE	5.000		4.1	6508.0
	•				

# 4587861- TE 68

Indicated Flow Capacity

68

Con

$$kh = \frac{1637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[ \frac{m(P^*) - m(P_f)}{m} - LOG \frac{kt}{\phi \mu c_f r_w^2} + 3.23 \right] -$$

Damage Ratio

$$DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 \text{ mS}}$$

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_f)}$$

MCFD

Indicated Flow Rate (Minimum)

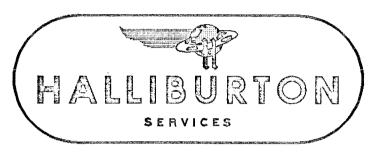
$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$$

MCFD

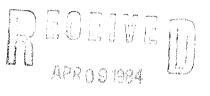
Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{kt}{-\phi\mu c_1}}$$

ft



TICKET NO. 58786000 22-NOV-83 BAKERSFIELD



DIVESION OF OIL & GAS

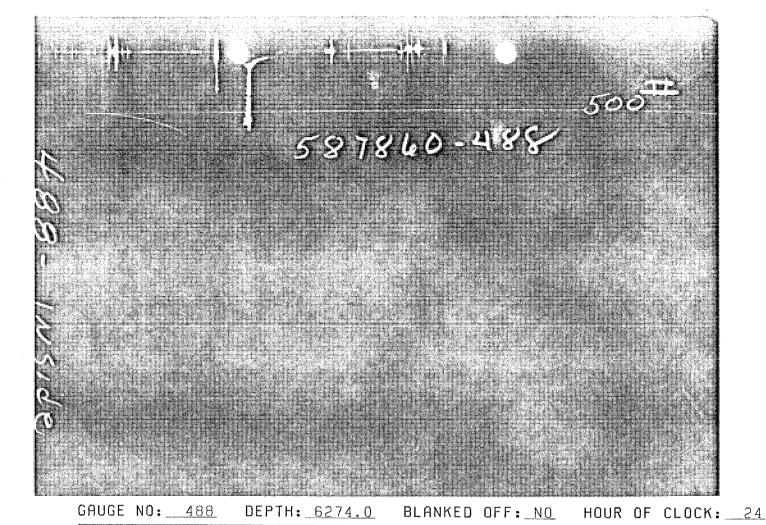
FORMATION TESTING SERVICE REPORT

CHANNEY RANCH

TESTED INTERVAL

STATE CALIFORNIA

HMENICHM FLOWIEK CAFFUNNIION LIBITOR



PRESSURE REPORTED | CALCULATED TIME ID DESCRIPTION TYPE REPORTED CALCULATED INITIAL HYDROSTATIC В INITIAL FIRST FLOW 305 132.9 10.0 8.6 F C FINAL FIRST FLOW 109 118.1 C INITIAL FIRST CLOSED-IN 109 118.1 61.0 C 59.4 D FINAL FIRST CLOSED-IN 653 104.8 INITIAL SECOND FLOW E 43 104.8 61.0 F 64.6

48.7

48.7

11.2

120.0

119.3

C

FINAL SECOND FLOW

FINAL HYDROSTATIC

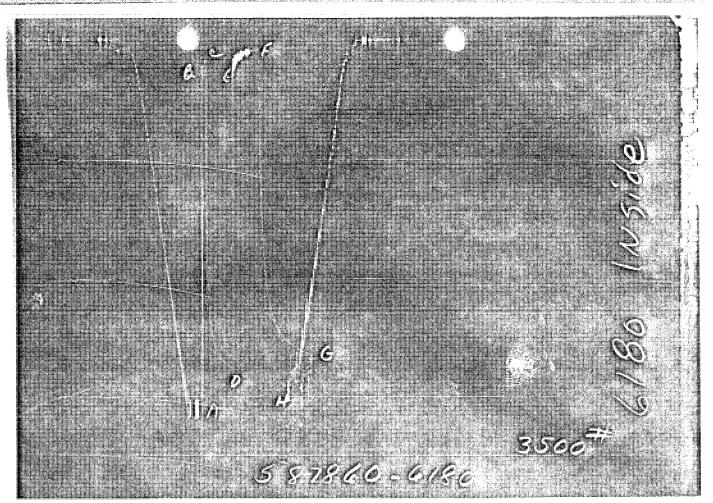
INITIAL SECOND CLOSED-IN

FINAL SECOND CLOSED-IN

F

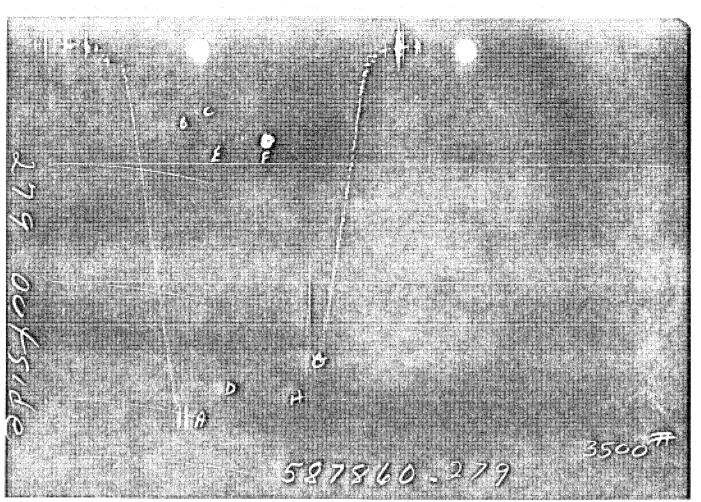
G

Н



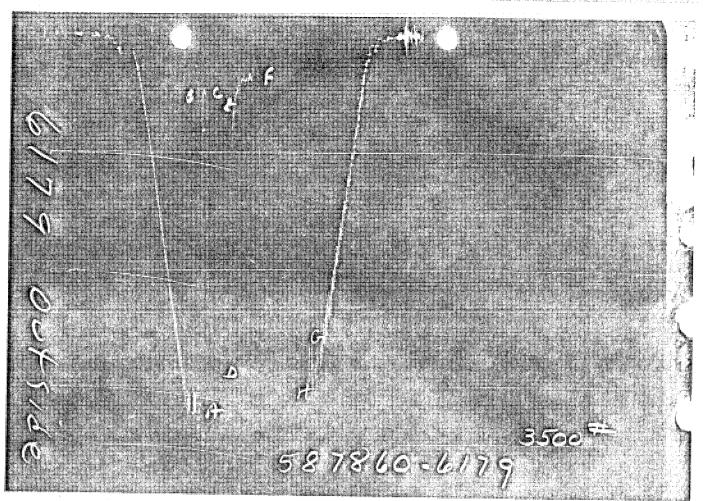
GAUGE NO: 6180 DEPTH: 6290.0 BLANKED OFF: NO HOUR OF CLOCK: 24

ID	DESCRIPTION		SSURE		ME	TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	3108	3094.3			
В	INITIAL FIRST FLOW	208	313.5	10.0	8.6	F
С	FINAL FIRST FLOW	167	163.8	10.0	0.0	_
С	INITIAL FIRST CLOSED-IN	167	163.8	61.0	59.4	С
D	FINAL FIRST CLOSED-IN	2747	2744.6	OI.U	JJ,4	
E	INITIAL SECOND FLOW	146	362.6	61.0	C4 C	F
F	FINAL SECOND FLOW	62	78.4	01.0	64.6	Г
F	INITIAL SECOND CLOSED-IN	62	78.4	120.0	119.3	С
G	FINAL SECOND CLOSED-IN	2641	2639.6	120.0	115.5	U
H	FINAL HYDROSTATIC	3108	2943.9			



GAUGE NO: 279 DEPTH: 6369.0 BLANKED OFF: YES HOUR OF CLOCK: 24

ID	DESCRIPTION	PRE	SSURE	TI	TYPE	l	
טו	DESCRIPTION	REPORTED	CALCULATED	REPORTED	CALCULATED		
А	INITIAL HYDROSTATIC	3115	3132.9				
В	INITIAL FIRST FLOW	487	617.1	10.0	8.6	F	-
С	FINAL FIRST FLOW	576	576.0	10.0	0.0		-
С	INITIAL FIRST CLOSED-IN	576	576.0	61.0	59.4	С	-
D	FINAL FIRST CLOSED-IN	2757	2772.6	01.0	55.4		
E	INITIAL SECOND FLOW	841	944.9	61.0	64.6	F	
F	FINAL SECOND FLOW	797	817.3	OI.O	04.0	<u> </u>	
F	INITIAL SECOND CLOSED-IN	797	817.3	120.0	119.3		- Constitution
G	FINAL SECOND CLOSED-IN	2645	2654.4	120.0	115.5		
Н	FINAL HYDROSTATIC	3115	2972.5				-



GAUGE NO: 6179 DEPTH: 6373.0 BLANKED OFF: YES HOUR OF CLOCK: 24

ID	DESCRIPTION	PRES	SSURE CALCULATED	T I REPORTED	ME CALCULATED	TYPE
A	INITIAL HYDROSTATIC	3120	3129.9	KEFURIEU	CHLCOLHIED	Particular Malifestria de La marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca de la marca dela marca dela marca de la marca de la marca de la marca dela marc
В	INITIAL FIRST FLOW	481	559.9			
С	FINAL FIRST FLOW	523	509.3	10.0	8.6	F
С	INITIAL FIRST CLOSED-IN	523	509.3	0.4		_
D	FINAL FIRST CLOSED-IN	2758	2756.2	61.0	59.4	С
E	INITIAL SECOND FLOW	523	649.4	0.4		
F	FINAL SECOND FLOW	314	337.2	61.0	64.6	F
F	INITIAL SECOND CLOSED-IN	314	337.2	100 0	4.4.0	
G	FINAL SECOND CLOSED-IN	2630	2650.3	120.0	119.3	С
Н	FINAL HYDROSTATIC	3120	2969.2			

TYPE & SIZE MEASURING DEVICE: . CHOKE TICKET NO: 58786000 GAS RATE LIQUID RATE SURFACE CHOKE REMARKS PRESSURE TIME SIZE PS1 MCF BPD 11-15-83 1 " 1906 OPENED TODL 1 " 1910 28# GAS TO SURFACE 28 1916 1 CLOSED TOOL 2017 .75 OPENED TODL 2019 .75 30 GAS 2037 .75 20 GAS 2045 .75 17 GAS 15 2100 .75 GAS 2118 .75 15 CLOSED TOOL 2318 PULLED LOOSE

REMARKS:

CLOCK NO: 13740 HOUR: 24



GAUGE NO: 488

DEPTH: 6274.0

. L U		IACA T.	en perior de la completa de la propria de manuel de 1990 - commune de 1990 - commune de 1990 - commune de 1990			* Type season to the season to the season to	CONTRACTOR OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE PARTY OF THE		110000	program de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la companya de la company	1 1×11	1. 1
REF		MINUTES	PRESSURE	ΔP	<u>t ×Δt</u> t +Δt	$\log \frac{1+\Delta t}{\Delta t}$	REF	MINUTES	PRESSURE	ΔΡ	1 × Δ1 1 + Δ1	1091
	•		FIRST	FLOW								
D		0.0	132.9									
3	1	8.6	118.1	-14.7								
		F	IRST CL	OSED-I	N							
C D	j 2	0.0 59.4		-13.3	7.5	0.059						
			SECONI	) FLOW							•	
E	1	0.0	104.8								* 4	
_	2	10.0	103.5								1.1	
	3 4	20.0 30.0										
	5	40.0		-8.5								
F	6	50.0	54.3									
Γ	7	64.6	40,7	-3.0								
		S	ECOND (	CLOSED-	IN							
F G	1 2	0.0 119.3		-37.4	45.	4 0.208						
5	-	115.0										
i							11					

+ Δt Δt CLOCK NO: 26292 HOUR: 24



GAUGE NO: 6180

DEPTH: 8290.0

L						3.5	RVICES	nancze s		. 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
REF	F	MINUTES	PRESSURE	ΔΡ	<u>t×∆t</u> t+∆t	$\log \frac{t + \Delta t}{\Delta t}$	RE	F	MINUTES	PRESSURE	ΔP	<u>t×Δt</u> t+Δt	$\log \frac{t + \Delta t}{\Delta t}$
			FIRST	FLOW			G	\$E0	COND CLOSED	-IN - CONTIN	JED 2561.2	45.4	0.208
BC	1	0.0 8.6	313.5 163.8	-149.7									
		F	IRST CL	OSED-IN									
	1 2 3 4 5 6 7 8 9 10 11 11 12 11 3 11 4 11 5 11 6	0.0 4.0 8.0 12.0 16.0 20.0 24.0 28.0 32.0 36.0 40.0 44.0 48.0 52.0 56.0	163.8 2005.2 2286.5 2429.9 2515.4 2575.4 2614.9 2646.7 2669.7 2687.0 2701.7 2715.4 2724.9 2733.2 2740.6 2744.6	1841.4 2122.7 2266.1 2351.6 2411.6 2451.1 2482.9 2506.0 2523.3 2537.9 2551.6 2561.2 2569.4 2576.8 2580.8	2.7 4.1 5.0 5.6 6.0 6.3 6.6 6.8 7.0 7.1 7.2 7.3 7.4 7.5								
			SECOND	FLOW									
	1 2 3 4 5 6 7	0.0 10.0 20.0 30.0 40.0 50.0 64.6	362.6 162.8 124.2 103.5 95.1 90.4 78.4	-199.8 -38.6 -20.7 -8.5 -4.7 -12.0									
		SE	COND CL	OSED-IN	~	-							
	1 2 3 4	0.0 8.0 16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0 80.0 88.0 96.0 104.0	78.4 1683.6 2018.9 2204.5 2319.6 2394.2 2446.7 2486.2 2519.6 2546.1 2567.3 2588.1 2603.9 2618.7 2630.0	1605.3 1940.5 2126.2 2241.2 2315.8 2368.3 2407.8 2441.2 2467.7 2488.9 2509.7 2525.5 2540.3 2551.6	7.2 13.1 18.1 22.3 25.9 29.0 31.7 34.2 36.3 38.2 40.0 41.6 43.0 44.3	1.005 0.747 0.608 0.517 0.452 0.403 0.363 0.331 0.305 0.282 0.263 0.246 0.232 0.219							

CLOCK NO: 13680 HOUR: 24



GAUGE NO: 279

DEPTH: 6369.0

L			3000 1	100K: 24		AR!	AVICE:
	REF	MINUTES	PRESSURE	ΔP	<u>t ×Δt</u> t +Δt	$\log \frac{t + \Delta t}{\Delta t}$	
			FIRST	FLOW			
E	) i	0.0 8.6	617.1 576.0	-41.1			
		F	IRST CL	OSED-IN			
C	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	0.0 4.0 8.0 12.0 16.0 20.0 24.0 28.0 32.0 36.0 40.0 44.0 48.0 52.0 56.0 59.4	576.0 1977.7 2283.8 2435.0 2539.8 2602.7 2645.2 2673.2 2697.2 2714.8 2728.7 2741.6 2751.9 2759.8 2767.1 2772.6	1401.7 1707.7 1859.0 1963.8 2026.6 2069.1 2097.1 2121.2 2138.7 2152.7 2165.6 2175.9 2183.8 2191.1 2196.5	2.7 4.2 5.0 5.6 6.3 6.6 6.8 7.1 7.2 7.3 7.4 7.5	0.497 0.317 0.236 0.188 0.156 0.133 0.117 0.104 0.093 0.085 0.078 0.072 0.067 0.062 0.059	
			SECOND	FLOW			
E	1 2 3 4 5 6 7	0.0 10.0 20.0 30.0 40.0 50.0 64.6	944.9 878.6 873.7 800.9 784.2 794.3	-66.3 -4.9 -72.8 -16.7 10.0 23.1			
		ŞEC	COND CL	OSED-IN			
F	1 2 3 4 5 6 7 8 9 10 11 12 13 14	0.0 8.0 16.0 24.0 32.0 40.0 48.0 56.0 64.0 72.0 80.0 88.0 96.0 104.0	817.3 1746.7 2069.2 2242.1 2345.1 2418.1 2470.8 2510.0 2540.2 2565.5 2586.8 2605.5 2620.4 2633.6 2645.9	929.3 1251.9 1424.7 1527.7 1600.8 1653.5 1692.6 1722.8 1748.2 1769.5 1788.2 1803.0 1816.2	18.1 22.3 25.9 29.0 31.7 34.2 36.3 38.2 40.0 41.5 43.0	1.008 0.746 0.608 0.517 0.452 0.402 0.363 0.331 0.305 0.282 0.263 0.246	

~~~~						
REF		MINUTES	PRESSURE	ΔΡ	<u>t ×Δt</u> t + Δt	1094
G	SEC 16		-IN - CONTIN 2654.4		45.4	0.208

CLOCK NO: 28235 HOUR: 24

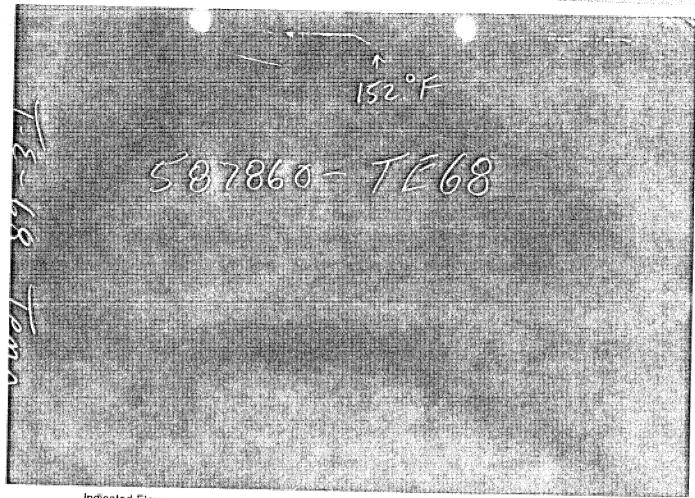


GAUGE NO: 6179

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	7 B	48.0 56.0	2461.4 2502.2	2124.2	29.0	0.403								
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1 : 1 2		80.0 88.0	2581.8 2600.2	2244.5	38.2	0.282								
13		96.0	2614.6	2263.0 2277.4	40.0 41.6	0.263								
14 15		104.0	2629.7	2292.5	41.6	0.246 0.232								
10		112.0	2641.2	2303.9	44.3									

REMARKS: FLOW READINGS MAY BE QUESTIONABLE

		0.0.	1.0.	LENGTH	DEPTH
	DRILL PIPE	5.000	4.276	6100.0	
0	IMPACT REVERSING SUB	6.000	3.000	1.0	6089.0
	DRILL COLLARS		3.000	180.0	
	CROSSOVER		3.000	0.9	
	HANDLING SUB & CHOKE ASSEMBLY	5.750	2.250	4.6	
	AP RUNNING CASE	5.000	3.000	<b>4.</b> 2	6274.0
0	DUAL CIP SAMPLER	5.000	0.750	7.0	
D	HYDROSPRING TESTER	5.000	0.750	5.0	6288.0
	AP RUNNING CASE	5.000	3.000	<b>4.</b> 2	6290,0
	JAR	5.000	1.750	5.0	
	VR SAFETY JOINT	5.000	1.000	2.8	
	OPEN HOLE PACKER	7.750	1.530	5.8	6302.0
	OPEN HOLE PACKER	7.750	1.530	5.8	6308.0
	ANCHOR PIPE SAFETY JOINT	5.000	1.250	4.2	
	FLUSH JOINT ANCHOR	5.000	2.370	46.0	
	TEMPERATURE RUNNING CASE	5.000	2.440	4.6	6365.0
D	BLANKED-OFF RUNNING CASE	5.000		3.9	
0	BLANKED-OFF RUNNING CASE	5.000			6369.0
		- 5 5 5		4.1	6373.0



Indicated Flow Capacity

$$kh = \frac{1637 Q_g T}{m}$$

md-ft

Average Effective Permeability

$$k = \frac{kh}{h}$$

md

Skin Factor

$$S = 1.151 \left[ \frac{m(P^*) - m(P_f)}{m} - LOG \frac{kt}{\phi \mu c_f r_w^2} + 3.23 \right] - -$$

Damage Ratio

$$DR = \frac{m(P^*) - m(P_f)}{m(P^*) - m(P_f) - 0.87 \text{ mS}}$$

Indicated Flow Rate (Maximum)

$$AOF_1 = \frac{Q_g m(P^*)}{m(P^*) - m(P_f)}$$

MCFD

Indicated Flow Rate (Minimum)

$$AOF_2 = Q_g \sqrt{\frac{m(P^*)}{m(P^*) - m(P_f)}}$$

MCFD

Approx. Radius of Investigation

$$r_i = 0.032 \sqrt{\frac{kt}{-\phi\mu c_t}}$$

ft

### DIVISION OF OIL AND GAS

### Report on Operations

Jeff Greening, Agent		
AMERICAN HUNTER EXPLORATION,	LTD. Coalinga	Calif.
611 E. Clay, P. O. Box 468	June 25.	Caiu.
Colusa, CA 95932		
Your operations at well "Souza"	1 API No	019-21924
Sec. 36, T.14S, R. 12E M.D. B.& M. were witnessed on 6/19/84	Field, in	
were witnessed on 6/19/84	. T.S. Boar	cdman manuscratti C
the supervisor, was present from 1300 Engineer.	to <u>1900</u> . There were a	lso present <u>Dave Gunderson</u> ,
Present condition of well: 9-5/8" cem. 1	709'; 5-1/2" 10,213', c.p.	10,061'-10,060', 9871'-
<u>9870', 9468'-9467', 9352'-9351', 6</u>	5553'-6552'. 6411'-6410' 14	100! perfs 10 0/5! 9967!
<u>9632'-9689', 9423'-9380', 9199'-9</u>	L59', 6491'-6466', 6330'-63	310' T.D. 10 217'
<u>bridge plug 10.1//, 96/0, 9145</u>	. 6401' - Retainer 9862' C	9460! 6545! Plugged
$\frac{\text{W}/\text{30 sx of cem. below } 9862^{\circ}, 50 \text{ s}}{}$	c of cem. below.9460'. 50 s	ex of cem. below 9340'.
rrugged with cem. 6330'-6155', 140	00'-1200'-, 90'5'.	
The operations were performed for the purpo	se of <u>abandonment.</u>	
DECISION: THE PLUGGING AND CEMENTI	NG OPERATIONS AS WITNESSED	AND REPORTED ARE APPROVED.
TSB/bcm		
cc: Company, Canada	sure of	
,, ,	and the same	
	460	
DEFICIENCIES CORRECTED		
None		
DEFICIENCIES TO BE CODDECTED		

M. G. MEFFERD

State Gil and Cas Supercishr

By

Richard F. Curtin - Deputy Supervisor (for)

None

CONTRACTOR: Ganache Well Service, Inc.

### DIVISION OF OIL AND GAS Cementing/Plugging Memo

API N	No	219	ican Hunter 1924				Sec.	36	9	P 145	D 178	m.D	· B&M	
Field	1			, Co	unty	Fresmo			•	On 3:	ane 19. 1	984		
There	were	e als	o present	, rep Dave	resent Gunde	ative ( r≤o~/	of the s	superv	1801	r was p	resent f	com <u>1300</u>	<u>to 1900.</u>	
Casir	ng rec	cord	of well: 9	sk"cem	1709	51/2"ce	FW 10513	5 cp //	006/	-10060	9871-987	0,9468	-9467 <u>/ 935</u> 2	
<u>9351,</u>	6552	655	2 6411-6411	5 Perfs	10045	<u>-996</u>	7, 9832	-9689	94.	<u> 20 - 40</u>	80, 9199	-9159	6491-6466	
6330	-6310	·	771501 GT	BP 101	77, 967	10, 9145,	6401 Ret	ALART 9	862	19460%	6545.	Pl	ugged w/	
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6330	<u>-615</u>	<u> </u>	400-12007	, 907-	5		4							
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PERN	IIT TO	CONDU	JCT W	ELL (	OPE	RAT	IONS	(field	code)
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								Ab	d
Jeff Greening, Agent	·							(new po	ool code
AMERICAN HUNTER EXPLO	RATION LTD.	40000000 og en og gjander						(old po	ol code)
306 Pescado Circle				_	Coa	linga,		, C	alifornia
Rancho Murieta, CA 9	5683			•••			3, 1986		
Your	proposal to_	ABANDO	ON	well_	I	''Souza'	<u>'</u> 1		_
A.P.I. No. 019-21924	,	Section	36, T	<u> 148</u>	_, R	12E	M.D.	B. & M.,	,
ung Nija din nija din qua, tiki sela sena sena suna		d	100 OND DEG COS DOG AND DEG		are	2		-	pool,
Fresno Count lled in this office.	y, dated <u>11/</u>	12/85_, red	ceived <u>1/2</u>	7/85_h	as been	examine	ed in conju	nction with	records

THE PROPOSAL, COVERING WORK ALREADY COMPLETED IN ACCORDANCE WITH PRIOR AGREEMENT, IS APPROVED.

Blanket Bond CP/bcm cc: Company, Canada

A copy of this permit and the proposal must be posted at the well site prior to commencing operations.

Records for work done under this permit are due within 60 days after the work has been completed

### RECEIVED

### STATE OF CALIFORNIA DEPARTMENT OF CONSERVATION

### DIVISION OF OIL AND GAS

JAN 27 1986

DIVISION OF OIL & GAS

(Date)

### Notice of Intention to Abandon Well

This notice must be given at least five days before work is to begin.

			FOR DIVISION	USE ONLY						
	DIVISION OF OUR AND ORG		CARDS BOHO	FORMS OGD/14 OGD12/						
	DIVISION OF OIL AND GAS									
	In compliance with Section 3229, Division 3, Public Resour	rces Code, notice	is hereby given that	it is our intention						
	to abandon well AMERICAN HUNTER SOUZA #1									
	Sec. 36, T. 14S, R. 12E, MD B. & M.,	Fie	ld, FRESNO	County.						
	commencing work on NOVEMBER 4th , 19 83	<u>3</u>								
	The present condition of the well is: Plugged & Abandone	Additional	data for dry hole (s	show depths):						
	1. Total depth 10,217	5. Oil or gas	shows	070 -1						
	2. Complete casing record, including plugs and perforations	DST #1: 620	71-6249 Moreno, 18-6373 Moreno	GTS - 5' flame GTS - 750 MCF	5					
	Casing: 9-5/8", 36#/ft, K55, LT&C @ 1709'	DST #3: 646	3-6512 Moreno.	GTS - 400 MCF						
	5-1/2", 20#/ft, 180, 1T&C @ 10213'	#DST #4 #5.	0156 0200 15+	huan MD						
	Perfs: Lathrop 9990-9999,9975-9986,9967-9971 Set cement retainer @ 9862',	DST #6, #7,	#8: 9382-9433	, 9652-9778 Lat	throp-MR					
	squeeze 6 bbls. cement									
	Lathrop 9832-9698, 172 shots	6. Stratigraph	ic markers	Moreno Shale	5130					
	Set bridge plug @ 9670'	Tumey	2572	Bluewett	6540					
	3. Last producedN/A cont'd below	11	•	Tracey	7437					
	(Date) (Oil, B/D) (Gas, Mcf/D) (Water, B/D)	Domengin	e 3655	Lathrop	9159					
	or .	7. Formation	and age at total dep	th						
	4. Last injected N/A  (Date) (Water, B/D) (Gas, Mcf/D) (Surface pressure)	S Boss of Care	Lathrop	1700'						
	The proposed work is as follows:	o. Dase of fres	n water sands	1700						
Perfs:	Lathrop 9380-9423, 86 shots									
	Set cement retainer @ 9340'									
	Squeeze 50 sks cement									
	Lathrop 9192-9199, 9182-9185, 9159-9176, 57 st	nots								
	Set bridge plug @ 9145' Moreno 6491-6466									
	Set bridge plug @ 6401'									
	Moreno 6310-6330									
	Spot 6 bbls. cement across perfs									
	9-5/8"-5-1/2" Casing Annulus: 1399-1400									
	Circulate 15 bbls. cement between casings									
	inside 5-1/2" tasing: Spot 2 bbls. cement in casing 39									
	5' - 30'. Cut off casing 6' bel level.	ow ground								
	It is understood that if changes in this plan become n	ccessary we are	to notify you imm	nediately						
	Address 435 - 4th Avenue S W		R EXPLORATION	-						
	Calgany Albaira Tan ano	DAY CUEDE	(Name of Operator)							
	(City) (State) (Zip)	MAI SHEPE	(Print Name) 85							
	Telephone Number <u>(403)</u> 260-1824	MANIMIN	85	-11-12						

[Area Code]

00100 1010 1 1011100 10111

(Number)

10,213

### MEMORANDUM OF TELEPHONE OR PERSONAL CO. VERSATION

		COALING	Lite.	_, Calif.
		JUNE	18	1984
Operator AMERICAN HUNTER	Well No	"Souza"		ogicagan a saliquid de gran a silviador monorque
Field FRESNO COUNTY	Sec. 36	T. 145. R. 1	S. E	1. D. B&M
personal A telephone conversation was held, concer	rning above	well, with	Mr. Dave	GUNDERSE
for above operate	or on Jon	e 18	ල 19 <u>_84at_</u> 8	BAO A.M.
Details of the conversation were as follo				
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# MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION

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# MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION (Proposed Well Operations)

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'ield	Sec.	T.	R * *	B&M
personal telephone conversation was held, con	ncerning ab	ove well,	with Mr.	
for above oper				
Details of the conversation were as fo	ollows:			
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Oil or gas showings				
Results of tests				
Stratigraphic markers				
Geologic age at bottom			of fresh water_	
Operator proposes the following work:	:			
	-			
Additional requirements outlined:				
Test of W.S.O. to be witnessed by D.	O.G. at	en mandarit er fall der fall der er eine spellen fall der eine der eine der eine der eine der eine der eine de	By operator at	
Plugs to be located by D.O.G. at		Ву ој	perator at	
Notice to be filed immediately ( )	Yes ( )	Not neces	sary	
Other data				
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## MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION

		COALINGA	, Calif.
		APRIL 26	
Operator American Hunter	Well No.	Souza' 1	
Field FRESNO COUNTY personal	Sec. 34	T. 145 R. 12 E.	M.D. B&M
A telephone conversation was held, o			
		er Z6, 1984	
Details of the conversation were as			**************************************
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# MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION (Proposed Well Operations)

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## MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION

	COALINGA, Calif.
	DECEMBER 7 1983
Operator AMERICAN HUNTER	
Title 1 or at Section co.	Sec. 36 T. 145, R. 12E. M. D B&M
A telephone conversation was held, concer	ming above well, with Mr. Down Marco
(403) 260-1740 for above operato	or on December 7 1983 at 3:00 P.M.
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## MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION (Proposed Well Operations)

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## américan hunter

TRANSMITTAL		
TO: State of California	DATE	: April 191984
Oil and Gas Commission		
PO Box 60 RE: WELL NAME: Amorron Auster Souze	<b>₩</b> 1	
Coalunga, CA 93210 50 36- II45, RIZE, F	<u>.</u> <b>2</b> :5/\@	Co.,ca
ENCLOSED PLEASE FIND THE FOLLOWING:		
1. copies of A.F.E. for		
2. copies of Survey Plan		
3. copies of Well Licence Application		Park Pro-
4. copies of Geological Prognosis and Drilling Program		
5. copies of Approved Well Licence		
6. copies of Field Prints of Logs	1	
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9 copies of Drilling/Completion Report		
10 copies of Fluid (gas, water, oil) Analysis		
11. copies of Geological Report		
12. copies of Core Analysis/Description		
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Sent by James M. trucker	ž.	
REMARKS: The Division of Oil and Gas requires duplicate set	s of	records,
logs, histories etc. Please send 1 more set of al	1 10	gs listed above.
RECEIVED W: 7.5, Bondman DATE: 4/26	64	Thank you
DIMER ACCION DECETED BY SECUING AND DETICIPATING T	Ne .	

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#### DIVISION OF OIL AND GAS

## Report on Operations

AMERICAN HUNTER EXPLORATION, LTD. 611 E. Clay, P. O. Box 468	Coalinga, November 10, 1983					
Colusa, CA 95932						
Your operations at well "Souza" 1 Sec. 36, T.14SR. 12E, M.D. B.& M were witnessed on 11/8/83 the supervisor, was present from 0130 to 0327 Pusher for Montgomery Present condition of well: 9-5/8" cem. 1709'. T.D.	Field, in Fresno C. Parli There were also present	County,, representative of Joe Lindsey,				
The operations were performed for the purpose oftestingand_installation.  DECISION: THE BLOWOUT PREVENTION EQUIPMENT AND						
CP/bcm cc: Company, Canada						
DEFICIENCIES CORRECTED None						
DEFICIENCIES TO BE CORRECTED None						
CONTRACTOR: Montgomery Drilling						

By Deputy Supervisor (for)

Richard F. Curtin

OG109(12-80-15M)

#### DIVISION OF OIL AND GAS WOUT PREVENTION EQUIPMENT MEMC

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OGD 9(5-79-DWRR-3M)

# DEFICIENCIES - TO BE CORRECTED NONE

DEFICIENCIES - CORRECTED NONE

CONTRACTOR MONT Gomery Drilling

REPORT ON PROPOSED OPERATION	(field code)
	(area code)
	(new pool code)
Jeff Greening, Agent	adas card
AMERICAN HUNTER EXPLORATION LTD.	(old pool code)
P. O. Box 468 Coalinga,	, California
Colusa, CA 95932 October 13	3, 1983
Yourproposal todrillwell"Souza"	1
A.P.I. No. 019-21924 , Section 36 , T. 14S , R. 12E	
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Fresno County, dated 10/6/83 , received 10/12/83 has been examine	ed in conjunction with records
filed in this office.	

#### THE PROPOSAL IS APPROVED PROVIDED:

- Sufficient cement shall be pumped back of the 9-5/8" casing to fill to the surface.
- Mud fluid of sufficient weight and proper consistency to prevent blowouts shall be used in drilling, and the column of mud fluid shall be maintained to the surface at all times, particularly while pulling the drill pipe.
- Blowout prevention equipment conforming to Division of Oil and Gas Class III A 3M is installed on the 9-5/8" casing and maintained ready for use at all times. Copy of requirements is enclosed.
- Blowout-prevention practice drills are conducted at least weekly and recorded in the log book.
- Sufficient cement shall be used to fill the annular space behind the 5-1/2" casing to at least 500' above oil and gas zones and excessive pressure intervals.
- THIS DIVISION SHALL BE NOTIFIED: 6.
  - TO WITNESS a pressure test of the blowout-prevention equipment prior to drilling out the shoe of the 9-5/8" casing.
  - TO WITNESS a test of the 5-1/2" water shut-off immediately above the objective zone.

NOTE: To contact this Division call (209) 935-2941.

Blanket Bond VEV/bcm cc: Company, Canada

M. G. MEFFERD, State Oil and Gas Supervisor

A copy of this report and the proposal must be posted at the well site prior to commencing operations.

Records for work done under this permit are due within 60 days after the work has been completed or the operations have been suspended.

RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

Notice of Intention to Drill New Well

DIVISION OF OUR

	-	. INFORMATION	W)		FOR DIVISION US	SE ONLY	
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I depth immediately  I, Individual, etc.)	groum  ft. 3  ft. 3  ,200  Code 2P 3.



Resources and Development Department

#### WAIVER OF APPEAL PERIOD

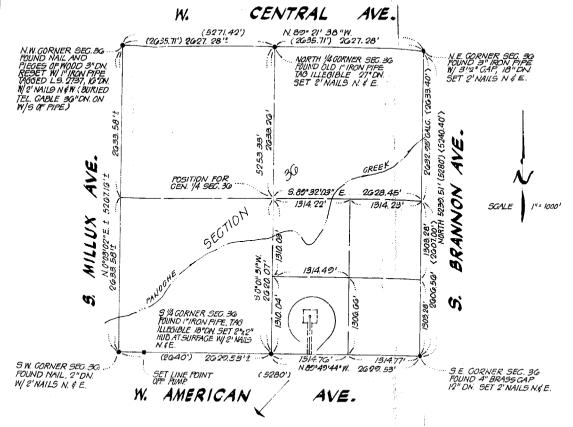
Application	CUP	\$2016	
Date Approved _		2/63	MINAGAMAN
Required Appeal	Period	15 DAYS	-

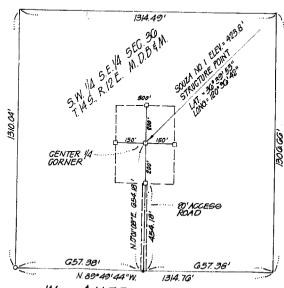
The undersigned hereby agrees to meet all the requirements of the above approval, and requests the Director of the Resources and Development Department of the County of Fresno to issue all necessary construction permits and perform the necessary construction inspections to determine Code compliance authorized by the above approval prior to the expiration of the required appeal period.

The undersigned further agrees that should the above application not become effective for any reason, the permittee or owner shall remove any improvements or construction authorized by this application (if in conflict with existing zoning regulations) within 30 days after written notice from the Director of the Department of Resources and Development, and restore said property as nearly as practicable to it's prior condition.

The undersigned further agrees to hold the County of Fresno harmless for any damages incurred in the event the removal of the improvements are required as provided above; the undersigned also agrees to pay all costs of court and counsel incurred in the event legal action is required to enforce the provisions of this waiver.

Owner's Name	Permittee's Name EXPLORATION LTP.
Signed	Signed & Mulinbla
Date:	Date: 02/2/1983
Accepted By	Date: 10/12/63,





W. AMERICAN SCALE : 1"= 300"

#### LEGEND

- CORNERS FOUND AND ACCEPTED AS NOTED
- SET I"X 2" STAKES, FLUSH
- DATA PER GOVERNMENT SURVEY
- DATA PER SCOTT MCKAY RECORD BK. GQ FG. 14 MARCH 1912.
- SET NAIL AND TIN

### MAP OF SURVEY OF SECTION 30, T.145, R.12E., M.D.B. &M.

for AMERICAN HUNTER EXPLORATION L.T.D.

W.O. DENTRY 4780 E. TULARE AVE. TELEPHONE

LIGENGED LAND SURVEYOR FRESNO, CALIFORNIA 93702 (209), 251-7527

# APPENDIX 3 CALGEM RECORDS - BENDER SILVER CREEK 57X-18

#### SUBMIT IN DUPLICATE

#### RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

## History of Oil or Gas Well

	Operator NAHAMA & WEAGANT ENERGY COMPANY Field CHENEY RANCH GASCOUNTY FRESNO Well CHENEY RANCH 57X-18  A.P.I. No. 019-20736 Sec. 79., T 14S., R 13E., MD. B. & Name TRENT ROSENLIEB  Date JULY 9, 1991 (Person submitting report) Title VP ENGINEERING (President, Secretary or Agent)	
	Signature Frent Rosenlier	O?
	602 "H" Street, Bakersfield, CA 93304 (805) 323-9075	
Date	History must be complete in all detail. Use this form to report all operations during drilling and testing of the well or during redril of cement used, top and bottom of plugs, perforation details, sidetracked junk, bailing tests and initial production data.	lling unts
	ABANDONMENT HISTORY	)
<u>1991</u>	SEP 0 1 199;	
4/30	Road rig to location 3 hrs. Move in and raised hoist. RIGNOUT GUL & GAS wires, set circ. pump. Set out pump lies & tie to water tank.  Pulled 123 7/8" x 30' rods. EOT 7:00 p.m.	У
5/1	7:00 a.m. removed tee, worked stuck csg. donut loose. Installed BOPE. Attempted to release packer with no results, worked packer to 70,000# (shear 60,000#). Pumped down annulus & pressure to 1000 p.s.i., casing standing full. Worked packer, fluid in annulus dropped. Pumped 70 BW into annulus at 1000 to 1200 p.s.i. No returns SI well, EOT 5:30 p.m.	0
5/2	Commenced operations 7:00 a.m. Rigged up & ran 1 9/16" over-shot grapple and engaged rod fish @ 3690'. Worked fish, slipping off fish and was unable to get back over. POOH with tools and found grapple bent. RIH with 1 7/16" slips and was unable to get over the pooh. RIH with 1 1/2" spiral grapple, engaged fish but was unable to hold on. POOH, SI well, EOT 6:30 p.m.	
5/3	Commenced operation @ 7:00 a.m. Ran 1 9/16" overshot with grapple. Engaged fish. Tools slipping off. POOH, SI well & shut down rig 11:00 a.m.	
/6	Commenced operations @ 8:30 a.m. Ran a 1 1/2" O'Bannion overshot grapple. Engaged fish and could hold on. POOH ran a 1 3/8" - 1 1/2" slip type overshot and was unable to engage fish. POOH. Ran a 1 5/8" O'Bannion overshot grapple. Engaged fish but was unable to hold fish. Good bite. POOH. SI well FOT 6:30 m.	

to hold fish. Good bite. POOH, SI well. EOT 6:30 p.m.

5/1

5/2

5/3

5/6

## RECEIVED

#### Page 2 Cheney Ranch 57X-18 Abandonment

## CEP 0 1 1991 DIVISION OF OIL & GAS

- Commenced operations 7:00 a.m. Ran a 1 9/16" Bowen spiral grapple. Engaged fish, good bite but slipped off. Unable to get back on fish. POOH and found spiral grapple broken and out of overshot barrel. Ran a second 1 9/16" spiral grapple. Engaged fish, tools acted exactly like 1st run and found in same condition when POOH. Ran a 1 5/8" Bowen spiral grapple and engaged fish. Good bite. Increased pull in increments to 30,000# when grapple failed. POOH and found spiral grapple out of overshot.
  - Rigged up to attempt jarring packer out of hole. Worked tbg for 1.5 hrs, rotating and jarring packer. Packer came loose @ 5:30 p.m. Pulled tbg to rod fish. SI well, EOT.
- Commenced operations 7:00 a.m. Stripped out rods w/ tbg Ran 2" open ended tbg to 7339'. No fill. Pulled 5 stands. SI in well, EOT 4:30 p.m.
- Commenced operations @ 7:00 a.m. Ran in 5 stands tbg to 7339' 5/9 Rigged up Halliburton and pumped in 10 bbls fresh water ahead of 40 c.f. Class "G" cement. Displaced cement with 150 c.f. water. Pulled 10 stands tbg and cleared tbg with water. CIP @ 9:20 a.m. W.O.C. Layed down 7/8" rods. Ran tbg to top of hard cement @ 7124'. The location & hardness of cement plug was witnessed & approved by Glenn Muggelberg, from the D.O.G. Displaced hole fluid with 135 bbls 72#/cf drilling mud. Mud was approved by D.O.G. representative. Layed down 180 jts. of tbg on trailer. shot at 1400' was witnessed & approved by D.O.G. representative. Rigged out wireline. Ran open-ended tbg to 1399'. Rigged up Halliburton and pumped in 2 bbls water ahead of 26 cf Class "G" cement mixed with 3% CaCl2. Displaced cement with 4.5 bbls water. Pulled 10 stands of tbg & cleared tbg with water. Rigged out Halliburton. Closed well in. EOT 10:00 p.m.
- Commenced operations 7:30 a.m. Ran tbg to tag cement plug. The location and hardness of cement plug at 1291' was witnessed and approved by Glenn Muggelberg of the D.O.G. Displaced hole fluid with 72#/cf drilling mud approved by D.O.G. representative. POOH with tbg laying down on trailer. Installed a cmt wiper plug @ 50'. Released rig at 2:30 p.m.
- Commenced operations 8:00 a.m. Loaded out rod bundles on Oilfield Express trailer plus miscellaneous wellhead equipment. Cut csg head off 6' below ground level. Dumped ready mix cement in well from 50' to surface. Welded a steel plate with well no. on plate over casing stubs. D.O.G. representative Michael Woods witnessed & approved surface abandonment operations. Operations complete 2:00 p.m.

#### RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

Vo.	T	591-260
	-	

## **Report on Operations**

Charles F. Green CENCAL DRILLING INC. 1224 Coast Village Circ	le <u>1119 20, 1991</u>	Calif.
were witnessed on May 17, 1991 the supervisor, was present from There were also present Scotty Present condition of well: 16" across	Creek" 57X , API No. 019 , M.D. B. & M. Cheney Ranch Fresno M. Woods 1045 to 1110 Helton for Nahama & Weagant Energy 30'; 9 5/8" cem. 1693'; 5½" cem.	County, , representative of rgy Co.
The operations were performed for the	Durpose of abandonment.	
DECISION: THE PLUGGING OPERA	FIONS AS WITNESSED AND REPORTED A	RE APPROVED.
UNCORRECTABLE DEFICIENCIES:	Used aggregate cement slurry (no for surface plug.	t sand cement)
CONTRACTOR: Pride Petroleum	Service.	

MW/jp

M. G. MEFFERD

State Oil and Gas Automist

By Deputy Supervisor

RICHARD F. CURTIN



### DIVISION OF OIL AND GAS Cementing/Plugging Memo



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UNCORRECTABLE DEFICIENCES

Vses aggregate cament sturry (not sand severes) for surface plug

CONTRACTOR

Pride Petroleum Services



## PANOCHE CREEK FARMS - FIREBAUGH, CALIFORNIA

February 19, 1993

Mr. Roy Houde Department of Conservation Division of Oil and Gas 466 North Fifth Street Coalinga, CA 93210

Dear Mr. Houde:

Attached is a letter dated December 28, 1992 pertinent to CenCal Drilling locations 57x, Sec. 18, 14/13 and 77x, Sec. 19, 14/13.

Please be advised that Panoche Creek Farms is the surface owner of these well locations. Panoche Creek Farms has requested that the tank at well 77x be left for Panoche Creek's use, as well as other equipment mentioned in the letter pertaining to both 77x and 57x. Any equipment or material not used by Panoche Creek Farms will be removed by Panoche Creek Farms.

Very truly yours,

John D. Blackburn

Attachment

134

00

(field code)

## PERMIT TO CONDUCT WELL OPERATIONS

	(area code)
	Abd
Rocky Rasley, Agent	(new pool code) 05
NAHAMA & WEAGANT ENERGY COMPANY	
602 IIII Stroot	(old pool code)
Rekerafield CA 02204	, California
April 26, 1991	, ountillia
Yourproposal toabandonwellSilver Creek" 573	Inc.
Cheney Ranch Gas Section 18 , T. 14S , R. 13E , MD B	. & M.,
Fresno County dated 4/24/91 4/25/01, area, (V) Cretaceous	pool,
Fresno County, dated $4/24/91$ , received $4/25/91$ has been examined in conjunctified in this office.	ion with records

THE PROPOSAL IS APPROVED PROVIDED:

- Blowout prevention equipment conforming to CDOG Class II 2M requirements is installed on the 5 1/2" casing and maintained ready for use at all times.
- All portions of the well not plugged with cement are filled with inert mud fluid having a minimum density of 72 lbs./cu. ft. and a minimum gel-shear strength (10 min) of 20 lbs./100 sq. ft.
- Freshwater deposits are protected by squeeze-cementing through perforations at 1400' or by placing a cement plug across a cavity shot at that depth. In either case, cement must fill the casing to at least 100' feet above the perforations or cavity shot.
- The proposed cement plug from 1800' to 1500' extends from 1400' to at least 1300'. 4.
- THIS DIVISION SHALL BE NOTIFIED: 5.
  - To witness the location and hardness of the cement plug from 7340' to 7040'.(7189')
  - To witness the mudding of the well.
  - To witness the cavity shot on squeeze cementing at 1400'.
  - To witness the location and hardness of the cement plug from 1400' to 1300'. d.
  - To witness the placing of the cement surface plug from 50' to 5' including all uncemented annuli.
  - When the well site has been restored to a condition that will pass environmental f. inspection.

This Division does not pass upon your right to enter the property, but merely NOTE: approves the proposal as conforming to our requirements.

The base of the usable freshwater.

Engineer Glenn Muggelberg

Phone (209) 935-2941 Cencal Drilling, Inc. M. G. MEFFERD, State Oil and Gas Supervisor

Deputy Supervisor

(FOR) RICHARD F. CURTIN

A copy of this permit and the proposal must be posted at the well site prior to commencing operations.

Records for work done under this permit are due within 60 days after the work has been completed or the operations have been suspended.

## STATE OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

## Notice of Intention to Abandon Well

	FOR DIVISION USE ONLY
	CARDS BOND FORMS OGD114 OGD1
DIVISION OF OIL AND GAS	000114 0001
In compliance with Section 3229, Division 3, Public Reso	urces Code, notice is hereby given that it is our inten-
o abandon well Cheney Ranch 57X-19 Silu	(And N) 57 V DIA 200
140 175 175	API No. CO 19 - WO 1
iec. , T. 14S, R. 13E, M.D. B. & M., Cheney Ra	ınch Gas Field, Fresno Cou
ommencing work on May 1 , 19_5	91
The present condition of the well is:	Additional data for dry hole (show depths):
. Total depth 7500 t	
	5. Oil or gas shows
<ul> <li>Complete casing record, including plugs and perforations (present hole)</li> </ul>	
5/8" csg cmt'd @ 1693'	
1/2" csg cmt'd @ 7357' JHPF 7327'-7335'	6. Stratigraphic markers
Last produced 9/85 42 581 1100  (Date) (Oil, B/D) (Gas, Mcf/D) (Water, B/1	
(Date) (Oil, B/D) (Gas, Mcf/D) (Water, B/I Or	7. Formation and age at total depth
	7. Tornation and age at total depth
(Date) (Water, B/D) (Gas, Mcf D) (Surface pressure	8. Base of fresh water sands est. 1650'
Is this a critical wall according to the deficient	
Is this a critical well according to the definition on the	ne reverse side of this form? $\square$ $X$ Yes No
he proposed work is as follows:	
Place cement plug from 7340' - 7040'. Change hole over to 72 pcf drilling mud.	
Place cement plug from 1800' - 1500'	_
Place cement plug from 50' - surface. Cut off casing 5 feet below surface,	RECEIVED
weld steel plate on casing stub.	APP 2 5 ··
Restore location.	APR 2 5 1991
	DIVISION OF OIL & GAS
It is understood that if changes in this plan become	
It is understood that if changes in this plan become	necessary, we are to notify you immediately.
ldress 602 "H" Street (Street)	Nahama & Weagant Energy Company (Name of Operator)
Rakersfield, CA 93304 (City) (State) (Zip)	By Trent Rosenlieb
{City} {State} {Zip}	[Print Name]

(Area Code)

OG108 (2/84/DWRR/5M)

(Number)

(Signature)

DIVISION OF OR AND CAS

RECEIVES

JAN 17 1974

WOODLAND, CALIFORNIA

PACIFIC GAS AND FLECTRIC CO. DEPT.OF FEGINFERING CENEARCH

FR STANCE, CON THE ANALYSIS OF BASTSASPLE

SAYPLF IDENTIFICATION: CHERRY RANCH FIELD, SAN MOADLIN DIVISION RENDER 57X18

Silver French LAR. NO. 73-796

DATE SAMPLED JUNE 13 1973

DATE ANALYZED JUNE 29 1973

GAS DHASE COMPONENT

UNLUME 更至ACTION

CALCULATED SPEC. GRAV.

CALCULATED BTUZCU.FT.

CAPPON DIOXIDE

0.0037

0.674

1167.1

NITPOGEN

0.0149

METHANE

0.8617

ETHANE

0.0544

PROPANE

0.038

ISO-BUTANE

0.0104

N-BUTANE

0.0101

ISO-PENTANE

0.0034

N-PENTANE

0.0022

HEXANES

0.0012

TOTAL

1.0000

歌欢烟篇意

Constitution assistances

ANALYST

3 HIRING GEOFFINECHINKEN.

2

DISTRIBUTION:

CELanthier/MRLee

S.A. PHANVÍRZOTE . RENTZ E.F. FOLICY ZE. A. BETTERZE. A. COOK PARTY 1 TOP O

#### RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION DIVISION OF OIL AND GAS

## REPORT OF WELL PLUGGING AND ABANDONMENT

Charles F. Green CENCAL DRILLING, INC. 1224 Coast Village Circle Santa Barbara, CA 93108

Coalinga, California March 1, 1993

Your report of abandonment of well	"Silver Creek" 57X
A.P.I. No. <u>019-20736</u> , Section _	18 , T. 14 S, R. 13 E. M.D.B. & M.
field,field,	Fresno County
dated <u>July 9, 1991</u> , received _	September 1, 1991 , has been examined
in conjunction with operations witness	sed and records filed in this office.
we have determined that all of the red	quirements of this Division have
been fulfilled.	

NOTE: Surface plugging completed on May 17, 1991.

CP/kt
cc: Cons. Committee
PI
Well File

WILLIAM F. GUERARD, JR.

ACTING STATE OIL AND GAS SUPERVISOR

By RICHARD F. CURTIN

DEPUTY SUPERVISOR

OG159

## SION OF OIL AND G

## WELL SUMMARY REPORT

SUBMIT IN DUPLICATE

	18 T.	145 R.	13E	M.I	) B. & M,	Cheney I	Ranch)	FieldFI	resno	County.
Loca	tion 660' N	orth & Ta	980' West	t fro	m S.E.	Corner	of Sec	. 18.		
7 y 139 14 4 <del>4</del>						ty or section corner,			357 feet	A - year which control and the property and
All d	epth measureme	ents taken from							6 feet al	
In preser	compliance with	h Sec. 3215, of the well and all	the Public Re-	SOurces	Code the	nformacion				ecord of the
Date.	8/2/73						Signed.	ž	<u>. 16. 12</u>	e ^r
Fı	ed Green									
т Английн ав архионали уудаг	(Engineer or G	eologist)		(5	uperintenden()		Title	Vice Pre	SLOENT , Secretary or Agent)	
Comr	nenced drilling_	4-24-73		-			GEOLOGICAL	MARKERS	D	EPTH
Comp	leted drilling	5-11-73	The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	and the second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second s		4. y.	p Crety	rations Ge	n Grad	
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		production	Clean Oil bbl. per da	y	Gravity Clean Oil	Per Cent Water including emulsio	on Mer.	Gas	Tubing Pressure	Casing Pressure
	Initial	production	Clean Oil bbl. per da	y in w	Gravity Clean Oil 60° aiting	Per Cent Water including emulsio	55 & E.	Gas	Tubing Pressure	Casing Pressure
of Casing	Initial	production	Clean Oil bbl. per da  10 Shut	in w	Gravity Clean Oil 60 aiting RECORD (	Per Cent Water including emulsio  none  on P.G.  Present Hole)	on Met. 55	Gas	Tubing Pressure	Casing Pressure
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of Casing P. U. 5/8"	Initial Production a  Depth of Shoe 1693	production fter 30 days  Top of Casing  Surf.	Clean Oil bbl. per da  10 Shut  Weight of Casing	in W  Casing	Gravity Clean Oil  60° aiting RECORD ( lew or and Hand H.	Per Cent Water including emulsion none on P.G.  Present Hole)  Seamless or Lapweld Smls	on Met. 55 & E.  Grade of Casing	Gas per day  O  Size of Holy Drilled	Tubing Pressure  2620  Number of Sacks of Cement  905	Casing Pressure  2750  Depth of Cementing
of Casing P. U. 5/8"	Initial Production a  Depth of Shoe 1693	production fter 30 days  Top of Casing  Surf.	Clean Oit bhl. per da  10  Shut  Weight of Casing  53.5#	in W  Casing	Gravity Clean Oil  60° aiting RECORD ( lew or and Hand H.	Per Cent Water including emulsion none on P.G.  Present Hole)  Seamless or Lapweld Smls	on Mer.  55 & E.  Grade of Casing  J-55	Gas per day  O  Size of Hol Drilled  13-3/4	Tubing Pressure  2620  Number of Sacks of Cement  905	Casing Pressure  2750  Depth of Cementing
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of Casing P. U. 5/8"	Initial Production a  Depth of Shoe  1693'  7357'	production fter 30 days  Top of Casing  Surf.  13  (Size, top, b	Clean Oil bhil. per da  10  Shut  Weight of Casing  53.5#  15.5 & 17.#	in w Casing Seco	Gravity Clean Oil 60 aiting RECORD ( few or and Hand H W	Per Cent Water including emulsion none on P.G.  Present Hole)  Seamless or Lapweld Smls  H  Casing and spacing of	Grade of Casing J-55 K-55  perforation	Size of Hol Drilled 13-3/4 7-7/8	Tubing Pressure  2620  Number of Sacks of Cement  905 693CF	Casing Pressure  2750  Depth of Cementing of through perforation
of Casing P. (.) 5/8" 1/2"	Initial Production a  Depth of Shoe  1693'  7357'	production fter 30 days  Top of Casing  Surf.  11  (Size, top, b)	Clean Oil bbl. per da  10 Shut  Weight of Casing 53.5#  15.5 & 17#  ottom, perfora	in w  Casing Seco S. Ne	Gravity Clean Oil  60° aiting RECORD ( New or and Hand H.  W ERFORATED Ervals, size:	Per Cent Water including emulsion none on P.G.  Present Hole)  Seamless or Lapweld Sm1s  II  CASING and spacing of continuous foot -	Grade of Casing J-55 K-55  perforation perfor	Size of Holy Drilled 13-3/4 7-7/8 and method.	Tubing Pressure  2620  Number of Sacks of Cement  905 693CF	Casing Pressure  2750  Depth of Cementing of through perforation
of Casing P. (.) 5/8" 1/2"	Initial Production a  Depth of Shoe 1693' 7357'	production fter 30 days  Top of Casing  Surf.  11  (Size, top, b)	Clean Oil bbl. per da  10 Shut  Weight of Casing 53.5#  15.5 & 17#  ottom, perfora	in w  Casing Seco S. Ne	Gravity Clean Oil  60° aiting RECORD ( New or and Hand H.  W ERFORATED Ervals, size:	Per Cent Water including emulsion none on P.G.  Present Hole)  Seamless or Lapweld Smls  H  Casing and spacing of	Grade of Casing J-55 K-55  perforation perfor	Size of Hol Drilled 13-3/4 7-7/8	Tubing Pressure  2620  Number of Sacks of Cement  905 693CF	Casing Pressure  2750  Depth of Cementing of through perforation
of Caring P. (.) 5/8" 1/2"	Initial Production a  Depth of Shoe 1693' 7357'	Top of Casing Surf.  (Size, top, b) ted 7289	Clean Oil bbl. per da  10 Shut  Weight of Casing 53.5#  15.5 &  17#  ottom, perfora 1/2",	in w  Casing Seco S. Ne  Prated inte 4 hol	Gravity Clean Oil  60° aiting RECORD ( New or and Hand H.  W ERFORATED Ervals, size:	Per Cent Water including emulsion none on P.G.  Present Hole)  Seamless or Lapweld Sm1s  II  CASING and spacing of continuous foot -	Grade of Casing J-55 K-55  perforation perfor	Size of Holy Drilled 13-3/4 7-7/8 and method.	Tubing Pressure  2620  Number of Sacks of Cement  905 693CF	Casing Pressure  2750  Depth of Cementing of through perforation

# SUBMIT EN DUPLICATE STATEM SALIFORNIA

### DIVISION OF OIL AND GAS

### PAGE #1

## History of Oil or Gas Well

	Well No. Si	iver Creek No. 57x-18, Sec. 18, T. 14S, R. 13E, B. & M.
	P.O. Box	52, eld, Ca. 93302 805-831-7461 Title
Date	It is of the gree drilling and testing as hole size, formati initial production da	(President, Secretary or Agent)  atest importance to have a complete history of the well. Use this form to report a full account of all important operations during the of the well of during re-drilling, altering of casing, plugging, or abandonment with the dates thereof. Be sure to include such items can test details, amounts of cement used, top and bottom of plugs, perforation details, sidetracked junk, bailing tests, shooting and ta.
1973	Depth	Remarks
4-24	1693'	Tiger Drilling Contractor spudded in at 4:00 AM, with 13-3/4" bit using 4-1/2" drill pipe and water base gel mud. 16" conductor at 30'.
4-25		B-J cementers cemented 45 joints, used 9-5/8" A.P.I. 53.5#, L.T.& C. & Vee thread, range 3, seamless casing, including open guide shoe at 1693' with 390 sacks Class G cement premixed with 390 sacks Diamix
		A and 8% gel, followed by 125 sacks Class G cement treated with 3% CaCl ₂ . Displaced one top rubber plug with 665 cu.ft. mud. Pumped in 25 sacks Class G cement thru l" pipe hung at 90' in annulus. Cement in place at 5 AM. Stood cemented 4 hours. Landed casing and tested B P.O.E. to 1500 p.s.i. Approved by D.O.G. Located top of cement 1680' with 7-7/8" bit.
4-26	3782	Drilled out shoe and drilled ahead with 7-7/8" bit.
4-28	6166'	Drilled 7-7/8" bit. Jacobs Formation logging on at 6112'. Mud 72.5#, Vis. 46.
4-20	7260'	Drilled 7-7/8" hole. Welex logged I-ES 7260-1693'.
5-1	75001	D.S.T7216-7260 - Lynes Tester set dual packers 7210-7216 with tail to 7260', using 4-1/2" drill pins
		including 536' drill collars and 500' water cushion and 5/8" bean. Tool opened 1 hours. Gas to surface 5 minutes with medium to fair blow through out test. Recovered 350'net rise slightly gas cut mud. I.S.I.P. 3213 p.s.i., I.F.P. 483 p.s.i., F.F.P. 312 p.s.i., F.S.I.P. 2584 p.s.i.; initial and final hydrostatic 3962 p.s.i. One hour slow down after pulling packer loose. Drilled ahead with 7-7/8" bit. No shows on mud logger 7260-7500'. Welex logged I-ES - 7490'. Mud 74#, Vis 48, W.L. 6.1 cc.

# SUBJECT IN DUPLICATE PRATE OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

PAGE #2

## History of Oil or Gas Well

	OPERATOR E. A. Bender, Operator FIELD Cheney Ranch
	Well No. Silver Creek No. 57X-18, Sec. 18, T. 14S, R. 13E, B. & M.
	P.O. Box 52,  Bakersfield, Ca.93302 805-831-7461  (Address) (Telephone Number)
Date	It is of the greatest importance to have a complete history of the well. Use this form to report a full account of all important operations during the as hole size, formation test details, amounts of cement used, top and bottom of plugs, perforation details, sidetracked junk, bailing tests, shooting and
1973	<u>Depth</u> Remarks
<b>5-2</b> 5-3	Plugged 7-7/8" open hole with 80 sacks, Class G cement premixed with 80 sacks Diamix A through 4-1/2" drill pipe hung at 7499'. Displaced with 555 cu.ft. mud 30 cu.ft. water ahead and 10 cu.ft. water behind. Cement in place at 8:00 AM. Dowell Cementers. Waited on cement. Location and hardness of plug at 6930'witnessed and approved by Eric Kaarlela, D.O.G. at 1:40 PM. Waiting on orders. New Operations took over at 4:00 PM. Waiting on cement for kick-off plug.
	Filed Form 107 with D.O.G. With opened end drill pipe at 4300' set kick-off plug using 100 sx of class "G" cement with 28% sand, 3% D-33 and 75% D-65 T.I.C. Pumped 100 cu.ft. of water ahead, 132 cu.ft. slurry, 8 cu.ft. of mud, plug in place at 2:30 AM.
5-4 5-5	Ran in the hole to 3870 could not break circulation, pulled out to 3560'; circulating and staging in the hole to 3917' and conditioning mud from 70# to 76#; cleaned out from 3917 to 3999 to top of cement, drilled out medium hard cement from 3999 to 4033', faced off cement from 4033-43'. Circulating and conditioning mud for dynadrill. Picked up dynadrill and ran in and oriented dynadrill due east, Eastman is doing the directional work. (See directional survey tabulation.)
	Drilled to 4338'. Survey at 4308' is N85E - drift angle 80
5-6	Drilled to 4961'. Survey at 4871' is N80E - drift angle 80
57 58	Drilled 668' to 5629'; survey at 5505' is N74E - drift angle 13°.  Drilled 563' to 6192'; survey at 6194' is N82E - drift angle 10° 30'. Jacob's Formation logging is on at 5920'.
5-9	Drilled 630' to 6812'; survey at 6812' is S81E - drift
5-10	Drilled 576' to 7379'; survey at 7101 is S74E - drift angle 90 45'.

#### STATE OF CALIFORNIA

DEPARTMENT OF COMSERVATION

## DIVISION OF OIL AND GAS

PAGE #3

## History of Oil or Gas Well

OPERATOR E. A. Bender, Operator	FIE	LD Cheney	Ranch		
Well No. Silver Creek No.57X-18 , Se				M.D.	
Date	Signed	, e ee aan an an an an an an an an an an an an			в. & М
Bakersfield, Ca. 93302 (805)831-	7461	Title		(President, Secreta)	

It is of the greatest importance to have a complete history of the well. Use this form to report a full account of all important operations during the decilling and testing of the well or during re-drilling, altering of casing, plugging, or abandonment with the dates thereof. Be sure to include such items as hole size, formation test details, amounts of cement used, top and bottom of plugs, perforation details, suderracked junk, bailing tests, shooting and initial production data.

Date 1973

5-10

(Continued)

TD 7379' - circulating and conditioning mud, rigged up Schlumberger, Schlumberger stopped at 6670', ran back in the hole and reamed from 6650' to 6805'; ran back to bottom conditioned mud, circulated, wiped hole 10 stands, ran back to bottom, had 14' of fill, circulated and conditioned mud for 2 hrs..pulled 10 stands and ran back to bottom, found no fill, pulled out, rigged up Schlumberger and ran Borehole Compensated Sonic Log with Caliper and Dual Induction—Laterolog with inear Correlation Log. Ran back to bottom and conditioned mud and circulated for casing; measured casing, casing two joints short.

5-12

5-11

Ran differential fillup shoe (2.15), a pup joint (12.10), float collar (1.65), 27 joints of 5-1/2" 17#, K-55,L.T.& C. casing (1157.02) and 143 joints of 5-1/2" 15.50#, K-55, L.T. & C. (6087.37) and two joints of 5-1/2" 17#, K-55, L. T. & C. casing (84.46) and joint of 5-1/2" 15.50#, K-55 casing, casing got stuck at 7357', could not circulate, after three attempts finally broke circulation - circulated for 2 hours and cemented casing with 143 sx of class "G" cement and 1-1 mixture of Pozmix D 6% gel, 18% salt followed with 200 sx of class "G" neat cement, Pozmix mixture yield 3.23 cu.ft./sx of cement - weight 93#/cu.ft. (total 463 cu.ft.) cement 230 weight 115-117#/cu.ft. - displaced with 1040 cu.ft. of water (calculated displacement 983 cu.ft.) bumped plug with 1800 psi, float held. Waited 8 hours landed casing with a joint* of 15.50#, K-55 casing, flanged up tubing head and tested casing and released rig.

#### Completion

Laid down drill pipe, running casing.

Well pulling crew arrived at 11:00 AM, rigged up pulling unit, picked up 4-3/4" bit and 4, 3-3/16 drill collars and tubing (2-3/8)", 4.70#/ft., N-80 EUE).

5-22

## SUBMIT IN DUPLICATE STATE OF CALIFORNIA

DEPARTMENT OF CONSERVATION

### DIVISION OF OIL AND GAS

PAGE #4

#### History of Oil or Gas Well

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Bender Operator Fullo	Cheney Ranch
Creek No.57X-18, Sec. 18 , T.	145 , R. 13E , M.D. B. & M.
(Telephone Number)	(President, Secretary or Agent)
s, amounts of cement used, top and bottom of plugs, perfe	report a full account of all important operations during the opposition with the dates thereof. Be sure to include such items oration details, sidetracked junk, bailing tests, shooting and
	Bender Operator FIELD Creek No. 57X-18, Sec. 18, T.  19 Signed  1. 93302 (805) 831-7461 To the complete history of the well. Use this form to the during re-drilling alterior of the well. Use this form to the during re-drilling alterior of the well.

1973 Dept

Felt soft cement at 7210', rigged up revers circulating unit, drilled to 7351 and rubber plug and found float collar at 7352' - circulated clean.

Felt for fill, no fill, came out of the hole measuring on the hook, picked up 4-3/4" but and Baker casing scrapper and 4 drill collars and ran in the hole; scrapped casing using poorboy swivel from 7150 to 7352'.

Ground gave away on the South side of cellar, moved to the North side, mixed salt water to increase weight to 69#/cu.ft. - displaced fresh water and mud out of the hole.

Called Schlumberger to shoot WSO holes and Halliburton to test; came out of the hole with scrapper, made up perforating gun, went into hole, collars checked ok, perforated four holes at 7289'. Ran tester with 567' fresh water cushion, set packers at 7242' tail at 7257', opened tester at 4:50 PM, strong blow of gas to surface in 3 minutes, flowed for 2 hours at 2600 psi- 1/4" bean, closed well in over night - 12 hours. Shut in tubing pressure 2720.

Flowed well through 1/4" choke through a small test separator for two hours, pressure 2600 psi, estimated rate 550 MCF/D. Pulled packers loose. Mixed a batch of 74#/cu.ft. of salt water before starting out of the hole and pumped into well 30-40 bbls at a maximum pressure of 1350 psi at the pump. Started out of the hole keeping hole full with 74# mud, well started gassing up about 2 stands out of the hole, a bubble of gas must have followed packers. Closed tubing rams, bled off gas, pulled tools out of the hole (recovered 216) of gas pulled tools out of the hole (recovered 216) of gas pulled tools out of

the hole, (recovered 316' of condensate and 62' of condensate cut mud, I.H.P. 3332 psi, I.F. 256 psi, F.F. 3060 psi, F.S.I. 3332 psi, F.H.P. 3332 psi, WSO approved

Date

5-23

5-24

5-25

5-26

5-27

Date

5-27

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6-13

6-14

7-21

#### SUBMIT IN DUPLICATE

RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

PAGE #5

### History of Oil or Gas Well

Operator	E. A. Bender, Operator Cheney Ranch
Well No.	Silver Creek No. 57X-18, Sec. 18, T. 14S, R. 13E, M.D. B. & M.
	Sox 52,
Bakers	field, Ca. 93302(805)-831-7461 Title Vice President
(Addr	(Telephone Number) (President, Secretary or Agent)
dinning and	the greatest importance to have a complete history of the well. Use this form to report a full account of all important operations during the testing of the well or during re-drilling, altering of casing, plugging, or abandonment with the dates thereof. Be sure to include such items formation test details, amounts of cement used, top and bottom of plugs, perforation details, sidetracked junk, bailing tests, shooting and tion data.
diverse	Completion (Continued)
	by Mr. E. V. Kaarlela of DOG), dropped donut into the
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	Pressure on casing 750 psi - Halliburton arrived with 200 sx of salt and a pump truck; changed valve on tubing and rigged up Halliburton to pump into casing, mixed more 74#/sx of salt water, bled well down, pumped in 30 bbls of salt water, well appears dead. Ran 230 joints of 2-3/8", 4.70#, N-80 EUE tubing to 7284' (Schlumberger measurements), landed tubing, installed Xmas tree. Rigged up to swab. Swabbed 45 bbls of salt water into 340 bbls tank. Shut in over night.
	Tubing pressure and casing pressure about 1270 psi blew down tubing, swabbed 10 times, well started flowing into tank, released pulling rig. Well looks like it is cleaning up, flowing pressure is 1900 psi on 11/64" bean. Shut well in about 9:00 PM.
PP Colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in the colombra in	Tubing pressure 2500 psi; will production test WSO holes.
	Cleaning up location.
	Shut in tubing pressure 2570 psi, casing pressure 2673 psi. Opened well to determine stablized flow rate at 12:07 PM, well stabilized producing at 1200 Mcf/d rate through 3/16" orifice, tubing pressure 1465 psi, casing pressure 1680 psi. Produced heavy condensate mixed with gas and no apparent water.
	Shut in pressure: tubing 2419; casing 2670.
	Halliburton pumped down casing 60 bbls of salt water while

venting gas through tubing.

Silver Creek #57X 18
BIT RECORD

Stop for D.S.T.	Flug back to 3999' Face off cement plug
Hours 16-1/2 11-1/4 10-1/2 11-1/4 7-1/2 4-1/4	3/4 6-1/2 2-3/4 11 6-3/4 8 11-3/4 9 6 11-3/4
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#### RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

### DIVISION OF OIL AND GAS

PAGE #6

### History of Oil or Gas Well

OPERATOR E. A. Bender, (	Operator	Fier	_D Cheney	Ranch	i j		
Well No. Silver Creek No.	57X (18), Sec.	18	. T. 14S	R.	13E	M D. R	8r 34
					j	Af	a CC IVI.
P.O. Box 52,							and the second section in the sec
Bakersfield, Calif.93 (Address)	3302 (805) 831- (Telephone Number)	7461	Title		(Presid	ent, Secretary or Ag	gent)
It is of the greatest importance to have a drilling and testing of the well or during reas hole size, formation test details, amounts of initial production data.							

Date

1973

7-22

7-23

.7 - 24

Completion (Continued)

Bled tubing pressure to 1500 psi.

Welex using portable mastpole and Double Bowen Flow Tubes and Magnetic Sidekicker perforated four holes per foot from 7327 to 7335 through tubing.

Flowed salt water through tubing into 300 bbls water tank; well cleaned up. Shut well in. Preparing location for producing equipment.

PTAYE OF CALIFORNIA DEPARTMENT OF CONSERVATION

### DIVISION OF OIL AND GAS

PAGE 8

#### History of Oil or Gas Well

OPERATOR E.A. BENDER,	OPERATOR	Fiel	Cheney	Ranch	·
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Date			<del></del>	· · · · · · · · · · · · · · · · · · ·	., ., ., ., ., ., ., ., ., ., ., ., ., .
Bakersfield, Ca. 93	309(805) 831-	-7461	Tirla		
(Address)			A RIC	(Pre	sident, Secretary or Agent)

It is of the greatest importance to have a complete history of the well. Use this form to report a full account of all important operations during the drilling and testing of the well or during re-drilling, altering of casing, plugging, or abandonment with the dates thereof. Be sure to include such items as hole size, formation test details, amounts of cement used, top and bottom of plugs, perforation details, sidetracked junk, bailing tests, shooting and initial production data.

Date 1973

#### Single Shot Deviation Record

Depth	Angle
1590'	00 15
2774'	10 45 ·
3832 '	30 15 4
4952'	2º 30 t
54551	1° 00'
6142'	3º 00 •
6828'	N.G.
7260'	30 30+

are Projected.

Stations at 7329' and 7379'

D

Date: May 1973 Job No. L5-1973

Well No. Silver Creek 57X-18 Cheney Ranch, California Elevation:

Section Bearing (None) Decl. 16 0 East

Survey by: Eastman Oil Well Survey Co.

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sec. 18-145-13E **

OPERATOR E. A. BENDER, OPER. "Silver Creek" WELL NO. 57X-18 LEASE 3681KB FIELD AREA Cheney Ranch COUNTY Fresno ELEV. MAP W-33 4 AM 4/24/73 SPUD. LOCATION From SE cor Sec., 660°N 1980°W 5/30/73 сомр. RSM. RECOMP. ABAND. DATE OF ISSUE: 6/9/73 7500 , Rd.7379 T. D. A.P.L. 019-20736 CLASSIFICATION: Gas PLUG CASING RECORD 1973 footage drilled 10,846 SIZE DEPTH MARKERS T. Cherry Sy 9음 1693 Cmtd. ら言 7359 Cmtd. 2-7/87285 Hung INTERVAL 4 holes at 72891 DATE | DIPTH | 12/22/72 Location. CONTRACTOR Tiger Drilling Co., #6 12/23/72 Location, D.O.G. GEOLOGIST 4/23/73 Rigged rotary. Cemented  $9\frac{5}{8}$ " at 1693 . ENGINEER 4/25/73 1693 4/26/73 2570 Drilling 4/27/73 4307 Drilling PROPOSED DEPTH 4/30/73 7260 Ran Welex 1-ES. 5/ 1/73 Drill stem tested. ½ mile N of Operator's "Cheney 5/ 2/73 7500 Ran I-ES 7260-75001. Ranch" #73X, completed 10/20/72, 5/ 3/73 Plugged back to redrill. for 2570 MCF/D, 4" bean, 2263/2320% 5/ 4/73 Redrilling from 4033 with Int: 7253-631 - Moreno Sand. dyna-drill. 5/ 7/73 Redrilling at 56291. 5/ 8/73 Redrilling at 61921. 5/ 9/73 Redrilling at 68121. 5/10/73 Bd.7379 Redrilled to 73791. Ran Sonic and I-ES. 5/14/73 Standing cemented with  $5\frac{1}{2}$ " casing at 7359". Released rig 6 PM 5/12/73. 5/18/73 Moved in Pyramid Oil Co. Production Rig. 5/21/73 Ran Cement Bond Log. 5/25/73 Drilled out cement to bottom of casing. 5/29/73 Flowed 3000 MCF/D thru 16/64" bean on WSO test of 4 holes at 72891. Completed 5/30/73 flowing 500 MCF/D thru #" choke, 2610% T.P., 5/31/73 on 2 hr. test thru 4 holes at 72891.

-10N 1 9 19/3

6-19-73

# RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

# Report on Operations

	No. T 573-123
Mr. Merlin J. Fresch. Agent E. A. HENDER, OPERATOR P. O. Box 52 Bekersfield, CA 93302	Coalinga Calif
DEAR SIR:	
on May 27. 1973 Mr. E. V. Kasrie	e were also present O. Salman, Engineer
The operations were performed for the purpose of	testing the 55" water shut-off by a force-

NVK:ef

JOHN F. MATTHEWS, JR. State Oil and Gas Supervisor

By C. H. Corn

_Deputy

10842-705 1-73 22M @ OSP

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#### RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

# Report on Operations

	No. T 573-100
Mr. Merlin J. Frasch, Agent E. A. BENDER, OPERATOR P. O. Box 52 Bekersfield, CA 93302	Coalinga Calif.
DEAR SIR:	
Operations at well No. "Silver Creek" 57X  M.D., B & M.  on Nav 2, 1973 . Mr. E. V. Kaar  present from 1300 to 1330 . The  Present condition of well: 9-5/8" cere. 1693	Field, in County, were witnessed representative of the supervisor was ere were also present R. McGoey, Engineer
The operations were performed for the purpose of process of redrilling.	of witnessing the plugging operations in the
DECISION: THE LOCATION AND HARDNESS O	F THE CEPENT PLUG AT 6930° IS APPROVED

MW tef cc: Company

JOHN F. MATTHEWS, JR. State Oil and Gas Supervisor

_Deputy

10942-705 1-78 22M @ OSP

FORM 109 (REV. 1-73)

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### RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

# DIVISION OF OIL AND GAS

# REPORT ON PROPOSED OPERATIONS No. P.573-95

Mr. Merlin E. A. Meno P. O. Rox	J. Frasch, Agent SA, OFERATOR	Coalings	Calif
	3, CA 93302	Mar 4, 1973	
DEAR SIR: Your Section 18, dated 5-3-7	T. M. S., R. 13 F., M.D. B. & M.,  73 , received 5 12 , has been examined in	(019-20736) Well No. Silver Creek* 57 Field, Freano conjunction with records filed in th	X, County, nis office.
DECISION:	THE PROPOSAL IS APPROVED PROVIDED THAT to accordance with the provisions outlined : December 22, 1972.		

Mlenket Bond CMC:of co: Company

JOHN F. MATTHEWS, Jr., State Oil and Gas Supervisor

# STATE OF CALIFORNIA DEPARTMENT OF NATURAL RESOURCES

# DIVISION OF OIL AND GAS

# Notice of Intention to Deepen, Redrill, Plug or Alter Casing in Well

This notice must be given before work begins; one copy only

			Bakersfield,	Calif. M	ay 3. 19 73
DIVISION OF	OIL ANI	GAS			
		Coalinga,	Calif.		
	vork of skeep	estringe redrilling, (Cross out unne	Chapter 93, Statutes of 1939,  plugging un abscing coming at	Well No. Silver Cr	eek No. 57X-18
AL-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-1844 AA-184		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	, Sec. 18 , T. 14	S. , R. 13 E.	, M. D. B. & M.
Cheney Ra			Field,		County.
The present cond	lition of the	well is as follows	:		County.
	al depth.	7500 t 6936 t		1.3 19	DAY 1 - 1873
2. Con	nplete casin	g`record.		( .	er en en en en en en en en en en en en en
()	7/8" ope		1693' to 6936'.		
The proposed worl		(Date)	(Net Oil)	(Gravity)	(Cut)
2. ]	Redrill NOTE: A	from 4100 to	s telephone conversa- eer for E. A. Bender	tion on 5-3-73 wir Operator.  BENDER, OPERATOR (Name of Operator)  M. Lossel	th Mr. Ralph

# MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION (Proposed Well Operations)

Operator EA Bender, Ope	Well No. Silver Croek 57x
Field Freshe Co.	Sec. 18 T. 145 R. 13 E B&M
A telephone conversation was held,	concerning above well, with Mr. Ralph Mc Goey
	operator MAM 3 1973, at 1032 4 M.
Details of the conversation were as	*
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Casing record 97/2 Came /	793
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	By operator at
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will be the new engin	Yes () Not necessary (In contradors porque of in Benedis mame only Band Orhan And
V	(Signed) Rank
	Title

# MEMORANDUM OF TELEPHONE OR PERSONAL CONVERSATION (Proposed Well Operations)

Operator C.A.	Well No. Silve	Cristian 57)	
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for above operation	ator May	19 <u>70</u> , at	<u>11 45 AM.</u>
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A soo water cushion was used and I.P. 3213, I.F.P 423, FTP 31. Stratigraphic markers	2, 1.34. 2584		v.
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3. Plug from 1743 - 1643			
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Additional requirements outlined:			
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	Title Messiles	Est.	Miller (M. ), margine and other Product and shall be a still delivery and a second sec

# RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

# DIVISION OF OIL AND GAS

## Report on Operations

	No. T 573-94
Mr. Herlin J. Frasch, Agent. E. A. BENDER, OPERATOR P. O. Box 52 Bakersfield, CA 93302	Coalinga Calif.
DEAR SIR:  Operations at well No. "Silver Creek" 57%  N.D., B & M.  on April 25, 1973 Mr. E. V. Kaarle.  present from 0900 to 0930 There  Present condition of well: 9-5/8" cem. 1593"	, API No. (C19-20736), Sec. 18, T.14S., R. 13E.,  Field, in County, were witnessed to representative of the supervisor was e were also present Fatthews, Driller (Tiger Drilling Co.)  T.D. 2000* (drilling)
The operations were performed for the purpose of equipment and installation.  DECISION: THE BLOWOUT-PREVENTION EQUIPMENT.	inspecting the blowcut-prevention  ENT AND INSTALLATION ARE APPROVED.

TVK:ef cc: Company

JOHN F. MATTHEWS, JR. State Oil and Gas Supervisor

- 04

Deputy

10942-705 1-79 22M @ OSI

7373-94

Operator E.A. E	ender C	<u>Qv.                                    </u>							
Well No. "6; luev Field	CLEEK 31X	1012-5013	(a)	Sec. 18	, T	6, R. 18	E, M	<u>, β</u> , Β	&M
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# RESOURCES AGENCY OF CALIFORNIA DEPARTMENT OF CONSERVATION

## DIVISION OF OIL AND GAS

## REPORT ON PROPOSED OPERATIONS No. P. 572-327

Mr. Merlin J. Frasch, Agent			
E. A. BENTER, OFFICATOR		Coalinga December 22, 1972	
P. O. Sox 52 Sakersfield, CA 93302		1100000000 66 <b>9</b> 6716	
		(019-20736)	
Dear Sir:	arll.	Well No. Silver Creek 57X	9
Your proposal to Section 18, T. 14, S, R. 13 S. M.D.B. & M.,	apriliamentos estas sente difere	Field, Fresno Co	ounty,
dated 12-21-72, received 12-22-72, has	been examined in	conjunction with records filed in this	office.
DECISION: THE PROPOSAL IS APPROVED P	ROVIDED THAT:		
1. The 9" surface casing shall be contained from the shoe to the			o£.
2. Mud fluid of sufficient weight and	d proper consis	stency to prevent blowouts s	
be used in drilling, and the column surface at all times, particularly			!
3. Adequate blowout-prevention equip	ment shall be	installed, consisting in par	
power-operated equipment capable or out of the hole. Power-operate			r in
derrick floor and at a remote loc	etion. For thi	is well, minimum equipment s	hall
consist of an annular preventer a	nd two ram-type	e preventers, one of which i	s a
complete shutoff and the other is 4. This Division shall be notified to		id the drill pipe.	
a. A pressure test of the blowou	t-prevention ex		ring
prior to drilling below the si	hoe of the $9^{n}$ (	i <b>asing.</b> not marforetione immediately	
above the objective sand, price			
Note: Information on file in this of	lice indicates	that the base of the usable	
fresh water deposits should be	encountered at	make a debru of Tim.	
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cc: Company			
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## DIVISION OF OIL AND GAS

## Notice of Intention to Drill New Well

This notice and surety bond must be filed before drilling begins

1 2073			Bakers:	field	Calif	December 21	1972
DIVISION OF O	IL AND (	GAS					
In compliance v	vith Section	n 3203, Division III,	Article 4, Pu	blic Resources C	Code, notice	is hereby giver	that it is our
ntention to comm	ence drillin	ig well No. Silver	Creek No	. 57X-18	/ G.VI	, Sec. 18	, T. 14 S.,
1.13 E., M.	D. B. &	M., Cheney Ran	ch Gas	Fiel	d,	Fresno	County.
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T 14 S. R.	13 E.	MD B&M					
		MDB&M				REC.	CF OB. AND GAS
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# APPENDIX 4 EFFICACY OF MUD PLUGS

## **APPENDIX 4**

## MUD COLUMN CHARACTERISTICS AND CONDITIONS

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### 1.0 EFFICACY OF MUD PLUGS IN ABANDONED WELLS

#### 1.1 SUMMARY

Common drilling mud is largely composed of clays and water, forming a colloidal base. Typically, bentonite (sodium montmorillonite) is added to the drilling mud as the clay and is used to obtain viscosity in the slurry and promoting the formation of wall cake (the low-permeability layer of clay lining the borehole). Bentonite is hydrophilic (it readily absorbs water), and its flat platy shape is the primary reason it is desired for use in common drilling fluids. The development of gel strength in a drilling mud is due to the tendency of the clay platelets to align in a configuration where positively charged edges are adjacent to negatively charged surfaces, resulting in a medium with thixotropic properties. Thixotropy is the characteristic whereby certain gels evolve to a semisolid state when allowed to stand undisturbed but liquefy upon shock disturbance. The gel phase is desirable because it assists in suspending cuttings released by the drilling procedure, producing the required viscosity and mud cake properties in the circulating mud system.

The physical characteristics that make clay-based drilling mud useful during active drilling operations also make it an effective barrier to vertical fluid movement within abandoned boreholes. In thixotropic behavior, under static conditions the clay platelets aggregate (flocculate) in three ways: 1) face-to-face, 2) edge-to-edge, or 3) edge-to-face, because the platelets are electrically charged. This thixotropic or gelling property of a clay-based bentonite slurry is what gives drilling mud its gel strength. In clay-based mud systems, gel structures build with time (progressive gel) as the positive edge of one particle or plate moves toward the negative surface of another; that is, when the platelets are layered (Gray et al., 1980). Laboratory studies have shown that although the exact relationship between gel strength and time varies, depending on specific mud composition and additives, the gel strength always increases with time. Additionally, this orientation of the clay plates reduces the vertical permeability of the mud column significantly because tortuosity through the mud is increased.

Clay-based drilling fluids that contain bentonite or natural clays provide adequate long-term protection against vertical fluid movement into and within in abandoned wellbores. Field studies of mud conditions in decades old abandoned wellbores confirm expectations gained from laboratory testing data and can be used to predict the long-term behavior of relevant mud properties.

1

#### 1.2 INTRODUCTION

Whenever effluent is injected into a subsurface geologic formation, the pressure within the injection interval will increase. This pressure increase will be greatest at the injection well(s) and will decrease with distance away from the injection site. Because of the driving force supplied by the increase in formation pressure within the injection intervals, artificial penetrations within the radius of the effluent plume have the potential to convey effluent out of the injection zone, and artificial penetrations within the Area of Review have the potential to convey formation brines into an Underground Source of Drinking Water (USDW). This is especially so in the specific case where a well is abandoned with brine in the open spaces of the wellbore and/or annulus. However, in rotary drilled wells this is exceedingly rare and only occurs where a formerly productive well is "walked away" from without abandonment.

In a rotary drilled well, the driving force due to injection is opposed by the flow resistance of the material (drilling mud and /or drilling mud and cement plugs) residing in the borehole or the borehole by casing annulus. In order to pose a potential threat to a USDW (*i.e.*, pressure buildup from injection sufficient to drive fluids into a USDW), the pressure increase in the injection interval must be greater than the pressure necessary to displace the material residing within the open spaces in the borehole. This pressure necessary to displace the material residing within the borehole is defined as the allowable buildup pressure.

A mud column exerts pressure. For a well to provide a pathway for fluid movement, the pressures acting on the mud column (pressure due to injection plus original formation pressure) must be greater than the mud column pressure (Davis, 1986). Exploration and production wells are commonly drilled at a mud weight that provides 200 psi or more overbalance to the formations encountered during the drilling activity (Pearce, 1989). In a static fluid column of drilling mud, such as exists upon abandonment of the well, the gel strength of the mud must also be considered. Gel strength refers to the shear stress required to initiate flow after static periods of time (*i.e.*, without mud circulation) and is a measure of the degree of gelation that occurs due to the attractive forces between particles in the mud over time. The gel strength adds to the flow resistance in the well and fluid movement cannot begin until the pressure in the injection interval has increased beyond this critical threshold value necessary to overcome the flow resistance of the borehole material (weight and gel strength).

As long as the pressure buildup in the injection interval is less than the threshold value, the artificial penetration cannot serve as a conduit for either effluent or formation brines (Davis, 1986; Collins

1986). Therefore, as long as the threshold value is not exceeded, the artificial penetration is safe, and corrective action tore-enter and plug the well is not necessary.

#### 1.3 PROPERTIES OF CLAY-BASED DRILLING MUD

The physical characteristics which make drilling muds useful during drilling also make them effective barriers against formation fluid entry into a wellbore and mud-column displacement into a wellbore. This is particularly true of a commonly used base for mud, bentonite, which is predominantly sodium montmorillonite clay. Bentonite-based mud types are used the Cheney Ranch field wells. The platy electrically charged clay particles comprising bentonite strongly attract water, a polar molecule. This causes the clay to swell, thereby increasing the borehole fluid viscosity (Davis, 1986). Of the clays, montmorillonite has the greatest hydration potential and effects the greatest viscosity enhancement for a given amount of solids. This accounts for its long-standing popularity of bentonite as an additive.

A second important property, the gel strength of clay-based drilling muds comes from the tendency of the plate-like clay particles to align so that positively charged edges are adjacent to negatively charged flat surfaces. The gel is "a disheveled yet interconnected network of parallel clay particles separated by an average distance" (Jahnke, 1987). If the mud is agitated, then the gel breaks down. If, on the other hand, the mud sits at rest, then gel strength increases with time as the additional clay particles come into alignment. This is documented by studies conducted by both Garrison (1939) and Gray, et al. (1980). If the drilling fluid is at rest for a long time, high pump pressures are sometimes necessary to restore circulation in the borehole (see example from Cheney Ranch field below). This strong resistive force in a mud column would also need to be overcome during injection.

For many years, alternating cement and mud plugs have been advocated for properly abandoning well bores because they provide an effective barrier to vertical fluid flow. The "balanced method" is the most common method used for the placement of cement plugs during well abandonment procedures. Mud plugs have been shown to have a very low permeability and provide great resistance to fluid movement. In addition, mud plugs have been shown to plug an artificial penetration through time and under the various conditions encountered within a wellbore. A mud plug, with its inherent low permeability, in combination with the hydrostatic head of an overbalanced mud column, is sufficient to counterbalance increased formation pressure due to injection effects, thereby creating an effective barrier to fluid flow. These sealing and fluid barrier characteristics of mud plugs, combined with hydrostatic pressures and natural borehole closure processes, minimize the chance of encountering a truly open conduit in an artificial penetration that was drilled in unconsolidated sediments.

Drilling mud is largely composed of clays and water. Commonly, bentonite-type clays (sodium

montmorillonite) is added to the drilling mud to obtain viscosity in the slurry, in addition to promoting the formation of wall cake (the low-permeability layer of clay lining the borehole). Bentonite is hydrophilic (it readily absorbs water), and its flat platy shape is the primary reason it is desired for use in drilling mud fluids. Clay platelets aggregate (flocculate) in three ways:

- 1) face-to-face,
- 2) edge-to-edge, or
- 3) edge-to-face

Because the platelets are electrically charged. This thixotropic or gelling property of a bentonite slurry is what gives drilling mud its gel strength, as discussed below. Gel structures build with time as the positive edge of one particle or plate moves toward the negative surface of another; that is, when the platelets are layered (Gray et al., 1980). This orientation reduces the vertical permeability of the mud column significantly because tortuosity is increased.

The gel strength and wall cake of bentonite clay mud systems provide an effective barrier against both vertical fluid migration within the wellbore, and migration of fluids into overlying formations. The following subsections examine various aspects of mud plugs and their ability to effectively prevent migration of fluids.

The permeability of drilling mud in abandoned wells depends on the amount and size of the clay particles and other colloids available in the mud slurry, as well as the time the mud has been left in the hole. Although the permeability of mud in deep boreholes has not been measured directly, the permeability of other similar clay mixtures, such as those used in slurry wall construction and bentonite grout slurry mixtures used to plug shallow borings, has been measured and quantified. Alther (1982), while investigating the use of bentonite for clay caps and slurry wall containment, found that a mixture of bentonite and high-permeability soils reduced the coefficient of permeability to  $10^{-9}$  cm/sec. Alther (1982) used a falling head permeameter to measure the permeability of a mixture of 8 percent bentonite and 92 percent Lake Michigan sand.

Polk and Gray (1984) investigated the adequacy of mud as a sealing agent in abandoned boreholes related to mineral exploration. Their focus was on the ability of a bentonite mud to form a filter cake with a low enough permeability to ensure that there would not be fluid flow between aquifers penetrated during drilling. Polk and Gray (1984) directly measured filter cake permeabilities using the cake formed in a standard American Petroleum Institute (API) filter press filtration test run for 30 minutes at a differential pressure of 100 psi. The cake that formed on the filter paper was then

tested with water to determine the cake's permeability. The cake had measured permeabilities ranging from 2 x 10⁻⁸ to 8 x 10⁻⁹ cm/sec, which are regarded as low enough permeability values to prevent fluid flow from one aquifer to another through an open borehole. The filter cake essentially keeps all the solid particles within the mud column. The formation of these low permeability filter cakes is one of the most desirable properties of clay-based mud systems. Experiments show the filter cake to have permeability below microdarcy values (Kelessidis, et al, 2007; Elkatatny et al., 2012). This mud filter cake acts as a membrane "skin" or barrier that effectively seal off formations and prevent fluid loss from the mud column to the formation or loss of fluid from the formation when the well was drilled.

Because the EPA defines "low permeability" for soil as  $1 \times 10^{-7}$  cm/sec, the minimum required permeability of the three feet of compacted clay beneath a landfill or surface impoundment, then it is reasonable to believe that the permeability of a column or mud plug ( $1 \times 10^{-7}$  cm/sec or less) is more than sufficient to prevent movement of fluids within an "open" unplugged well bore.

### 1.3.1 Long-term Properties of Drilling Mud

The functions of the drilling mud result from its physical properties. The primary functions of drilling mud are to prevent the inflow of formation fluids and prevent the collapse of formation materials into the wellbore. These are primarily accomplished by altering the mud weight during drilling. Mud weight can be increased by increasing the salinity of the mud or adding insoluble solids, typically barite (BaSO₄). In general, mud weight is increased with depth so that the mud column will overbalance the encountered formation pressures by 200 to 400 psi (Pierce, 1989). The physical characteristics that make the mud useful during drilling also make it an effective barrier to vertical fluid movement over the long-term.

## 1.3.1.1 Static Mud Column Height

In general, the top of the mud column is found at, or very near, ground level for re-entered boreholes. Documentation offered from several field examples are:

• In the Nora Schulze wellbore, located in Nueces County, Texas, was reentered by K. E. Davis Associates during 1988. The top of the mud plug was encountered immediately below the cement plug at the top of the wellbore (top cement plug), with no fallback in the mud column.

- Subsurface, Inc. (1976) reentered and replugged the Brewster Bartle Drilling Company (British American Oil Production Company), University of Texas No. 1B well located in Galveston County, Texas, during 1976, at the request of Amoco and Monsanto. During the re-entry operation, drilling mud was found immediately below the surface cement plug with its properties relatively intact. This confirms that mud properties maintain their plugging capabilities and offer major resistance as fluid barriers.
- AIC (1988), in a study of well reentries originally plugged 20 to 30 years prior, found that
  in the Texas Gulf Coast and West Texas, most operators reported finding the top of the
  mud just below the surface plug.
- Mr. John Luttig, PE, stated in a letter that he has never encountered voids in e a wellbore devoid of mud in any well reentry in his more than 30 years in the oil fields of East Texas (Luttig, 1990: Pers.Com.). This includes wells that had been plugged for more than 50 years following plugging. He also indicated that he confirmed this statement with his contemporaries.

It is not possible to force significant quantities of mud out of the borehole and out into a permeable formation because of the effect of nearly impermeable residual mud cake that forms along the formation wall.

#### 1.3.1.2 Mud Column Properties

The long-term properties of mud can be determined from a theoretical standpoint. Mud weight should not vary significantly from that at abandonment because virtually all the weighting (barite) particles will remain in suspension due to mud gel strength, which quickly develops. Pearce (1989) found that gravitational settling of barite or other mud additives has been overestimated. Even though settling of the largest drill cuttings particles may occur, overall, this effect does not diminish mud density, or more importantly, affect the plugging and sealing characteristics of a column of mud in an abandoned borehole. The higher the gel strength of a mud column, the larger the particle that can remain in indefinite suspension. This is completely analogous to a solid mechanics problem where a sphere is suspended in an elastic solid. Only when the maximum shear stress on the surface of the particle exceeds the gel strength of the mud will the particle have the potential to settle out of the mud column. For mud-based barite weighting particles, with a density of 4.2 gm/cm³, the critical diameter (in centimeters) for settling is approximately equal to

the gel strength of the mud (lb./100 ft²) divided by 100. For a reasonable low-end gel strength of 20 lb./100 ft² (typically required at 30 minutes measurement time) all barite particles smaller than 0.2 cm will remain in indefinite suspension. In a typical weighted drilling mud, barite particles are generally an order of magnitude less than 0.2 cm in diameter (NL Baroid, 1988). The maximum diameter of the largest 3 percent of the barite particles in standard API weighted mud systems can be no greater than 0.00635 cm (Gray et al., 1980), or 31 times smaller than the theoretical settling size. A gel strength of only 6 lb./100 ft² is needed to suspend 97 percent of the barite in the mud column and the larger drilled solids in the well (Pearce, 1989). Even if these larger drilled solids settle out of the mud, this will not readily affect the weight of the mud as these larger drilled particles are routinely screened out of the mud at surface during active drilling and circulation of the mud system (Pearce, 1989).

Since the solids remain in the mud column, the only way to relieve formation stresses imposed on the static mud column is by compaction and the consequent movement of water from the mud out into the formation. However, this process is self-limiting, any water movement from the mud column will increase the average density of the mud due to the loss of low density water, increase the gel strength and the solids are brought closer together and decrease the effective permeability of the mud column (Pearce, 1989).

#### 1.3.1.3 Mud Column Gel Strength

The relationship between gel strength and time varies with the mud type, depending on such variables as composition, pH, temperature, pressure, solids, and degree of flocculation (Figure 1). Srini-Vasan (1957) investigated the affect of temperature (up to 220 °F) on water-based muds with drilling weights like the wells in the Cheney Ranch Field. Annis (1967) showed that the gelling process is depends on both time and temperature, with 18 parts per billion (ppb) bentonite solution at any temperature having a gel strength six times that of the initial gel strength of the mud. Vryzas et al. (2016) found that the gel-like structure of water/bentonite suspensions proved to be rheologically stable after an aging period of 30 and 60 days.

As shown in Davis and Pearce (1989), Chevron conducted laboratory experiments to determine the expected condition of mud left in wellbores. Chevron formulated muds like those used in Mississippi and "aged" the mud samples at temperature and pressure for a two-week period. The testing showed that the muds developed significant compressive strength and was described as a "plug", with a gel strength too high to measure with standard equipment (Davis and Pearce, 1989).

Field evidence of the longevity of mud as a plugging material has been demonstrated during well reentries. The Nora Schulze No. 2, located in Nueces County, Texas, was reentered by Envirocorp in the late 1980's. The well was plugged with 10.6 to 11.0 lb./gal mud when abandoned in 1959 (Pearce, 1989). Mud samples were taken upon reentry to a depth of approximately 754 feet using tubing pushed into the mud column from a depth of 120 feet. Below a depth of 754 feet, the mud could only be displaced from the well by breaking circulation (Pearce, 1989). Results of measured mud characteristics are presented in Figure 2. The average mud weight of the recovered samples was 11.1 lb./gal, showing that the mud did not appreciably change over the intervening 29 years following abandonment. The gel strengths of the samples ranged between 217 lb./100 ft² to greater than 320 lb./100 ft². These values are over an order of magnitude greater than the 20 lb./100 ft² value required in California plugging rules and commonly used for modeling purposes (Pearce, 1989). In addition, shear strengths of the mud samples ranged from 170 lb./100 ft² to 7,000 lb./100 ft², increasing with depth (Pearce, 1989).

### Additional information on mud characteristics from well reentries are:

- Subsurface, Inc. (1976) reentered and replugged the Brewster Bartle Drilling Company (British American Oil Production Company), University of Texas No. 1B well located in Galveston County, Texas, during 1976, at the request of Amoco and Monsanto. Cement plugs were placed from 11,000 to 11,200 feet, and from 130 to 180 feet, and near the surface (top cement plug) with mud-laden fluid filling the remainder of the wellbore (conforming to Texas Railroad Commission plugging and abandonment requirements of 1961). During the re-entry operation, drilling mud was found immediately below the surface cement plug with its properties relatively intact. The mud had to be circulated out using 12-lb/gal mud.
- AIC (1988), in a study of well reentries originally plugged 20 to 30 years prior, found that
  in the Texas Gulf Coast, most operators reported that the mud was generally hard, with the
  following comments reflecting the condition of the drilling mud and/or borehole fluids
  encountered in the Gulf Coast:
  - mud set up like cement;
  - mud set up firm after about five years; and
  - mud encountered is hard and firm

#### 1.4 CONCLUSIONS

The long-term properties of clay-based drilling mud can be determined from a theoretical standpoint. Mud weight is not expected to vary significantly from that at abandonment (start of static conditions) because virtually all of the weighting barite particles (97%) will remain in indefinite suspension due to gel strength of the mud. Gel strength in clay-based muds generally increases with time due to the electrical attraction of the clay platelets in the mud to continually align.

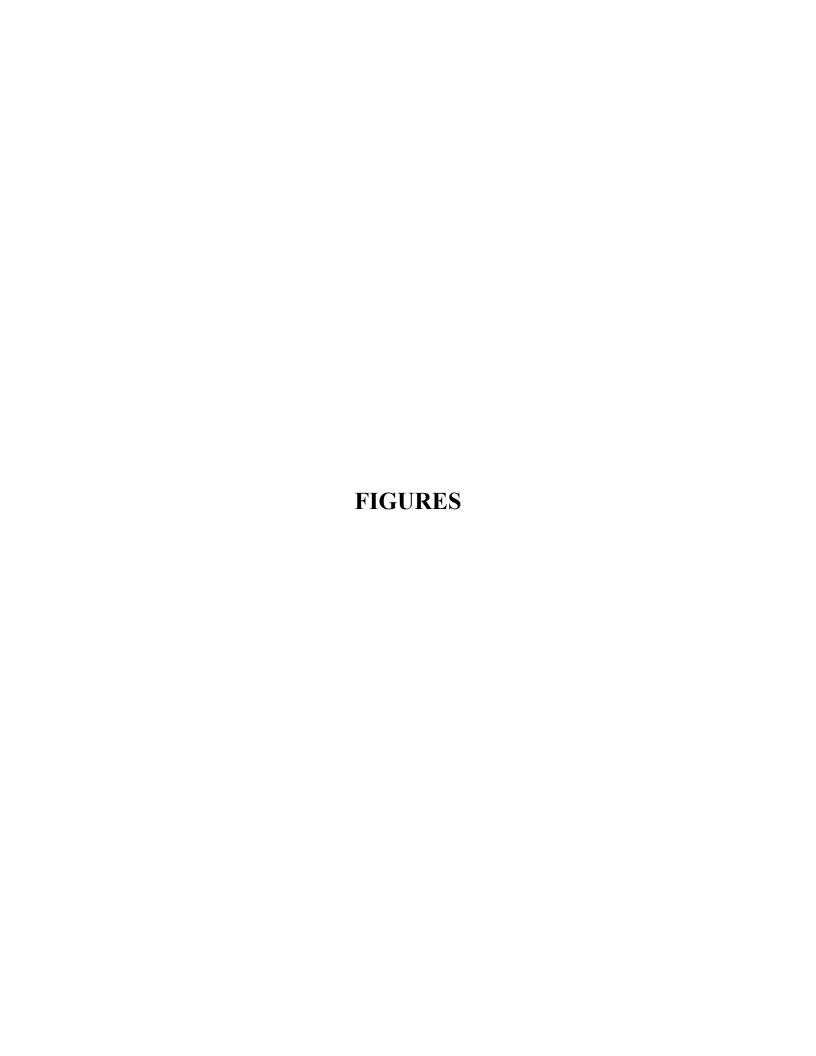
Field investigations from well reentries have found that measured mud properties support the expectations associated with extrapolating laboratory studies over an extended period of time. In the reentry of the Nora Schulte wellbore, mud density remained essentially unaltered, gel strength exceeded 100 lbs./l00 ft², and, even for the most highly gelled samples, the mud remained a fluid. All evidence gathered to date indicates clay, water-based drilling fluids provide adequate protection against vertical fluid migration over short and long time periods.

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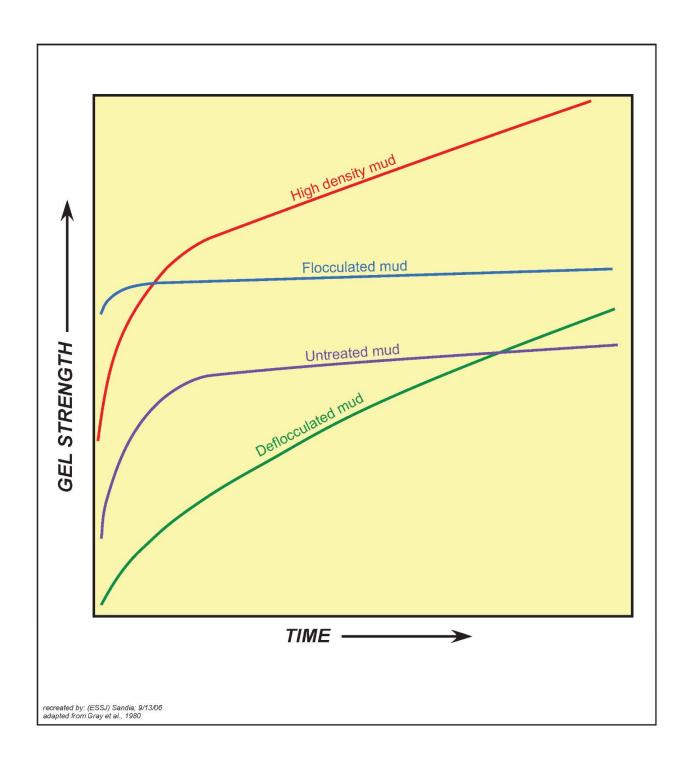


Figure 1 Gel Strength Increase Through Time (Adapted from: Gray et al., 1980)

